TOFINO ASSOCIATES, INC. NORTHERN AVENUE HOMES, INC. (413) 256-0321

31 Campus Plaza Road, Hadley, MA 01035

November 13, 2008

Northampton Planning Board City Hall 212 Main Street Northampton, MA 01060

RE: Application for Special Permit and Site Plan Review/Major Project North Street Condominiums Map 25C, Parcels 12 & 17

Dear Members of the Planning Board,

Enclosed for filing with regard to the North Street townhouse condominium project, please find the following:

- An original and 13 copies of packages containing the following: Application for Special Permit and Site Plan Review Project Summary Building Elevations Summary of Stormwater Drainage Analysis Summary of Traffic Study 24x36" Plans
- 2. Two copies of the full Stormwater Drainage Analysis Report and Management Plan
- 3. Two copies of the full Traffic Study
- 4. A certified abutters list and two sets of stamped, addressed envelopes
- 5. A check in the amount of \$2,682.00 made payable to the City of Northampton.

Additionally, we will file two sets of Planning Board Plans and all supporting material with the Department of Public Works. We are simultaneously submitting a Stormwater Management Permit application with the DPW, and a Notice of Intent with the Conservation Commission.

North Street Condominiums is an infill project consisting of 25 townhouse condominium units on approximately 5.6 acres, located ½ mile from downtown. While the project requires no variances from the Northampton Zoning Ordinance, we are requesting waivers of two of the requirements of Site Plan Review, specifically:

- Waiver of a lighting/photometric plan The project has no street lights. Houses are set close to the interior streets and there will be adequate ambient lighting from front porch lights
- Waiver of a signage plan There will be a single sign with the name of the development, which will be located at the entrance to the project on View Avenue, a private way owned by the applicant. No other signs are proposed except for standard City street name signs, and a temporary construction sign in conformance with 350-7.2(L).

We look forward to presenting this project to the Board in the next month. If you should have any questions, please feel free to contact me at the above phone number.

Sincerely,

Déuglas A. Kohl, President Tofino Associates, Inc. Northern Avenue Homes, Inc.

North Street Condominiums On-Line Application for Special Permit with Site Plan Review

Will the project PROTECT adjoining premises from seriously detrimental uses

The location is zoned for residential use, and it is surrounded by other residential uses.

Will the project MITIGATE and MINIMIZE traffic impacts

This project is true infill development, within easy walking distance of schools, jobs, retail establishments, restaurants, and entertainment. It also provides an important pedestrian connection from the existing sidewalk on North Street to the Norwottuck bike path.

Will the project PROMOTE a harmonious relationship of structures and open space

The townhouse dwelling units are compactly laid out on the land, and an existing path through the open space will still connect the existing houses, as well as the new townhouses, to the bike path.

Will the project PROTECT the general welfare

The proposed townhouse residential use is not detrimental to the general welfare. It is surrounded by other residential uses.

Will the project AVOID OVERLOADING and MITIGATE City resources

The project will not overload the existing City water and sewer in the vicinity, but will most likely add school-aged children. Stormwater is managed on site. The private roadways will be maintained by a Homeowners Association.

Will the project PROMOTE and NOT HARM City planning objectives

The project is consistent with City planning objectives to encourage infill development. It provides attractive residential opportunities within walking distance of downtown, as well as open space and a connection to the bike path.

Will the project Meet all zoning requirements

The project meets zoning requirements and does not require any variances.

Which preferred methods of improved circulation are used

Project minimizes curb cuts Project uses an existing side street Project uses extra measures to reduce parking need Project separates vehicular traffic from bicycle and pedestrian traffic

Describe how the project meets the improved circulation goals (above) and how you reduce curb cuts and parking demand.

The project uses an existing curb cut on North Street (an unnamed subdivision street), and View Avenue (an existing, private side street off North Street) for access. No additional curb cuts are required. Parking is provided by a garage and driveway space in most units, so the use of parking lots is minimized. Vehicular and pedestrian traffic is separated by the use of a separate sidewalk from North street to bike path.

How does project mitigate all traffic impacts?

I am providing justification that there will be no increase in traffic impacts from the project

MAJOR PROJECTS: This project mitigates stormwater impacts by:

All catch basins and manholes have 4' sumps

- All runoff from a 0.4 inch rainstorm (first flush) will be detained for an average of 6 hours
- No increase from PRE to POST-development peak flow during 1, 2, or 10 year NRCS design storm

The impacts are otherwise mitigated (explain)

Runoff is reduced and water is treated through the use of rain gardens/bioswales, a proprietary treatment chamber, an infiltration trench, dry wells, deep sump hooded catch basins, and 2 detention basins. All DEP stormwater requirements are met or exceeded.

I REQUEST a WAIVER from these Site Plan filing requirements (describe why below)

10. Existing and proposed signs locations, dimensions, and details There will be a single sign with the name of the development to be located at the entrance to the project on View Avenue, a private way owned by the applicant. No other signs are proposed except for standard City street name signs, and a temporary construction sign in conformance with 350-7.2(L).

12. Lighting/Photometric Plan (maximum 0.5 foot candles at property boundary) No street lights are proposed

North Street Condominiums Project Summary

Introduction

The proposed project consists of a 2-unit townhouse condominium on Northern Avenue and 23 townhouse condominiums off North Street, for a total of 25 new dwelling units. The site consists of 5.59 acres, and is located within easy walking distance of Downtown.

Circulation Systems

Traffic: The vehicular entry to the project is View Avenue, a private way owned by the applicant, and egress is provided by both View Avenue and an unnamed subdivision street. Roads within the project are narrow, with slow speeds.

Pedestrian: The sidewalk into the project provides a connection to the bike path in a vital location, from an existing and much-used sidewalk along North Street.

Parking: The project minimizes concentrated parking areas; 16 of the 25 units have garages with space to park a second vehicle in the driveway. The other 9 units have driveway surface parking either in front of the unit or elsewhere on site. Additional visitor parking spaces are provided throughout the site.

Traffic mitigation: The project is true infill development, within easy walking distance of downtown, the Bridge Street School, and is adjacent to the Norwottuck bike path.

Support Systems

Water and Sewer: The project is served by City water and sewer along both North Street and Northern Avenue.

Lighting: The project has no street lights – houses are set close to the interior streets and there will be adequate ambient lighting from front porch lights

Signs: There will be a single sign with the name of the development to be located at the entrance to the project on View Avenue, a private way owned by the applicant. No other signs are proposed except for standard City street name signs, and a temporary construction sign in conformance with 350-7.2(L).

Refuse Removal: The Homeowners Association will contract with a private company, such as Pedal People, for trash pick-up. There will be a covenant forbidding dumpsters.

Snow Plowing: The condominium roadways will remain private. A Homeowners' Association will contract with a snow removal service. Roadways are designed for easy snow-plowing, with areas to pile snow at the end of the road near units 21 and 22, the end of the road at unit 3, and in the grass area between units 7 and 8. There will be a covenant also requiring the sidewalk to be plowed up to the end of the units. If the Norwottuck bike path is plowed at some time in the future, then the sidewalk will be plowed up to the bike path.

Plantings and Screening

We would be willing to install street trees, and/or screen plantings, and/or a fence along the street opposite units 3 through 8. This would be done only with the consent of the individual abutters.

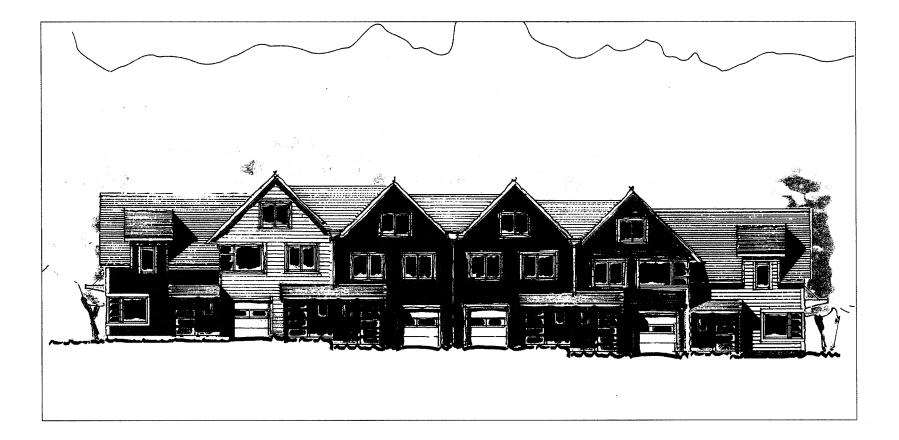
Street trees: Street trees are provided along roadways wherever there is a sufficient adjacent planting area to accommodate a large street tree. We are also willing, at the discretion of the property owners abutting the streets in and out, to plant street trees on their properties.

Screen Plantings: Evergreens will be planted behind units 14-21 to screen the townhouses from abutting houses.

Entry plantings: Each pair of units has a small planting area in front of the porches. There will be a flowering tree, such as a star magnolia, as well as shrubs and groundcovers, planted in each of these planting beds.

Stormwater Management

The project meets or exceeds all 10 stormwater management standards of the MADEP. All runoff from a 0.4 inch rainstorm (first flush) will be detained for an average of 6 hours. Peak flow rates are maintained or reduced in the 2-, 10-, and 100-year storms. For water quality, there is a stormwater treatment chamber, all catch basins have hoods and deep sumps, all road runoff is pre-treated, rain gardens and bioswales slow and filter stormwater. Dry wells are used to infiltrate roof run off.



Northern Avenue Townhouses Stepped Units Northampton, MA June 5, 2007

Kohl Construction

 $\begin{array}{c} \hline KUHN \cdot RIDDLE \\ A & R & C & H & I & T & E & C & T & S \\ 28 & AMITYST \cdot SUITE & 2B \\ A & M & H & E & R & S & T \\ MASSACHUSETTS & 01002 \\ \hline \end{array}$

Aleta DeLisle

From:Gloria McPherson [glm@kohlconstruction.com]Sent:Monday, November 17, 2008 10:21 AMTo:Aleta DeLisleSubject:[Fwd: Planning Board and Zoning Board Application Form Results]

Original Message ----- Subject: Planning Board and Zoning Board Application Form Results
 Date: Fri, 14 Nov 2008 11:54:23 -0600 (CST)
 From: wfeiden@northamptonma.gov <form_engine@fs12.formsite.com>
 Reply-To: wfeiden@northamptonma.gov
 To: glm@kohlconstruction.com

Planning Board and Zoning Board Application

Planning and Zoning Boards

Owner First Name

* Owner Last Name OR Business Name Tofino Associates

* Owner Address 31 Campus Plaza Road

* City Hadley

* State Massachusetts

* Zip Code 01035

Applicant First Name

* Applicant Last Name Northern Ave Homes

Business (if applicable):

* Applicant Street Address 31 Campus Plaza Road

* City Hadley

* State

Massachusetts

* Zip Code 01035

* Phone (413) 256-0321

* Email glm@kohlconstruction.com

* Assessors' Map(s) and Parcel ID(s) 25C-12 and 17

* Parcel Deed Book and Page 8428-219 and 8829-341

* Work Location 8 View Ave and Northern Ave

* Post Office for property Northampton 01060

* Zoning/Overlay Districts URB

* What PERMITS or AMENDMENTS are you applying for?

PLANNING Special Permit w/ INTERMEDIATE Site Plan (\$200, except flag lots \$1,000) PLANNING Special Permit w/MAJOR Site Plan (\$1,000 plus, unless this is an amendment, \$0.05/sq ft of proposed new Х building) PLANNING Intermediate Site Plan (\$200) PLANNING Major Site Plan Approval (\$1,000 plus, unless this is an amendment, \$0.05/sq ft of proposed new building) APPROVAL NOT REQUIRED Surveys (\$250/plan page) PRELIMINARY SUBDIVISION (\$1,000-Type II or \$600-Type I PLUS \$75 per unit) DEFINITIVE SUBDIVISION (Greater of \$3,000 OR \$10/linear foot of new roadway; \$4,600 OR \$14/foot if no preliminary; \$400 PLUS \$10/foot for one lot minor subdivisions; \$500 for Amendments) ZONING BOARD Special Permit (\$200) ZONING FINDING (\$200) APPEAL OF BUILDING COMMISSIONER-Zoning (\$200) COMPREHENSIVE 40B PERMIT (\$500 plus \$0.05/sq ft of proposed new building) VARIANCE (\$1,000 plus \$0.05/sq ft of proposed new building) 43D Permit (Any Planned Village commercial project) * Relevant sections of zoning and subdivision regulations 350-11.3, 11.4, 11.5, 11.6(A-F) * Describe project and relief/approvals needed infill project consisting of 25 townhouse condominium units on approximately 5.6 acres discussed my application with my neighbors (highly recommended) X I HAVE

Finding Request

* How does the project meet the Finding criteria?

The existing property, use, or building is legally preexisting nonconforming

The project does NOT create a new zoning violation

The project is NOT more detrimental to the neighborhood than the old use

* Describe in detail how you meet the Finding Criteria

Appeal of Building Commissioner Action

* Are you claiming:

The Building Commissioner erred in a zoning related matter

A UNIQUE injury as a result of such error that meets the standing test

* Explain in detail 1) What the alleged zoning error the Building Commissioner made and 2) What is the unique injury YOU suffer from the alleged error?

Comprehensive 40B Permit

* Check all that apply for your 40B project

We are not requesting any waivers

We are requesting Zoning waivers

We are requesting Subdivision waivers

We are requesting waivers of other local rules

Attached is our Site Eligibility Letter

Attached is our Draft Affordability Agreement

Attached is our Financial Proforma in compliance with 40B

* Explain WHAT waivers are you requesting, WHY, and HOW could you AVOID them?

Variance Criteria

* I meet the following Variance Criteria

There are UNIQUE circumstances that effect ONLY this property/structure and not other properties in the neighborhood

A literal enforcement of the zoning would create a HARDSHIP, financial or otherwise

If denied there would be NO reasonable use of the property

The hardship is NOT self-imposed

Relief can be granted without detriment to the public good

The variance would not substantially derogate from the intent of the zoning

The request is for the SMALLEST relief possible

* You must document how you meet ALL of the Variance criteria.

Special Permit and Site Plan Criteria

* Will the project

X PROTECT adjoining premises from seriously detrimental uses

* How

The location is zoned for residential use, and it is surrounded by other residential uses.

* Will the project

X MITIGATE and MINIMIZE traffic impacts

* How

This project is true infill development, within easy walking distance of schools, jobs, retail establishments, restaurants, and entertainment. It also provides an important pedestrian connection from the existing sidewalk on North Street to the Norwottuck bike path.

* Will the project

X PROMOTE a harmonious relationship of structures and open space

* How

The townhouse dwelling units are compactly laid out on the land, and an existing path through the open space will still connect the existing houses, as well as the new townhouses, to the bike path.

* Will the project

X PROTECT the general welfare

* How

The proposed townhouse residential use is not detrimental to the general welfare. It is surrounded by other residential uses.

* Will the project

X AVOID OVERLOADING and MITIGATE City resources

* How

The project will not overload the existing City water and sewer in the vicinity, but will most likely add school-aged children. Stormwater is managed on site. The private roadways will be maintained by a Homeowners Association.

* Will the project

X PROMOTE and NOT HARM City planning objectives

* How

The project is consistent with City planning objectives to encourage infill development. It provides attractive residential opportunities within walking distance of downtown, as well as open space and a connection to the bike path.

* Will the project

X Meet all zoning requirements

* How

The project meets zoning requirements and does not require any variances.

Which preferred methods of improved circulation are used

X Project minimizes curb cuts

Project only uses one curb cut

Project uses a common driveway or shared service road for access

X Project uses an existing side street

X Project uses extra measures to reduce parking need

X Project separates vehicular traffic from bicycle and pedestrian traffic

Project is requesting a reduction in required parking spaces as follows:

* Describe how meet the improved circulation goals (above) and how you reduce curb cuts and parking demand. The project uses an existing curb cut on North Street (an unnamed paper street), and View Avenue (an existing, private side street off North Street) for access. No additional curb cuts are required. Parking is provided by a garage and driveway space in most units, so the use of parking lots is minimized. Vehicular and pedestrian traffic is separated by the use of a separate sidewalk from North street to bike path.
* How does project mitigate all traffic impacts?
X I am providing justification that there will be no increase in traffic from the project; OR
I am mitigating ALL off-site incremental traffic ANYWHERE from the project; OR
In lieu of studying and mitigating ALL off-site incremental traffic, I am proposing \$2,000 in-lieu of fee per peak hour vehicle trip (\$1,000 for projects within 1/2 mile of downtown or Florence Center)
I understand that traffic mitigation does NOT replace the need to ensure safe traffic circulation to the site from surrounding streets and nearby intersections
* MAJOR PROJECTS: This project mitigates stormwater impacts by:
All catch basins and manholes have 4' sumps
All runoff from a 0.4 inch rainstorm (first flush) will be detained for an average of 6 hours
No increase from PRE to POST-development peak flow during 1, 2, or 10 year NRCS design storm
The impacts are otherwise mitigated (explain)
DPW has issued a stormwater permit for the project
* I REQUEST a WAIVER from these Site Plan filing requirements (describe why below)
1. Site Plan at $1'' = 40'$ or greater
2. Name and address of the owner and developer, name of project, and date
3. Existing and proposed buildings, property line setbacks, building elevations, exterior entrances/exits
4. Present and proposed use of the land and buildings
5. Existing and proposed topography using 2' contours
6. Wetlands, streams, water bodies, drainage swales, wetlands, unique land features
7. Location of parking and loading, public and private ways, driveways and walkways, access and egress points, proposed surfacing
8. Location and details of all stormwater drainage, detention and water quality facilities, public and private utilities and easements, sewage disposal facilities, water supply facilities
9. Existing and proposed landscaping, trees, plantings, stone walls, buffers, and fencing
X 10. Existing and proposed signs locations, dimensions, and details
11. Provisions for refuse removal and screening
X 12. Lighting/Photometric Plan (maximum 0.5 foot candles at property boundary)
13. Erosion control plan (MAJOR projects only)
14. Traffic Study (MAJOR projects only)
15. Stormwater Management Plan AND Drainage Calculations(MAJOR projects only)
16. Plans stamped by Professional Engineer (10. There will be a single sign with the name of the development to be located at the entrance to the project on View Avenue, a private way owned by the applicant. No other signs are proposed except for standard City street name signs, and a temporary co)
* Add time and place of hearing as soon as it is available
X I have ALREADY posted the REQUIRED sign so it is visible from a public way
http://tinyurl.com/23mopt
ANR Applications must include the following in order to be processed:
 A box located on the lower right of each plan showing the following: A. Approval Not Required signature block
B. A note that "Planning Board Endorsement is not a determination that the lots shown are buildable lots"

C. A list of all parcels shown on the plan with a correspondence table to Northampton Assessors Parcel ID 2. An electronic copy of the survey in AutoCAD 2000 format with all parcels closing to an accuracy of 1 in 25,000 3. Control points when required by the Northampton Subdivision Regulations.

http://www.northamptonma.gov/opd/Abutters%5FLists%5FOld%5FPermits%5FHistoric%5FInventories/

A 43D project (applies to any project with a commercial or industrial component within the Planned Village District) guarantees that most applications for city permits will be processed within 180 days.

To take advantage of this:

- 1. You must apply for all relvent permits at the same time at the start of the process.
- 2. The time clock does not start until the City has determined that the permit applications are complete.

Contact Carolyn Misch, Permt Manager/Senior Planner, Office of Planning and Development, for details.

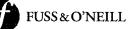
TRAFFIC IMPACT STUDY North Street Condos Northampton, MA

Kohl Construction Hadley, MA

October 14, 2008



Fuss & O'Neill, Inc. 78 Interstate Drive West Springfield, MA 01089



TRAFFIC IMPACT STUDY Proposed Retail Development Great Barrington, MA

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TRAFFIC IMPACT STUDY Proposed Retail Development Great Barrington, MA

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APPENDIX E

Intersection Capacity Analysis Worksheets - Weekday Morning Peak Hour

APPENDIX F

Intersection Capacity Analysis Worksheets - Weekday Afternoon Peak Hour



SUMMARY SHEET

As an aid to reviewers, this Summary Sheet has been included to outline the various study parameters utilized in this report. Although a full explanation of the study methodologies is included in the text of the report, this summary can serve as a useful reference for reviewers.

<u>APPLICANT</u>: Kohl Construction

DEVELOPMENT SIZE/TYPE: 25 Units - Residential Condominium/Townhome

<u>APPLICATIONS</u>: City of Northampton Planning Board

BUILD YEAR: 2013 (2008 +5 years)

BACKGROUND TRAFFIC GROWTH FACTOR: 1% - based on available MassHighway continuous count data

<u>TRAFFIC COUNTS</u>: Data Inc. – October 1, 2008 (Turning Movement Counts) Data Inc. – October 1-2, 2008 (Automatic Traffic Recorders)

<u>PEAK HOURS ANALYZED</u>: Morning Peak Hour – 8:00am to 9:00am Afternoon Peak Hour – 4:15pm to 5:15pm

EXPECTED TRIP GENERATION: Morning Peak Hour – 17 total trip ends Afternoon Peak Hour – 19 total trip ends

<u>CAPACITY ANALYSIS</u>: Technique – 2000 Highway Capacity Manual Execution – Synchro Professional Software, Version 7.0



1.0 INTRODUCTION

1.1 <u>Purpose of Report and Study Objectives</u>

The following report summarizes the site traffic impact assessment for the development of condominium/townhomes on North Street and Northern Avenue in Northampton. The proposed development will be composed of 25 new dwelling units. This report presents the results of a field investigation, traffic counts, and analysis of the estimated traffic to be generated by the proposed project.

1.2 <u>Project Overview</u>

The proposed redevelopment site is located northeast of downtown Northampton. The proposed condominium/townhomes will be located on the northwest side of North Street. Twenty-three units will access North Street via View Avenue, a private way and a proposed driveway also accessing North Street. Two of the units will be located at the end of Northern Avenue. The parcel is currently undeveloped.

The study area is primarily a residential area surrounding North Street. North Street connects King Street, on the east end to Bates Street and Day Avenue, on the west end. This study focused on the intersections and driveway used by the proposed development and major intersection at either end of North Street, where new trips will be most concentrated.

2.0 EXISTING CONDITION

2.1 <u>Site of Development</u>

A locus map of the site location and the surrounding area is provided in <u>Appendix B, Figure 1</u>. The property is zoned Urban Residential. Existing land uses surrounding the study area are:

- Single and Multi-Family housing surrounding the site.
- 0 Industrial Park to the northeast
- o Central Business District of Northampton to the southwest

Currently the proposed location for the condominium/townhomes is undeveloped.

2.2 Adjacent Roadway Network

The study area of influence includes North Street and Northern Avenue that provide access to the site and the surrounding roadway network.

North Street is a collector roadway that runs northeast-southwest through the study area. Pavement width for North Street is 26 feet in the vicinity of the site. North Street is a 2-lane roadway, without lane delineation, which is under the jurisdiction of the City of Northampton. At the time the traffic count was conducted North Street carried an average daily traffic (ADT) of approximately 4,025 vehicles per day in the vicinity of the site.



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Northern Avenue is a dead-end local road under the jurisdiction of the City of Northampton. Pavement width is 20 feet, which includes approximately 8 feet used for on-street parking on the northeast side of the street.

The PVTA does not have a bus route directly passing the site on North Street. There are bus stops within a half mile of the site, however. Sidewalks are provided on both North Street and Northern Avenue.

2.3 <u>Study Area Intersections</u>

The intersections analyzed for this study consist of the following:

- 1. King St (Route 5) / North Street
- 2. North Street / Market Street
- 3. North Street / Northern Avenue
- 4. North Street, Bates Street and Day Avenue

The intersection of King Street, Summer Street and North Street is signalized and actuated with 2 phases. The southbound approach has two lanes, a through lane and a shared through/left turn lane. The northbound approach has a through lane and right turn lane. The eastbound approach, Summer Street, is one-way entering the intersection with a left lane and a shared through/right turn lane. The westbound approach, North Street, has a shared left/right turn lane.

The intersection of North Street and Market Street is one-way stop sign controlled. The eastbound approach, North Street, is stop controlled and has a shared right/left turn lane. The north and southbound approaches are free flowing. The southbound approach, North Street, operates with a through lane and right turn lane. The northbound approach, Market Street, has a single shared left turn/through lane.

The intersection of North Street and Northern Avenue is one-way stop sign controlled. The North Street moves are free flowing while Northern Avenue is stop controlled. Each approach has a single lane shared for all related moves.

The intersection of North Street, Bates Street and Day Avenue is three-way stop controlled. Each approach has a single lane shared for all movements.

2.4 Traffic Volumes, and Counts

The greatest potential for traffic impact on the roadway network by the proposed development will occur during the weekday morning and afternoon peak hour, the period when traffic demand on North Street is typically at its highest level. In order to determine the traffic impact of the proposed development on adjacent street traffic, weekday morning and afternoon peak period manual turning movement counts were conducted in October at the four existing intersections in the study area. The traffic count data collected indicates that the weekday morning peak hour is 8:00am to 9:00am and the afternoon peak hour is 4:15pm to 5:15pm.



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These peak hours was subsequently analyzed for impacts. The existing traffic volumes for these peak hours are shown in <u>Appendix C.</u>

24 hour automatic traffic recorder data was also collected on October 1-2, 2008 on North Street southeast of Northern Avenue. Copies of the ATR traffic data are included in <u>Appendix D</u> of this report.

3.0 BACKGROUND TRAFFIC CONDITIONS

3.1 Growth Rate and Analysis Periods

The proposed project is expected to be completed and fully occupied before the year 2013 (five year projection). Future traffic conditions were estimated by applying a growth factor to all peak hour turning movement traffic volumes to account for regional growth characteristics such as other developments, increasing population, vehicle ownership, workers per household and increased travel mileage. In order to determine a reasonable growth rate for the background traffic volumes within the study area, count data were obtained from MassHighway for Routes 5 and 10 in the vicinity of the site for the years 2002 through 2006.

The count data showed an overall decline in traffic volume over the period data was recorded. Therefore, a growth factor of 1% increase was assumed for this study to be conservative. The data also indicated the month of October has higher than average month traffic volumes. The count data for this study was not adjusted (lower) for the average month.

3.2 Background Developments

There were no other programmed developments anticipated to be completed during the analysis period that would impact traffic within the study area at the time of this study.

3.3 Estimated Volumes

The raw count data for each of the count location were graphically applied to the study area network. The resulting volumes are used as the Base conditions for the traffic estimates. The weekday morning and afternoon 2008 Base condition traffic volume estimates are given in <u>Appendix B, Fig 2</u>. To determine the estimated traffic volumes at the time the project is expected to be fully constructed and occupied the base 2008 volumes were increased with a 1% growth rate for five years to year 2013. This volume estimate provides the 2013 No-Build condition. The weekday morning and afternoon 2013 No-Build condition traffic volume estimates are given in <u>Appendix B, Fig 3</u>.

4.0 PROPOSED CONDITIONS

4.1 Development and Site Access

The proposed development consists of 25 condominium/townhomes. The units are attached in groups with between 2 and 6 units in each group. Seventeen of the dwelling units will have attached garages plus driveway parking space. The remaining units will have driveway surface parking areas and additional visitor parking areas are provided throughout the site.

Two units are isolated on Northern Avenue and will have a driveway at the end of the street. The other 23 units will access the site to and from North Street via two existing private right-ofways to access North Street. The existing right-of-ways will be reconstructed to accommodate site traffic. The first is an unaccepted street View Avenue. View Avenue will serve as both an entrance and exit to the site. The second is a gravel driveway located between Northern Avenue and View Avenue. The on site portion of this driveway will be restricted to one-way exiting the site only.

4.2 <u>Trip Generation</u>

The expected site generated traffic volume was calculated using existing empirical data from the Institute of Transportation Engineers (ITE) publication <u>Trip Generation</u>, 7th edition, 2003. This publication is an industry-accepted resource for determining trip generation.

Trip generation estimated for the proposed developments were estimated based on the total number of proposed dwelling units. The land use for this development is LUC: 230 Residential Condominium/Townhome.

Based on ITE rates the proposed development is estimated to produce 198 new vehicle trips over a typical 24-hour period on weekdays. During the Weekday Morning peak hour the proposed development is estimated to generate 17 new trips and 19 new trips during the Weekday Afternoon peak hour. <u>Table 1</u> presents the daily weekday trip estimates and weekday afternoon trip estimates.

	1	
LUC: 230 Residential Condo	-	use
Development Trip Gene	eration Estimates	
		New Vehicle Trips
Weekday (24 Hour)		
	Entering:	99
	Exiting:	99
	Total:	198
Veekday AM Peak Hour of Adjacent Street Traffic		
Veekday AM Peak Hour of Adjacent Street Traffic	Entering:	3
weekday AM Peak Hour of Adjacent Street Traffic	Entering: Exiting:	3 14
Weekday AM Peak Hour of Adjacent Street Traffic	0	
Weekday AM Peak Hour of Adjacent Street Traffic	Exiting:	14
	Exiting:	14
	Exiting: Total:	<u>14</u> 17

4.3 <u>Trip Distribution</u>



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The distribution of new trips accessing the site was applied to the local road network based on consideration of the existing local traffic distribution and the layout of the adjacent roadway network. Arrival and departure distributions of site traffic were first estimated based on existing patterns at Northern Avenue and then subsequent intersection to the limits of the study area. The estimated trips were split between the three access points to the site the Site Driveway, View Avenue and Northern Avenue. The splits were based on the internal circulation and site layout. The one-way driveway will serve 52% of the trips leaving the site. View Avenue will serve 40% of the trips leaving the site and 92% of the trips entering the site. The two units on Northern Avenue comprise about 8% of the site traffic entering and leaving.

4.4 <u>Combined Volumes</u>

The 2013 Build condition traffic estimates were calculated by adding the site traffic to the projected No-Build traffic volumes. The 2013 Build condition traffic volumes are given in <u>Appendix B, Figure 4</u>. The estimated trip generation and trip distribution used for determining the Build condition traffic volumes are included in <u>Appendix B, Figure 3</u>.

5.0 ANALYSIS

5.1 Accident Review

An analysis to determine crash rate per intersection was prepared to review the level of safety at the study area intersections. Accident data was obtained from MassHighway for each of the study area intersections. The records were gathered for the most recent 3 years of available data, 2004 through 2006. The crash rates, expressed as "crashes per Million Entering Vehicles" (MEV), were determined using the turning movement counts and average number of crashes during the three-year period. A summary of the accident data and resulting crash rates is provided in <u>Appendix A, Table A-1</u>.

The crash rate is a measurement used by MassHighway that compares the number of crashes to the number of vehicles passing through a particular intersection. A crash rate at or below the regional average for a similar facility is an indication that there is likely no unusually hazardous condition or predominant safety factor influencing the frequency of crashes at a location. The crash rates were determined to be below the District 2 average with the exception of the King Street, Summer Street and North Street intersection. The elevated experience on King Street could be a result of the lack of a separate southbound left turn phase and also the offset east and west legs of the intersection.

5.2 Intersection Capacity Analyses

Capacity analyses for both signalized and un-signalized intersections were conducted using Synchro Professional Software, version 7.0.

Level of Service has been determined by the methodology of the "2000 Highway Capacity Manual" published by the Transportation Research Board to describe the operating condition of an intersection. LOS is a measure of the Control Delay experienced by stopped vehicles at an intersection, which is rated on a scale from A to F, with each letter grade assigned a range of delay values in seconds per vehicle. LOS A describes a free flowing condition of very low delay



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(less than 10 seconds per vehicle), and LOS F describes a congested condition where delays will exceed 50 seconds per vehicle at an unsignalized intersection. Control Delay measures the time accumulated when a motorist approaches an intersection including the initial deceleration, queue move-up time, stopped delay, and final acceleration delay. Therefore, intersections with longer Control Delay times are less acceptable to most drivers.

For unsignalized intersection capacity analyses, LOS provides a description of the delay and operational characteristics of the movements from the minor street (usually stop sign controlled) and left turns from the major street into the minor street. Major street through and right turn vehicles typically experience very little delay. Therefore, they are not rated with a LOS at unsignalized intersections.

Using the above referenced methodologies, weekday morning and afternoon peak hour capacity analyses were conducted at the <u>signalized</u> intersection of King Street (U.S. Route 5 and State Route 10), Summer Street and North Street.

Weekday morning and afternoon peak hour capacity analyses were also conducted at the following <u>un-signalized</u> intersections:

- o North Street and Market Street
- North Street & Northern Avenue
- o North Street, Bates Street and Day Avenue
- North Street & View Avenue
- o North Street & the Site Driveway

Existing (2008) and Future No Build (2013) Capacity Conditions:

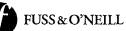
During the weekday morning and afternoon peak hours the LOS at the signalized intersection of King Street, Summer Street and North Street will be LOS C or better. The exception is the westbound approach from North Street. The morning peak hour is expected to operate at LOS E under the No-Build condition. The afternoon peak hour is expected to operate at LOS D under the No-Build condition.

During the weekday morning and afternoon peak hours the LOS at the unsignalized intersections will be LOS C or better under both the Base and No-Build conditions. The exception is the westbound approach from North Street.

Build (2013) Capacity Conditions.

During both the morning and afternoon peak hours the added site traffic is not expected to result in changes to the LOS. Slight increases in delay from site traffic are not significant enough to decrease the LOS letter grade. The new site accesses at View Avenue and the Site driveway will operate at LOS B or better under the Build condition.

The summarized results of the capacity analysis are provided in <u>Tables 2 - 5</u>. The capacity analysis worksheets are provided in <u>Appendices E & F</u>.



		2008 Existing		2013 No Build		2013 Build	
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS
King Street (U.S. Route 5) 8	King Street (U.S. Route 5) & North Street/Summer Street						
Summer Street	EB L	24.8	С	24.5	С	24.4	С
	EB T/R	24.4	С	24.1	С	24.1	С
North Street	WB L/R	52.8	D	60.6	Е	65.2	Ε
King Street	NB T	9.0	А	9.8	А	10.0	А
	NB R	6.3	А	6.7	А	6.8	А
	SB L/T	9.3	А	10.2	В	10.4	В
OVERALL		20.5	С	22.7	С	24.0	С

TABLE 2WEEKDAY MORNING PEAK HOURINTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

TABLE 3WEEKDAY MORNING PEAK HOURUNSIGNALIZED INTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

		2007 Existing			2013 No Build		 Build
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS
North Street & Market Stree	et						
North Street	EB L/R	17.5	С	19.3	С	19.7	С
Market Street	NB L	6.5	А	6.6	А	6.6	А
North Street & Northern Av	venue						
North Street	NB L/T	0.2	А	0.2	А	0.2	А
Northern Avenue	EB L/R	9.7	А	9.7	А	9.9	А
North Street & Bates Street,	/Day Avenue						
North Street	NB L/R	8.5	А	8.7	А	8.7	А
Bates Street	EB T/R	9.4	А	9.6	А	9.6	А
Day Avenue	WB L/T	8.4	А	8.6	А	8.6	А
North Street & View Avenue							
View Avenue	EB L/R	-	-	-		10.0	А
North Street	NB L/T	-	-			0.1	Α
North Street & Site Drivewa	ay						
	EBL/R		-		-	9.9	А

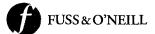


		2008 Existing		2013 No Build		2013 Build	
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS
King Street (U.S. Route 5 an	d Route 10) & N	orth Street/S	lummer				
Street							
Summer Street	EB L	37.5	D	35.0	С	34.6	С
	EB T/R	23.0	С	22.6	С	22.6	С
North Street	WB L/R	44.4	D	48.8	D	49.1	D
King Street	NB T	8.1	А	9.0	А	9.1	А
	NB R	5.0	А	5.4	А	5.5	А
	SB L/T	7.4	А	8.5	А	8.6	А
OVERALL		19.1	В	20.8	С	21.0	С

TABLE 4WEEKDAY AFTERNOON PEAK HOURINTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

TABLE 5WEEKDAY AFTERNOON PEAK HOURUNSIGNALIZED INTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		2008 E	xisting	2013 No Build		2013 Build	
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS
North Street & Market Stree	et					Ι	
North Street	EB L/R	18.9	С	21.1	С	21.1	С
Market Street	NB L	7.7	A ·	7.8	А	7.8	А
North Street & Northern Av	venue						
North Street	NB L/T	0.3	А	0.3	А	0.3	А
Northern Avenue	EB L/R	10.5	В	10.7	В	10.7	В
North Street & Bates Street	/Day Avenue						
North Street	NB L/R	8.0	А	8.0	А	8.1	А
Bates Street	EB T/R	10.6	В	11.0	В	11.1	В
Day Avenue	WB L/T	8.4	А	8.5	А	8.6	А
North Street & View Avenu	e						
View Avenue	EB L/R	-	-	-	-	10.9	В
North Street	NB L/T	-	-	-	-	0.3	А
North Street & Site Drivewa	ıy						
	EB L/R		-			10.8	В



5.3 <u>Findings:</u>

With regard to impacts due to added site traffic, there will not be a noticeable impact to operation at the existing intersections. The two proposed site accesses, View Avenue and the Site Driveway, will operate safely and efficiently.

Sight distance viewing to the north and south along North Street at both proposed access points, View Avenue and the Site Driveway, is adequate.

6.0 CONCLUSIONS AND RECOMMENDATIONS

The study indicates that completion and occupancy of the proposed development will generate 17 new entering and exiting vehicle trips per hour at the site during the weekday morning peak and 19 new entering and exiting vehicle trips per hour in the weekday afternoon peak.

The additional traffic generated by the proposed project will result in incremental increase in peak period traffic volumes on North Street that will have minimal impact on traffic operations. The site access intersections with North Street are designed to provide safe and efficient traffic operations and the turning movements can be accommodated without consideration of off-site improvements.

Stormwater Drainage Report

for Northern Avenue Housing Northampton, MA

November 11, 2008

Prepared by:

The Berkshire Design Group, Inc.

4 Allen Place, Northampton, Massachusetts 01060

Prepared for: Tofino Associates, Inc. 31 Campus Plaza Road Hadley, MA 01035

Stormwater Drainage Report

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- Figure 2Post Development Drainage Area Map
- Figure 3 USDA Soils Map

Appendices

- Appendix A Pre- and Post Development Hydrologic Calculations
- **Appendix B** Soil Test Pit Information
- Appendix C TSS Removal Summary and Calculations
- Appendix D Standard 3 Recharge Calculations
- Appendix E Proposed Stormwater Management System Operation & Maintenance Plan
- Appendix F Long Term Pollution Prevention Plan
- Appendix G Stormwater Pollution Prevention and Erosion Control Plan

Stormwater Drainage Report

I. Introduction

The following report presents an analysis of the stormwater management system for the proposed development of 25 housing units located off of Northern Avenue in zoning district URB in Northampton, Massachusetts. The proposed development includes 25 new housing units and associated parking areas, driveways, and sidewalks, utilities, landscape features and stormwater management system. The total site area is approximately 6 acres of which approximately 3.4 will be disturbed by construction activities. The impervious area on site will increase due to the new development and the stormwater management system has been designed to minimize proposed peak flows to reduce or match existing flows off the site. Mechanisms to reduce runoff and treat water quality include a rain garden, a proprietary treatment chamber, infiltration trench, dry wells, deep sump hooded catch basins, and 2 detention basins.

II. Site Terrain and Soils

The project site is comprised of gradual sloping terrain, which generally drains toward the wetlands on the west part of the site.

The USDA Soil Survey of Hampshire County, Massachusetts, Central Part report classifies the site soils as (see attached soil map):

• (Ra) Raynham Silt Loam

Hydrologic Group: C Flood Risk: None Depth to Water Table: 0.5'-2.0' Depth to Bedrock: >60"

• (Au) Amostown-Windsor Silty Substratum

Hydrologic Group: C Flood Risk: None Depth to Water Table: 1.5'-3.0' Depth to Bedrock: >60"

• (Ud) Udorthents Smooth

Soil formed by cutting or filling developed area. Reference pedon not given. *Assumed* Hydrologic Group: C

Stormwater Drainage Report

A series of test pits were conducted on site to determine subsurface conditions. The purpose of the test pits was to evaluate the site for the existence of ledge, the ability of the site to support stormwater drainage components, and for groundwater information. In general, the test pits confirmed the USDA Soil Survey findings for the site as ground water is generally very high throughout the site, thereby reducing the potential areas where infiltration would be feasible. The test pit logs are attached in Appendix B.

III. Existing Conditions

The existing site includes one drainage area: E-1. The existing drainage area boundary is depicted on the Pre-Development Drainage Area Plan (Figure 1). The overall curve number (CN) in existing conditions is 74. The control point to determine peak flow in existing conditions is the stream located on the property line west of the site shown on Figure 1 as E-CP. The following is a brief description of the drainage area:

<u>E-1</u>

E-1 is approximately 7.75 acres in size and contains existing houses, pavement, grass, wooded areas, and a large wetland area on the west part of the site. Runoff flows overland in a southwestern direction through the wetlands and to the stream located southwest of the site.

IV. Proposed Conditions

The stormwater management system in proposed conditions has been designed to treat and reduce runoff on site. The proposed site contains eight drainage areas: P-1, P-2, P-3, P-4, P-5, P-6, P-7 and P-8 (Figure 2) and the overall curve number (CN) in proposed conditions is 80. The control point to determine peak flow in proposed conditions is the stream located on the property line located west of the site shown on Figure 2 as P-CP. The following is a brief description of each drainage area:

<u>P-1</u>

P-1 is approximately 4.99 acres in size and contains the northwestern area of the site consisting of all of the wetland area, grass and wooded areas, and new roof and pavement. The drainage follows a similar pattern as in existing conditions. It flows overland in a southwestern direction through the wetlands and to the stream located southwest of the site. The runoff from the back of the new roof areas located within P-1 are directed to dry wells where the water is infiltrated into the ground. These dry wells are designed to be very shallow (approximately one foot in depth) due to high groundwater throughout the site. The dry wells are designed with an overflow outlet that allows roof water to sheet flow across the land toward the wetlands as it does in existing conditions. The new driveway and front roof

Stormwater Drainage Report

areas of units 1 and 2 will flow in a similar pattern as the pavement and grass area does in existing conditions.

<u>P-2</u>

P-2 is approximately 0.24 acres in size and is located in the eastern portion of the site. It contains a portion of the roof from unit 14 and 15 in which runoff flows through roof leaders into the infiltration trench which overflows into a catch basin within the area. This area also contains a small portion of new pavement, grass, and trees. Excluding the roof, all other runoff from this area is directed into a catch basin which flows into a water quality basin then to a detention basin (DB#2) located on the west part of the site.

<u>P-3</u>

P-3 is approximately 0.65 acres in size and is located in the northeastern part of the site. It contains new pavement and roof areas, grass, and a detention basin. Runoff from this area is directed to a water quality swale which flows into a water catch basin followed by a detention/infiltration basin (DB#1) that discharges approximately 100 ft to the south.

<u>P-4</u>

P-4 is approximately 0.34 acres in size in the east part of the site. It contains a portion of the new roof and pavement area, and grass and wooded areas. Runoff flows into a catch basin which directs the water to the infiltration trench noted is area P-2. The runoff follows the same pattern as area P-2 once within the trench.

<u>P-5</u>

P-5 is approximately 0.19 acres in size and is located toward the center of the developed portion of the site. It contains mostly new pavement and roof areas and a small portion is grass and wooded area. Runoff flows into a catch basin where it is directed to a water quality basin and detention basin (DB#2) which discharges approximately 40ft from the wetland, allowing adequate overland flow to occur.

<u>P-6</u>

P-6 is approximately 0.54 acres in size and is located on the south portion of the site. It contains a portion of the roof areas from units 16-21, new pavement, and grassed areas. The runoff is directed to a grass swale which flows into a catch basin. The catch basin flows through a proprietary stormwater treatment chamber that discharges into a detention basin (DB#2).

<u>P-7</u>

P-7 is approximately 0.27 acres in size and is located on the southwestern portion of the site. It contains approximately mostly new roof and paved areas and only a small portion of the area is grass. The runoff flows southwest to a proprietary treatment chamber which discharges into a detention basin (DB#2).

<u>P-8</u>

P-8 is approximately 0.53 acres in size and is located on the southwestern portion of the site. It contains a portion of the roof areas from units 22-25, new paved area, grass, and a detention basin (DB#2) and water quality basin. The paved area flows through a pre treatment system consisting of a stone diaphragm and grassed area which discharges into the water quality basin (rain garden) which overflows into the detention basin. The remaining area of P-8 sheet flows into the detention basin.

V. Calculations and Design

Drainage calculations were performed on Hydrocad Stormwater Modeling System version 8.0 using Soil Conservation Service (SCS) TR-20 methodology. The SCS method is based on rainfall observations, which were used to develop the Intensity-Duration-Frequency relationship, or IDF curve. The mass curve is a dimensionless distribution of rainfall over time, which indicates the fraction of the rainfall event that occurs at a given time within a 24-hour precipitation event. This synthetic distribution develops peak rates for storms of varying duration and intensities. The SCS distribution provides a cumulative rainfall at any point in time and allows volume dependent routing runoff calculations to occur. These calculations are included in the appendices.

The watershed boundaries for calculation purposes are divided according to the proposed site grading and the natural limits of the drainage areas. The curve numbers (CNs) and times of concentration for the existing and proposed subcatchment areas are based on the soil type and the existing and proposed cover conditions at the site. The soil hydrologic group assumed for the site is noted in Figure 3. Watershed subcatchment areas, runoff coefficients and watercourse slopes are based on survey information.

Calculations were performed for the 2-, 10-, and 100-year frequency storms under existing and proposed conditions. The results of the calculations are presented in Table 1 on the following page. Appendix A presents the Hydrocad calculations.

Flow Rates & Water Quantity

In the post development conditions the runoff from the proposed site will be routed to 2 open detention basins located along west part of the developed site. The proposed detention basins will attenuate peak flows in the proposed conditions through the use of outlet control structures. Stormwater will be discharged to the wetland that receives runoff in existing conditions. Although there are 5 infiltration systems are proposed (1 detention/infiltration basin, 4 dry wells and 1 infiltration trench) these were not included in the hydrocad

Stormwater Drainage Report

calculations in order to provide a more conservative runoff quantity. Table 1 on the following page presents the comparison of flow rates and water quantity at both existing and proposed control points.

Table 1	Peak Flow	v and Volu	me Summary

Condition & Point of		2-Year Storm		Storm	100-Year Storm		
Analysis		3.00"		0"	6.50"		
7 maryoro	Peak Flow	Volume	Peak Flow	Volume	Peak Flow	Volume	
	Rate(cfs)	(acre-ft)	Rate(cfs)	(acre-ft)	Rate(cfs)	(acre-ft)	
Existing – Control Pt. (E-CP)*	4.66	0.563	10.95	1.242	20.77	2.320	
Proposed – Control Pt. (P-CP)*	4.62	0.733	10.45	1.477	18.20	2.609	

*Names in parentheses refer to HydroCad model and calculations.

VI. MADEP Stormwater Standards Compliance

The following section details how the project will meet DEP Stormwater Management Policy's ten stormwater management standards.

Standard 1 - Untreated Stormwater

The proposed stormwater system is designed to treat the new point source discharge prior to flowing to the resource area. All new outlets are outfitted with flared ends and rip rap to prevent any erosion from occurring in the area. See Appendix C for TSS removal summary.

Standard 2 - Post-Development Peak Discharge Rates

The stormwater system is designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates leaving the site. In order to reduce runoff rates in proposed conditions 2 detention basins with outlet control structures are proposed. Note that although 5 infiltration systems are proposed, no exhilaration was included in the runoff calculations in order to maintain a more conservative peak discharge rate. Refer to Table 1 Peak Flow and Volume Summary and Appendix A for HydroCAD calculations.

Standard 3 - Recharge to Groundwater

Recharge to groundwater is designed to infiltrate to the maximum extent practicable in proposed conditions. The entire site consists of hydrologic group "C" soils and there is very high groundwater throughout most of the site (see Appendix B for test pit logs) which caused limitations for infiltration on many areas of the site because the separation of 2 feet from groundwater could not be

Stormwater Drainage Report

met. Where possible, infiltration is proposed: half of the areas of the roof from units 1-15 and 22-25 and a portion of the pavement located toward the center of the development are directed to dry wells and an infiltration trench sized to accommodate these areas. The upper detention/infiltration basin (DB#1) has been designed also hold and infiltrate the required recharge volume for its respective drainage area (see Appendix D for recharge calculations). Due to restrictions of the site terrain and soil conditions, not all of the impervious area could be directed to an infiltration system therefore all 5 of the infiltration systems proposed are designed to hold at least twice the required recharge volume and still drawdown within 72 hours in order to meet Standard 3 to the maximum extent practicable (see Appendix D for recharge calculations).

Standard 4 – Water Quality

The proposed stormwater management system has been designed to remove the average annual Total Suspended Solids (TSS) load in excess of 80% for the proposed site conditions (see Appendix C for calculations). There are 4 separate treatment chains proposed:

Treatment Train 1(total of 85% TSS removed)

The first treatment chain contains the impervious areas within P-3. The runoff is directed into a water quality swale to a catch basin which discharges into detention/infiltration basin (DB#1) which has been designed to hold the required water quality volume for its respective area which achieves a total TSS removal rate of approximately 85%. Note that the water quality swale was not included in the calculations of total TSS removal in Appendix C to maintain a more conservative removal rate.

Treatment Train 2(total of 93% TSS removed)

The second treatment chain contains the impervious areas from P-2, P-4, and P-5. The runoff is directed into a catch basins followed by a water quality basin (rain garden) which achieves a total TSS removal rate of approximately 93%. The water quality basin has been designed to hold a larger volume of water (738cf) than the water quality volume required (713cf) for the impervious area directed to it.

Treatment Train 3(total of 90% TSS removed)

The second treatment chain contains the paved impervious areas from P-8. The runoff is through a pretreatment system consisting of a stone diaphragm and grassed area which discharges into a water quality basin (rain garden) which achieves a total TSS removal rate of approximately 90%. The water quality basin has been designed to hold a larger volume of water (738cf) than the water quality volume required (713cf) for the impervious area directed to it.

Stormwater Drainage Report

Treatment Train 4(total of 83% TSS removed)

The third treatment chain contains the impervious areas from P-6 and P-7. The runoff is directed into catch basins and then to a proprietary treatment chamber (Stormceptor STC 900*) which achieves a total TSS removal rate of approximately 83%.

*Note: The stormwater treatment chamber has been sized based on MASTEP test evaluations. The attached table in appendix C displays TSS removal rates for systems based on the impervious area directed to the system. See attached Stormceptor sizing chart for impervious areas directed to the stormwater treatment chamber.

In addition to removal of TSS, a Long Term Pollution Prevention Plan has been created to maintain a clean site and ensure that all BMPs are functioning to their maximum potential. See Appendix F for Long Term Pollution Prevention Plan.

<u>Standard 5 - Higher Potential Pollutant Loads</u> The proposed project is not expected to yield high potential pollutant loads.

Standard 6 - Protection of Critical Areas

The project site does not discharge to critical areas as defined in MA DEP Stormwater Policy Handbook.

Standard 7 - Redevelopment Projects

The redevelopment of previously developed site standard is not applicable for this project.

Standard 8 - Erosion/Sediment Control

Erosion and sediment controls have been incorporated into the project design to prevent erosion, control sediments, and stabilized exposed soils during construction and land disturbance. See Appendix G for Construction Period Pollution Prevention and Erosion Sedimentation Control.

Standard 9 - Operation/Maintenance Plan

An Operation and Maintenance Plan for the proposed project is included in Appendix E. It includes general controls for construction and long term maintenance of the stormwater management system.

Standard 10 – Prohibition of Illicit Discharges

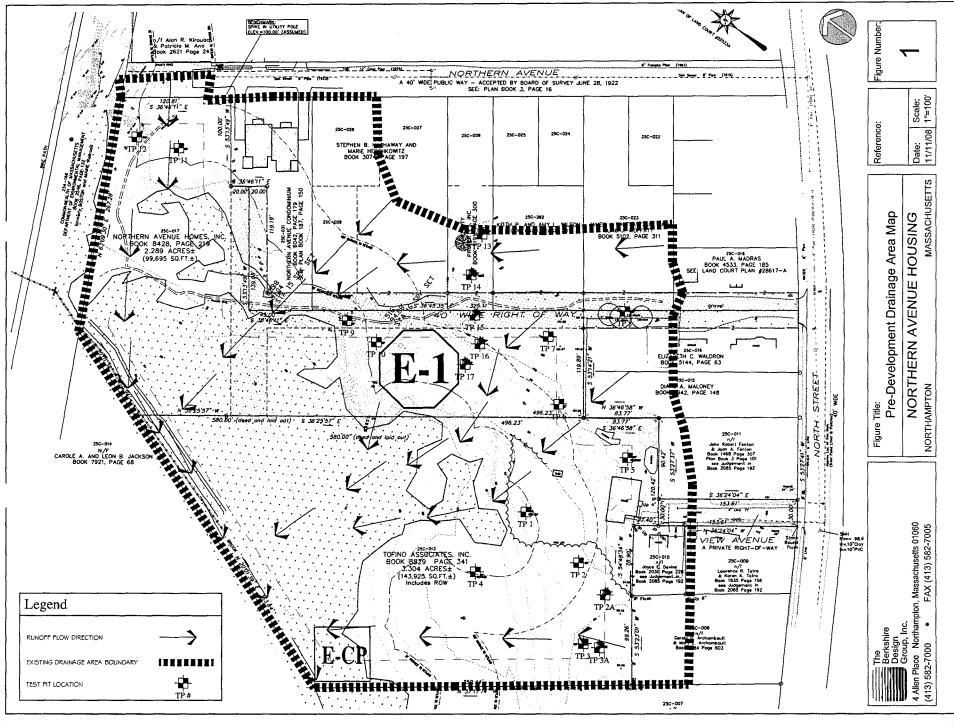
No Illicit Discharge Compliance Statement is included with this report however one will be submitted prior to the discharge of any stormwater to postconstruction BMPs.

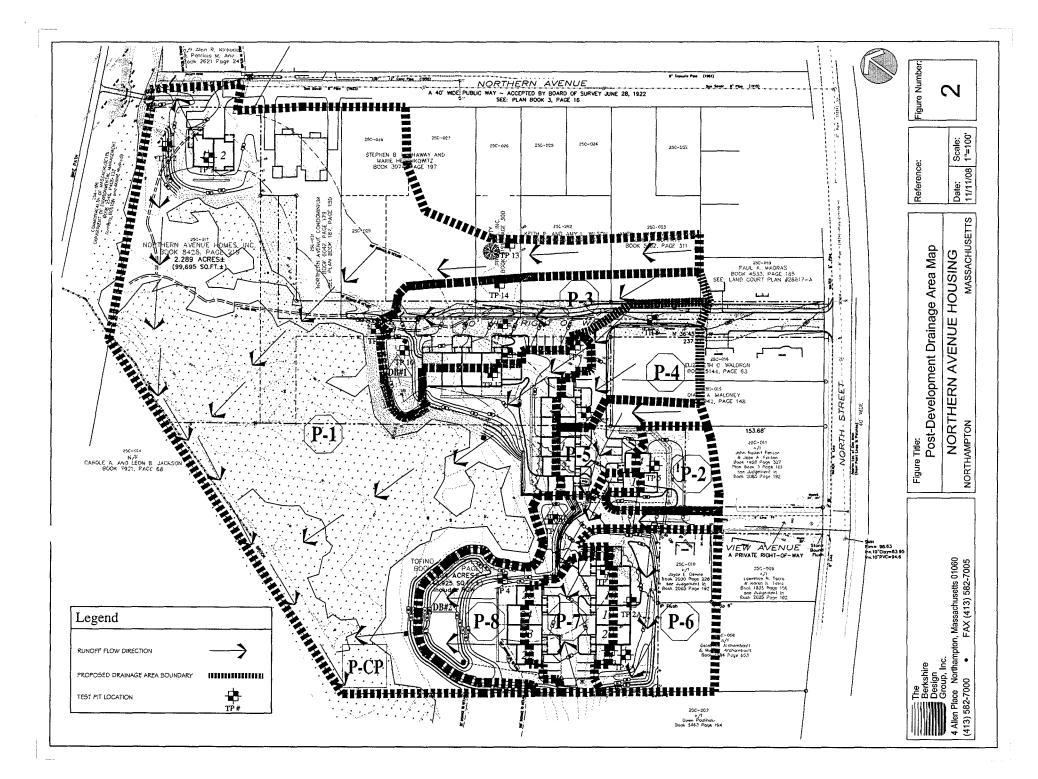
VII. Summary

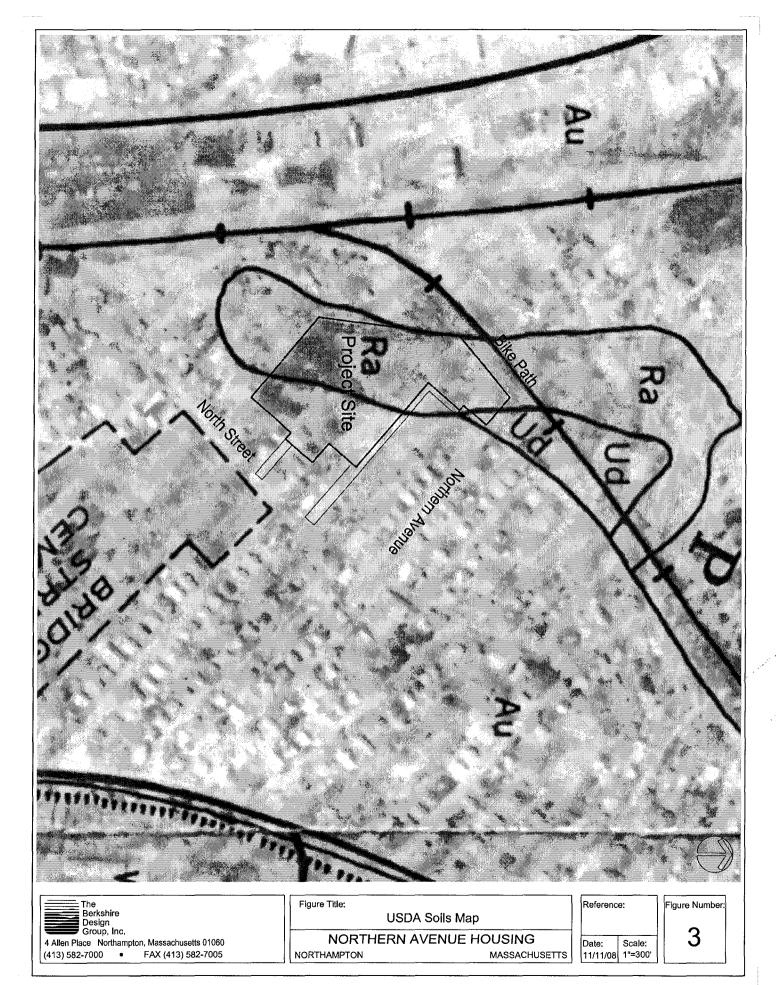
The impervious area from existing to proposed conditions will increase by approximately 51,000 sf from the new roadway and housing units. The proposed stormwater management system is designed to maintain or reduce the peak flow rates in proposed conditions for the 2-, 10-, and 100-year storm frequencies. Special care has been taken to treat runoff with a series of best management practices to ensure water quality and annual TSS removal rates in excess of 80%. These methods include deep sump hooded catch basins, a bioretention basin, a detention/infiltration basin, and a stormwater treatment chamber.

VIII. References

United States Department of Agriculture. 1998. Soil Survey of Hampshire County (Central Part), Massachusetts.







250-17 300' abutters pg. 1

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JACKSON CAROLE A & 90 WOODMONT RD NORTHAMPTON, MA 01060

MALONEY DIANE A 168 NORTH ST NORTHAMPTON, MA 01060

MATUSEK JACOB G & EDITH M 132 RUSSELL ST HADLEY, MA 01035

BRADLEY MARILYN J &

24 COLES MEADOW RD

CAPERS PHYLLIS A &

48 NORTHERN AVE

RAYMOND L

173 NORTH ST

ABBIE

PATRICIA

NORTHAMPTON, MA 01060

NORTHAMPTON, MA 01060

CZELUSNIAK ROBERT F &

NORTHAMPTON, MA 01060

DUNN JAMES PATRICK &

NORTHAMPTON, MA 01060

52 WOODBINE AVE

labels

http://www.northamptonma.gov/permitsearch/labels.aspx?ParcelID...

49 NORTHERN AVE

46 WOODBINE AVE

NOW MARY

186 NORTH ST

O'KANE EILEEN

50 NORTHERN AVE

25 SYCAMORE ST

NORTHAMPTON, MA 01060

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NORTHAMPTON, MA 01060

PAULINSKI DAWN TRUSTEE

SAN FRANCISCO, CA 94110

MUNSKA STELLA G & THOMAS

MERRIAM MARTHA A **63 EVERGREEN RD** LEEDS, MA 01053

MGM REAL ESTATE ASSOCIATES LLC 32 STRONG RD SOUTHAMPTON, MA 01073

NORTHAMPTON CITY OF **210 MAIN STREET** NORTHAMPTON, MA 01060

O'CONNOR COLLEEN M 28 WOODBINE AVE #1 NORTHAMPTON, MA 10160

OLANDER RAE 85 WOODMONT RD NORTHAMPTON, MA 01060

PELKEY LANCE EDWARD & 87 WOODMONT RD NORTHAMPTON, MA 01060

SHAHAR HAIM **38 WOODBINE AVE** NORTHAMPTON, MA 01060

TOFINO ASSOCIATES INC **31 CAMPUS PLAZA RD** HADLEY, MA 01035

WALDRON ELIZABETH C **176 NORTH ST** NORTHAMPTON, MA 01060

WILSON KEITH P & AMY L **20 NORTHERN AVE** NORTHAMPTON, MA 01060 MESSER TIMOTHY A & EILEEN MESSER TIMOTHY A & EHLEEN

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NORTHAMPTON, MA 01060

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WHITE VICTORIA A **15-17 NORTHERN AVE** NORTHAMPTON, MA 01060

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CROUSS TIMOTHY K 6 NORTH BEARS DEN DR SUNDERLAND, MA 01375

DUSHAME LAURA L 52 ORCHARD ST GREENFIELD, MA 01301

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LABATO THERESA'S TRUSTEE 185 NORTH ST NORTHAMPTON, MA 01060

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NORTHAMPTON, MA 01060

Stormwater Drainage Report

for Northern Avenue Housing Northampton, MA

November 11, 2008

Prepared by:

The Berkshire Design Group, Inc.

4 Allen Place, Northampton, Massachusetts 01060

Prepared for: Tofino Associates, Inc. 31 Campus Plaza Road Hadley, MA 01035



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

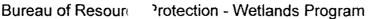
In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.





Checklist for Stormwater Report

B. Stormwater Checklist and Certification

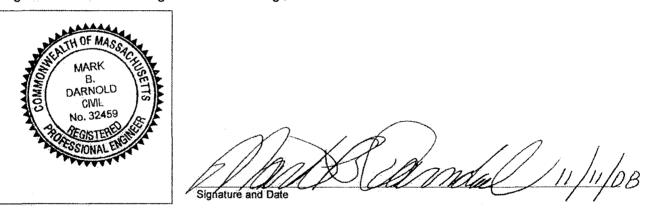
The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the



Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

- No disturbance to any Wetland Resource Areas
- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
 - Credit 1
 - Credit 2
 - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe):

Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Checklist (continued)

Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

- Soil Analysis provided.
- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume for its respective drainage area.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
 - Site is comprised solely of C and D soils and/or bedrock at the land surface
 - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
 - Solid Waste Landfill pursuant to 310 CMR 19.000
 - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Checklist for Stormwater Report

Checklist (continued)

Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- · Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- · Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- · Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.

Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:

is within the Zone II or Interim Wellhead Protection Area

- is near or to other critical areas
- is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)

involves runoff from land uses with higher potential pollutant loads.

- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Massachusetts Lepartment of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

Checklist (continued)

Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
 - The 1/2" or 1" Water Quality Volume or
 - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs) Not Applicable – Proposed project site is not expected to yield high potential pollutant loads.

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted *prior* to the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas Not Applicable - The project site does not discharge to a critical area.

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



Checklist (continued)

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

- The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:site with only "Hydrologic Group C" Soils
 - Limited Project
 - Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
 - Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
 - Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
 - Bike Path and/or Foot Path
 - Redevelopment Project
 - Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.
- ☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Checklist (continued)

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the **DRAFT** SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

Northern Avenue

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Figures

Figure 1	Pre- Development Drainage Area Map
Figure 2	Post Development Drainage Area Map

Figure 3 USDA Soils Map

Appendices

- Appendix A Pre- and Post Development Hydrologic Calculations
- Appendix B Soil Test Pit Information
- Appendix C TSS Removal Summary and Calculations
- Appendix D Standard 3 Recharge Calculations
- Appendix E Proposed Stormwater Management System Operation & Maintenance Plan
- Appendix F Long Term Pollution Prevention Plan
- Appendix G Stormwater Pollution Prevention and Erosion Control Plan

Northern Avenue

Northampton, Massachusetts

Stormwater Drainage Report

I. Introduction

The following report presents an analysis of the stormwater management system for the proposed development of 25 housing units located off of Northern Avenue in zoning district URB in Northampton, Massachusetts. The proposed development includes 25 new housing units and associated parking areas, driveways, and sidewalks, utilities, landscape features and stormwater management system. The total site area is approximately 6 acres of which approximately 3.4 will be disturbed by construction activities. The impervious area on site will increase due to the new development and the stormwater management system has been designed to minimize proposed peak flows to reduce or match existing flows off the site. Mechanisms to reduce runoff and treat water quality include a rain garden, a proprietary treatment chamber, infiltration trench, dry wells, deep sump hooded catch basins, and 2 detention basins.

II. Site Terrain and Soils

The project site is comprised of gradual sloping terrain, which generally drains toward the wetlands on the west part of the site.

The USDA Soil Survey of Hampshire County, Massachusetts, Central Part report classifies the site soils as (see attached soil map):

• (Ra) Raynham Silt Loam

Hydrologic Group: C Flood Risk: None Depth to Water Table: 0.5'-2.0' Depth to Bedrock: >60"

• (Au) Amostown-Windsor Silty Substratum

Hydrologic Group: C Flood Risk: None Depth to Water Table: 1.5'-3.0' Depth to Bedrock: >60"

• (Ud) Udorthents Smooth

Soil formed by cutting or filling developed area. Reference pedon not given. Assumed Hydrologic Group: C

A series of test pits were conducted on site to determine subsurface conditions. The purpose of the test pits was to evaluate the site for the existence of ledge, the ability of the site to support stormwater drainage components, and for groundwater information. In general, the test pits confirmed the USDA Soil Survey findings for the site as ground water is generally very high throughout the site, thereby reducing the potential areas where infiltration would be feasible. The test pit logs are attached in Appendix B.

III. Existing Conditions

The existing site includes one drainage area: E-1. The existing drainage area boundary is depicted on the Pre-Development Drainage Area Plan (Figure 1). The overall curve number (CN) in existing conditions is 74. The control point to determine peak flow in existing conditions is the stream located on the property line west of the site shown on Figure 1 as E-CP. The following is a brief description of the drainage area:

<u>E-1</u>

E-1 is approximately 7.75 acres in size and contains existing houses, pavement, grass, wooded areas, and a large wetland area on the west part of the site. Runoff flows overland in a southwestern direction through the wetlands and to the stream located southwest of the site.

IV. Proposed Conditions

The stormwater management system in proposed conditions has been designed to treat and reduce runoff on site. The proposed site contains eight drainage areas: P-1, P-2, P-3, P-4, P-5, P-6, P-7 and P-8 (Figure 2) and the overall curve number (CN) in proposed conditions is 80. The control point to determine peak flow in proposed conditions is the stream located on the property line located west of the site shown on Figure 2 as P-CP. The following is a brief description of each drainage area:

P-1

P-1 is approximately 4.99 acres in size and contains the northwestern area of the site consisting of all of the wetland area, grass and wooded areas, and new roof and pavement. The drainage follows a similar pattern as in existing conditions. It flows overland in a southwestern direction through the wetlands and to the stream located southwest of the site. The runoff from the back of the new roof areas located within P-1 are directed to dry wells where the water is infiltrated into the ground. These dry wells are designed to be very shallow (approximately one foot in depth) due to high groundwater throughout the site. The dry wells are designed with an overflow outlet that allows roof water to sheet flow across the land toward the wetlands as it does in existing conditions. The new driveway and front roof

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areas of units 1 and 2 will flow in a similar pattern as the pavement and grass area does in existing conditions.

<u>P-2</u>

P-2 is approximately 0.24 acres in size and is located in the eastern portion of the site. It contains a portion of the roof from unit 14 and 15 in which runoff flows through roof leaders into the infiltration trench which overflows into a catch basin within the area. This area also contains a small portion of new pavement, grass, and trees. Excluding the roof, all other runoff from this area is directed into a catch basin which flows into a water quality basin then to a detention basin (DB#2) located on the west part of the site.

<u>P-3</u>

P-3 is approximately 0.65 acres in size and is located in the northeastern part of the site. It contains new pavement and roof areas, grass, and a detention basin. Runoff from this area is directed to a water quality swale which flows into a water catch basin followed by a detention/infiltration basin (DB#1) that discharges approximately 100 ft to the south.

<u>P-4</u>

P-4 is approximately 0.34 acres in size in the east part of the site. It contains a portion of the new roof and pavement area, and grass and wooded areas. Runoff flows into a catch basin which directs the water to the infiltration trench noted is area P-2. The runoff follows the same pattern as area P-2 once within the trench.

<u>P-5</u>

P-5 is approximately 0.19 acres in size and is located toward the center of the developed portion of the site. It contains mostly new pavement and roof areas and a small portion is grass and wooded area. Runoff flows into a catch basin where it is directed to a water quality basin and detention basin (DB#2) which discharges approximately 40ft from the wetland, allowing adequate overland flow to occur.

P-6

P-6 is approximately 0.54 acres in size and is located on the south portion of the site. It contains a portion of the roof areas from units 16-21, new pavement, and grassed areas. The runoff is directed to a grass swale which flows into a catch basin. The catch basin flows through a proprietary stormwater treatment chamber that discharges into a detention basin (DB#2).

<u>P-7</u>

P-7 is approximately 0.27 acres in size and is located on the southwestern portion of the site. It contains approximately mostly new roof and paved areas and only a small portion of the area is grass. The runoff flows southwest to a proprietary treatment chamber which discharges into a detention basin (DB#2).

Stormwater Drainage Report

<u>P-8</u>

P-8 is approximately 0.53 acres in size and is located on the southwestern portion of the site. It contains a portion of the roof areas from units 22-25, new paved area, grass, and a detention basin (DB#2) and water quality basin. The paved area flows through a pre treatment system consisting of a stone diaphragm and grassed area which discharges into the water quality basin (rain garden) which overflows into the detention basin. The remaining area of P-8 sheet flows into the detention basin.

V. Calculations and Design

Drainage calculations were performed on Hydrocad Stormwater Modeling System version 8.0 using Soil Conservation Service (SCS) TR-20 methodology. The SCS method is based on rainfall observations, which were used to develop the Intensity-Duration-Frequency relationship, or IDF curve. The mass curve is a dimensionless distribution of rainfall over time, which indicates the fraction of the rainfall event that occurs at a given time within a 24-hour precipitation event. This synthetic distribution develops peak rates for storms of varying duration and intensities. The SCS distribution provides a cumulative rainfall at any point in time and allows volume dependent routing runoff calculations to occur. These calculations are included in the appendices.

The watershed boundaries for calculation purposes are divided according to the proposed site grading and the natural limits of the drainage areas. The curve numbers (CNs) and times of concentration for the existing and proposed subcatchment areas are based on the soil type and the existing and proposed cover conditions at the site. The soil hydrologic group assumed for the site is noted in Figure 3. Watershed subcatchment areas, runoff coefficients and watercourse slopes are based on survey information.

Calculations were performed for the 2-, 10-, and 100-year frequency storms under existing and proposed conditions. The results of the calculations are presented in Table 1 on the following page. Appendix A presents the Hydrocad calculations.

Flow Rates & Water Quantity

In the post development conditions the runoff from the proposed site will be routed to 2 open detention basins located along west part of the developed site. The proposed detention basins will attenuate peak flows in the proposed conditions through the use of outlet control structures. Stormwater will be discharged to the wetland that receives runoff in existing conditions. Although there are 6 infiltration systems are proposed (1 detention/infiltration basin, 4 dry wells and 1 infiltration trench) these were not included in the hydrocad

calculations in order to provide a more conservative runoff quantity. Table 1 on the following page presents the comparison of flow rates and water quantity at both existing and proposed control points.

Table 1 Peak Flow and Volume Summary

Condition & Point of	2-Year Storm		10-Year Storm		100-Year Storm	
Analysis	3.00"		4.50"		6.50"	
	Peak Flow	Volume	Peak Flow	Volume	Peak Flow	Volume
	Rate(cfs)	(acre-ft)	Rate(cfs)	(acre-ft)	Rate(cfs)	(acre-ft)
Existing – Control Pt. (E-CP)*	4:66	0.563	<i>10.9</i> 5	1.242	20.77	2.320
Proposed - Control Pl (P-(P)*	4.62	0733	10,45	1.477 (*)	^b 18.20	2.609

*Names in parentheses refer to HydroCad model and calculations.

VI. MADEP Stormwater Standards Compliance

The following section details how the project will meet DEP Stormwater Management Policy's ten stormwater management standards.

Standard 1 - Untreated Stormwater

The proposed stormwater system is designed to treat the new point source discharge prior to flowing to the resource area. All new outlets are outfitted with flared ends and rip rap to prevent any erosion from occurring in the area. See Appendix C for TSS removal summary.

Standard 2 - Post-Development Peak Discharge Rates

The stormwater system is designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates leaving the site. In order to reduce runoff rates in proposed conditions 2 detention basins with outlet control structures are proposed. Note that although 6 infiltration systems are proposed, no exfiltration was included in the runoff calculations in order to maintain a more conservative peak discharge rate. Refer to Table 1 Peak Flow and Volume Summary and Appendix A for HydroCAD calculations.

Standard 3 - Recharge to Groundwater

Recharge to groundwater is designed to infiltrate to the maximum extent practicable in proposed conditions. The entire site consists of hydrologic group "C" soils and there is very high groundwater throughout most of the site (see Appendix B for test pit logs). The soil conditions caused limitations for infiltration on many areas of the site because the separation of 2 feet from

groundwater could not be met. Where possible, infiltration is proposed: half of the areas of the roof from units 1-15 and 22-25 and a portion of the pavement located toward the center of the development are directed to dry wells and an infiltration trench sized to accommodate these areas. The upper detention/infiltration basin (DB#1) has been designed also hold and infiltrate the required recharge volume for its respective drainage area (see Appendix D for recharge calculations). Due to restrictions of the site terrain and soil conditions, not all of the impervious area could be directed to an infiltration system, therefore all 6 of the infiltration systems proposed are designed to hold at least twice the required recharge volume and still drawdown within 72 hours in order to meet Standard 3 to the maximum extent practicable (see Appendix D for recharge calculations).

Standard 4 – Water Quality

The proposed stormwater management system has been designed to remove the average annual Total Suspended Solids (TSS) load in excess of 80% for the proposed site conditions (see Appendix C for calculations). There are 4 separate treatment chains proposed:

Treatment Train 1(total of 85% TSS removed)

The first treatment chain contains the impervious areas within P-3. The runoff is directed into a water quality swale to a catch basin which discharges into detention/infiltration basin (DB#1) which has been designed to hold the required water quality volume for its respective area which achieves a total TSS removal rate of approximately 85%. Note that the water quality swale was not included in the calculations of total TSS removal in Appendix C to maintain a more conservative removal rate.

Treatment Train 2(total of 93% TSS removed)

The second treatment chain contains the impervious areas from P-2, P-4, and P-5. The runoff is directed into a catch basins followed by a water quality basin (rain garden) which achieves a total TSS removal rate of approximately 93%. The water quality basin has been designed to hold a larger volume of water (738cf) than the water quality volume required (713cf) for the impervious area directed to it.

Treatment Train 3(total of 90% TSS removed)

The second treatment chain contains the paved impervious areas from P-8. The runoff is through a pretreatment system consisting of a stone diaphragm and grassed area which discharges into a water quality basin (rain garden) which achieves a total TSS removal rate of approximately 90%. The water quality basin has been designed to hold a larger volume of water (738cf) than the water quality volume required (713cf) for the impervious area directed to it.

Stormwater Drainage Report

Treatment Train 4(total of 83% TSS removed)

The third treatment chain contains the impervious areas from P-6 and P-7. The runoff is directed into catch basins and then to a proprietary treatment chamber (Stormceptor STC 900*) which achieves a total TSS removal rate of approximately 83%.

*Note: The stormwater treatment chamber has been sized based on MASTEP test evaluations. The attached table in appendix C displays TSS removal rates for systems based on the impervious area directed to the system. See attached Stormceptor sizing chart for impervious areas directed to the stormwater treatment chamber.

In addition to removal of TSS, a Long Term Pollution Prevention Plan has been created to maintain a clean site and ensure that all BMPs are functioning to their maximum potential. See Appendix F for Long Term Pollution Prevention Plan.

Standard 5 - Higher Potential Pollutant Loads

The proposed project is not expected to yield high potential pollutant loads.

Standard 6 - Protection of Critical Areas

The project site does not discharge to critical areas as defined in MA DEP Stormwater Policy Handbook.

Standard 7 - Redevelopment Projects

The redevelopment of previously developed site standard is not applicable for this project.

Standard 8 - Erosion/Sediment Control

Erosion and sediment controls have been incorporated into the project design to prevent erosion, control sediments, and stabilized exposed soils during construction and land disturbance. See Appendix G for Construction Period Pollution Prevention and Erosion Sedimentation Control.

Standard 9 - Operation/Maintenance Plan

An Operation and Maintenance Plan for the proposed project is included in Appendix E. It includes general controls for construction and long term maintenance of the stormwater management system.

Standard 10 – Prohibition of Illicit Discharges

No Illicit Discharge Compliance Statement is included with this report however one will be submitted prior to the discharge of any stormwater to postconstruction BMPs.

VII. Summary

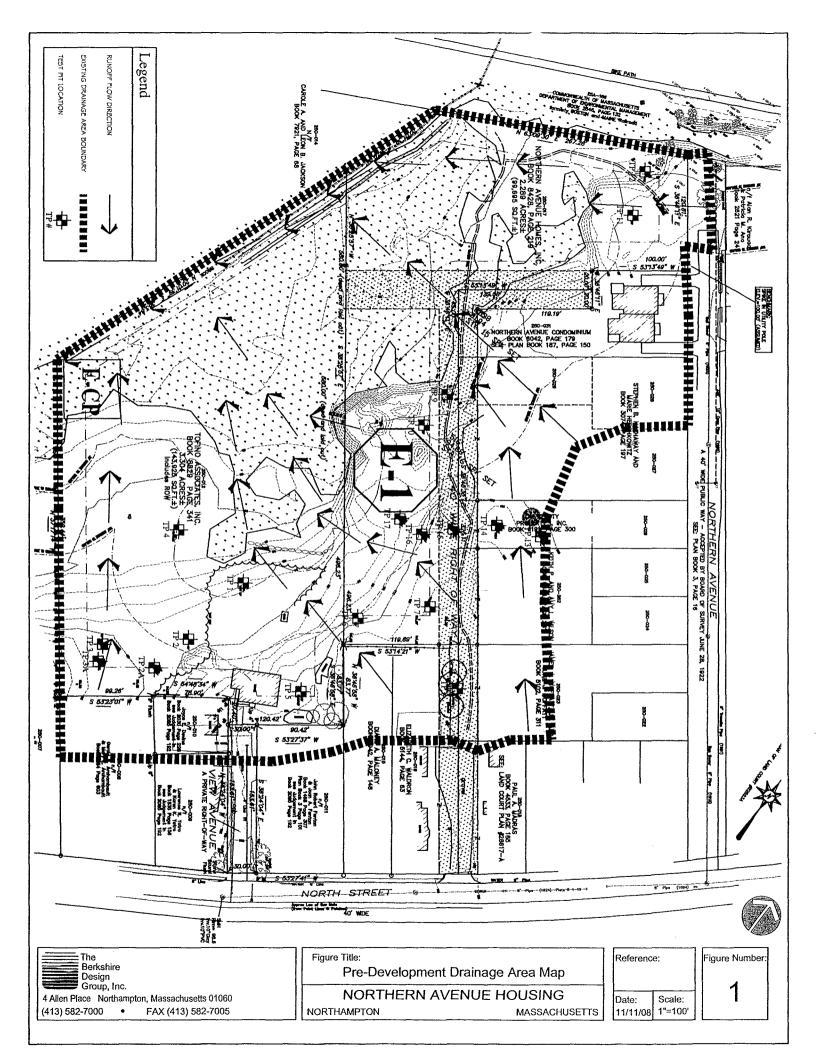
The impervious area from existing to proposed conditions will increase by approximately 51,000 sf from the new roadway and housing units. The proposed stormwater management system is designed to maintain or reduce the peak flow rates in proposed conditions for the 2-, 10-, and 100-year storm frequencies. Special care has been taken to treat runoff with a series of best management practices to ensure water quality and annual TSS removal rates in excess of 80%. These methods include deep sump hooded catch basins, a bioretention basin, a detention/infiltration basin, and a stormwater treatment chamber.

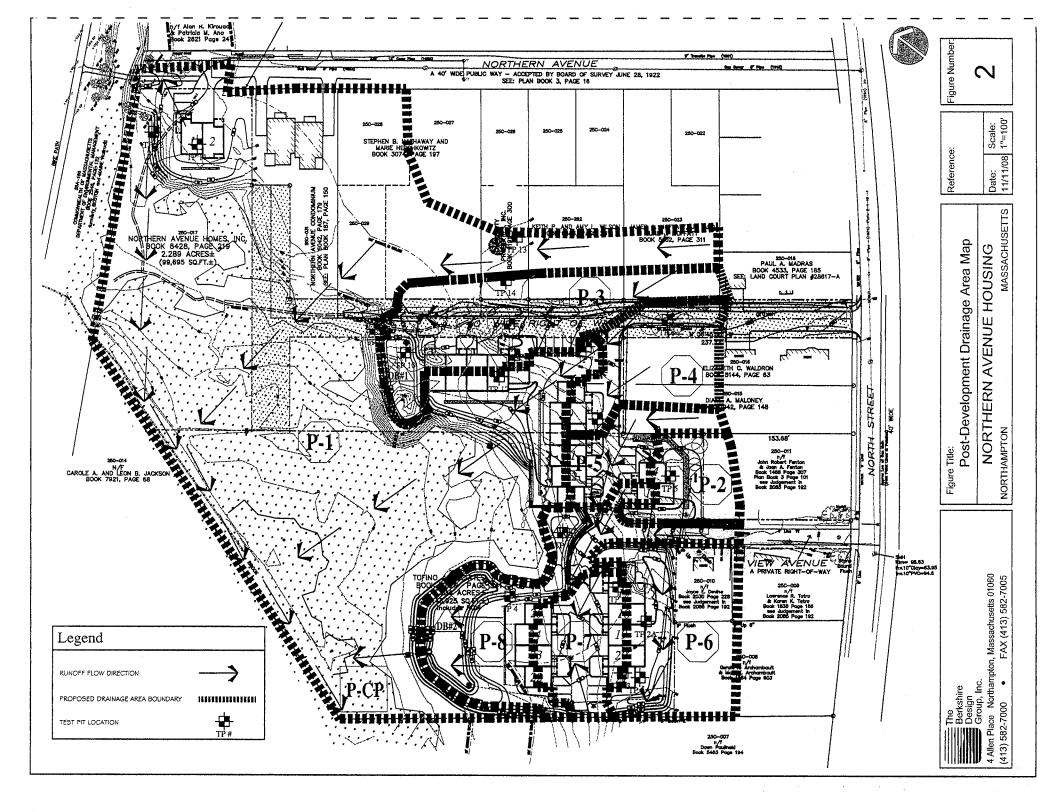
VIII. References

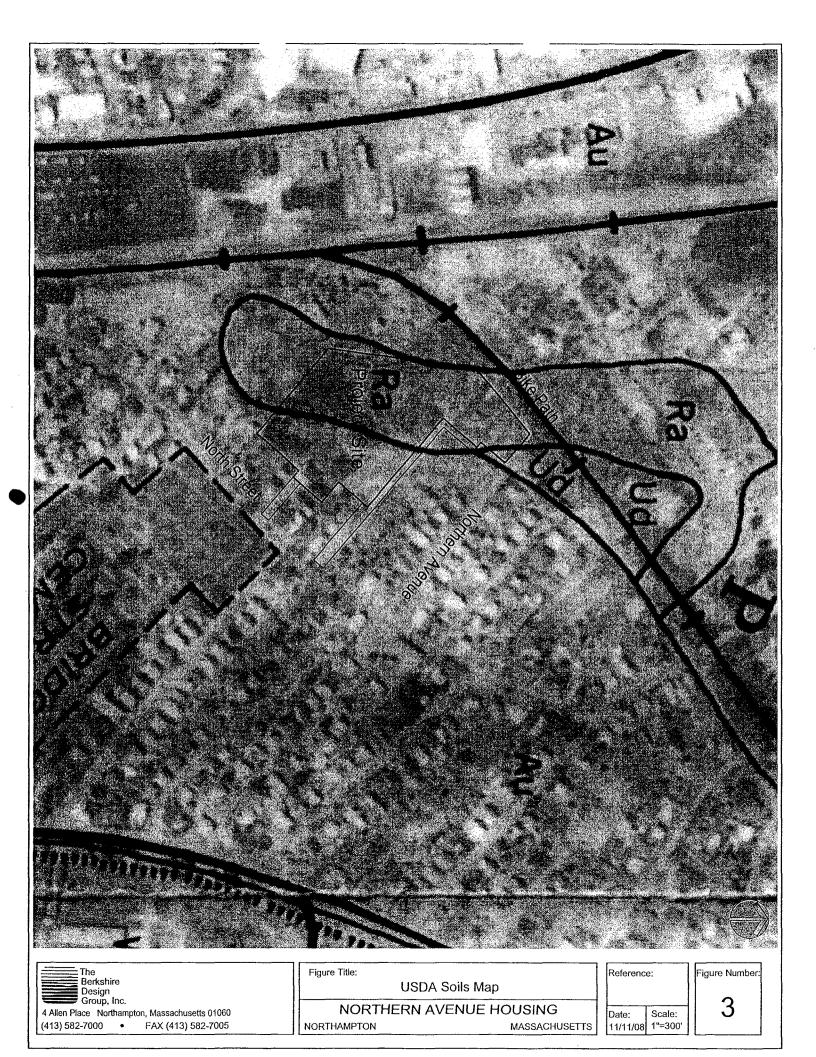
United States Department of Agriculture. 1998. Soil Survey of Hampshire County (Central Part), Massachusetts.

Stormwater Drainage Report Appendix

Figures





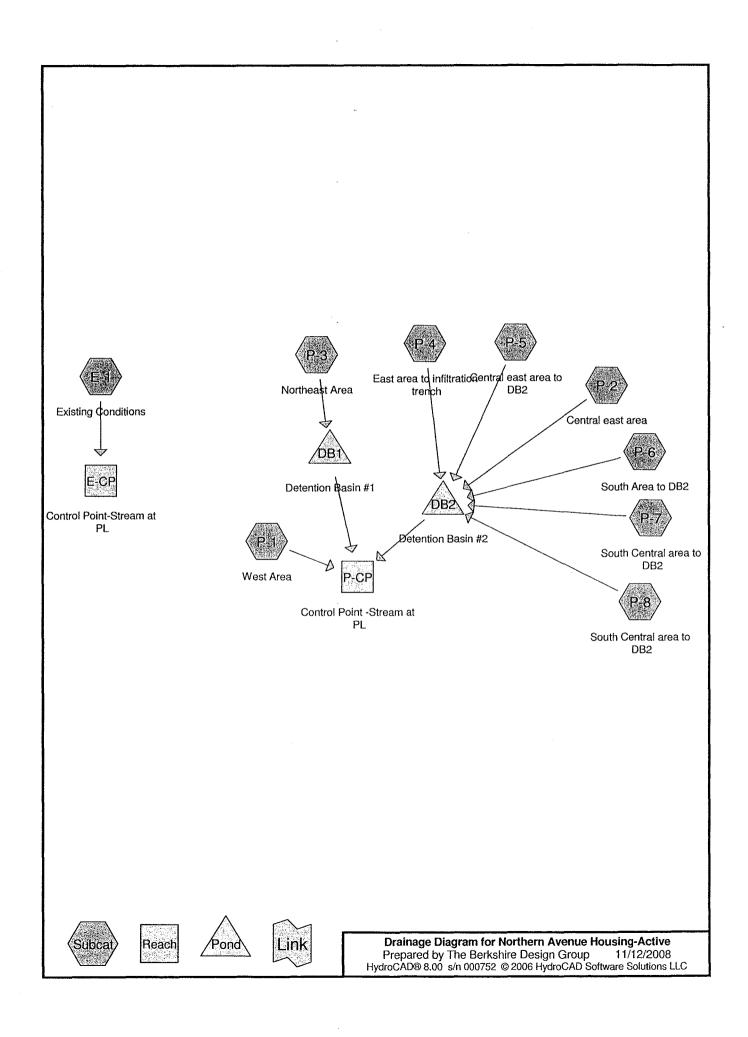


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Stormwater Drainage Report Appendix

Appendix A – Pre- and Post Development Hydrologic Calculations

Appendix



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Area Listing (selected nodes)

- Area (acres) CN Description (subcats)
 - 5.581 70 Woods, Good, HSG C (E-1,P-1,P-3,P-4,P-5,P-6)
 - 3.482 74 >75% Grass cover, Good, HSG C (E-1,P-1,P-2,P-4,P-5,P-6,P-6,P-7,P-8)
 - 4.416 78 Wetlands (E-1,P-1)
 - 0.257 79 50-75% Grass cover, Fair, HSG C (P-3)
 - 0.135 98 Imp. Bldgs, Pavement (E-1)
 - 1.299 98 Paved parking & roofs (P-1,P-2,P-3,P-4,P-5,P-6,P-7,P-8)
 - 0.290 100 Det Basin (P-3,P-8)
 - 0.034 100 Rain Garden (P-8)

15.496

Northern Avenue Housing-Active Prepared by The Berkshire Design Gre HydroCAD® 8.00 s/n 000752 © 2006 Hydro		- <i>Year Rainfall=2.95"</i> Page 3 <u>11/12/2008</u>	
•	.05 hrs, 481 points lod, UH=SCS Pond routing by Stor-Ind r	nethod	
Subcatchment E-1: Existing Conditions	Flow Length=570'	Runoff Area=337,494 Tc=23.1 min CN=74 Re	sf Runoff Depth>0.87" unoff=4.66 cfs 0.563 af
Subcatchment P-1: West Area	Flow Length=351'	Runoff Area=218,209 Tc=19.8 min CN=76 Ru	sf Runoff Depth>0.98" unoff=3.68 cfs 0.408 af
Subcatchment P-2: Central east area		Runoff Area=8,669 Tc=5.0 min CN=76 Ri	sf Runoff Depth>0.98" unoff=0.22 cfs 0.016 af
Subcatchment P-3: Northeast Area	Flow Length=330'	Runoff Area=26,786 Tc=10.0 min CN=89 Ri	sf Runoff Depth>1.85" unoff=1.15 cfs 0.095 af
Subcatchment P-4: East area to infiltrati		Runoff Area=15,343 ' Tc=6.4 min CN=81 Ri	sf Runoff Depth>1.27" unoff=0.51 cfs 0.037 af
Subcatchment P-5: Central east area to		Runoff Area=9,113 7 Tc=6.3 min CN=85 Ri	sf Runoff Depth>1.54" unoff=0.37 cfs 0.027 af
Subcatchment P-6: South Area to DB2	Flow Length=285	Runoff Area=22,259 7 Tc=3.9 min CN=79 Ru	sf Runoff Depth>1.15" unoff=0.71 cfs 0.049 af
Subcatchment P-7: South Central area t		Runoff Area=11,711 Tc=8.8 min CN=93 Ru	sf Runoff Depth>2.20" unoff=0.61 cfs 0.049 af
Subcatchment P-8: South Central area to	o DB2	Runoff Area=25,404 Tc=5.0 min CN=91 Ru	sf Runoff Depth>2.02" unoff=1.37 cfs 0.098 af
Reach E-CP: Control Point-Stream at PL			nflow=4.66 cfs 0.563 af tflow=4.66 cfs 0.563 af
Reach P-CP: Control Point -Stream at Pl	L		nflow=4.62 cfs 0.733 af tflow=4.62 cfs 0.733 af
Pond DB1: Detention Basin #1	Peak Elev=9	3.23' Storage=1,850 cf Ir	
Pond DB2: Detention Basin #2	Peak Elev=9	0.40' Storage=5,173 cf Ir	
Total Runoff Area = 15.49	6 ac Runoff Volu		

Total Runoff Area = 15.496 ac Runoff Volume = 1.342 af Average Runoff Depth = 1.04' 88.65% Pervious Area = 13.736 ac 11.35% Impervious Area = 1.759 ac

- - -

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Subcatchment E-1: Existing Conditions

Runoff 4.66 cfs @ 12.36 hrs, Volume= 0.563 af, Depth> 0.87" =

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=2.95"

•	A	rea (sf)	CN	Description							
		96,180	78	Vetlands							
		92,521	74 :	>75% Gras	75% Grass cover, Good, HSG C						
		5,881		mp. Bldgs,							
-	1	42,912	70	Woods, Go	od, HSG C						
		37,494		Neighted A	•						
	3	31,613		Pervious Ar							
		5,881		mpervious	Area						
	Ta	Longth	Clana	Volocity	Consolt	Description					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
	/////////	······	······································	······	(015)	Check Flow					
	6.7	60	0.0200	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 3.00"					
	4.8	280	0.0375	0.97		Shallow Concentrated Flow,					
	4.0	200	0.0375	0.97		Woodland Kv= 5.0 fps					
	11.6	230	0.0174	0.33		Shallow Concentrated Flow,					
	11.0	200	0.0174	0.00		Forest w/Heavy Litter Kv= 2.5 fps					
_	23.1	570	Total								

Subcatchment P-1: West Area

Runoff 3.68 cfs @ 12.30 hrs, Volume= 0.408 af, Depth> 0.98" =

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=2.95"

Area (s	f) CN	Description
96,18	0 78	Wetlands
23,51	4 74	>75% Grass cover, Good, HSG C
13,94	9 98	Paved parking & roofs
84,56	6 70	Woods, Good, HSG C
218,20	9 76	Weighted Average
204,26	0	Pervious Area
13,94	.9	Impervious Area

Northern Avenue Housing-Active

	d by The	e Berksh	sing-Act ire Desig	n Group	Type III 24-hr 2-Year Rainfall=2		
HydroCA	D® 8.00	<u>s/n 00075</u>	2 © 2006 I	-IydroCAD S	Software Solutions LLC 11/12/		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
8.4	89	0.0250	0.18		Sheet Flow, Grass: Short n= 0.150 P2= 3.00"		
1.5	62	0.0200	0.71		Shallow Concentrated Flow, Woodland Kv= 5.0 fps		
9.9	200	0.0180	0.34		Shallow Concentrated Flow, Forest w/Heavy Litter Kv= 2.5 fps		
19.8	351	Total			· · · · · · · · · · · · · · · · · · ·		
Subcatchment P-2: Central east area							
Runoff	=	0.22 cfs	s@ 12.0	9 hrs, Volu	me= 0.016 af, Depth> 0.98"		
			fall=2.95"				
A	rea (sf) 7,924 745	<u>CN</u> D 74 > 98 P	escription 75% Gras aved park	ing & roofs	ood, HSG C		
A	rea (sf) 7,924	CN D 74 > 98 P 76 V	escription 75% Gras	ing & roofs verage ea	ood, HSG C		
Тс	rea (sf) 7,924 745 8,669 7,924	CN D 74 > 98 P 76 V P Ir	Description 75% Gras Daved park Veighted A Dervious Ar	ing & roofs verage ea Area	ood, HSG C Description		
	rea (sf) 7,924 745 8,669 7,924 745 Length	CN D 74 > 98 P 76 W P Ir Slope	Description 75% Gras Vaved park Veighted A Vervious Ar npervious Velocity	ing & roofs verage ea Area Capacity			
Tc (min)	rea (sf) 7,924 745 8,669 7,924 745 Length	CN D 74 > 98 P 76 W P Ir Slope	Description 75% Gras Verghted A Vervious Ar npervious Velocity (ft/sec)	ing & roofs verage ea Area Capacity (cfs)	Description		
Tc (min)	rea (sf) 7,924 745 8,669 7,924 745 Length	CN D 74 > 98 P 76 W P Ir Slope (ft/ft)	escription 75% Gras vered park Veighted A vervious Ar npervious Velocity (ft/sec) Sub	ing & roofs verage ea Area Capacity (cfs)	Description Direct Entry, nt P-3: Northeast Area		
Tc (min) 5.0 Runoff Runoff b	rea (sf) 7,924 745 8,669 7,924 745 Length (feet) =	<u>CN</u> D 74 > 98 P 76 W P Ir Slope (ft/ft) 1.15 cfs R-20 meth	Description 75% Gras vaved park Veighted A vervious Ar npervious Velocity (ft/sec) Sub	ing & roofs werage ea Area Capacity (cfs) catchme 4 hrs, Volu	Description Direct Entry, nt P-3: Northeast Area		

Area (st)		Description
11,211	79	50-75% Grass cover, Fair, HSG C
4,511	100	Det Basin
9,302	98	Paved parking & roofs
1,762	70	Woods, Good, HSG C
26,786	89	Weighted Average
12,973		Pervious Area
13,813		Impervious Area

Prepare	d by The	e Berksh	sing-Act ire Desigi 2 © 2006 I	n Group	Type III 24-hr 2-Year Rainfall=2.95" Page 6 Software Solutions LLC 11/12/2008			
Тс	Length	Slope	Velocity	• •	Description			
<u>(min)</u>	(feet)	<u>(ft/ft)</u>	(ft/sec)	<u>(cfs)</u>				
8.6	100	0.0300	0.19		Sheet Flow, Grass: Short n= 0.150 P2= 3.00"			
1.4	230	0.0330	2.72		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps			
10.0	330	Total						
	Subcatchment P-4: East area to infiltration trench							
Runoff	Runoff = 0.51 cfs @ 12.10 hrs, Volume= 0.037 af, Depth> 1.27"							
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=2.95"							
A	rea (sf)	CN D	escription					
	3,068	74 >	75% Gras	s cover, Go	bod, HSG C			
	5,529			ing & roofs				
	6,746			od, HSG C				
	15,343	81 V	Veighted A	verage				
	9,814	Р	ervious Ar	ea				
	5,529	lr	npervious	Area				
Tc	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
5.8	100	0.0800	0.29		Sheet Flow,			
0.2	20	0.0180	2.01		Grass: Short n= 0.150 P2= 3.00" Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps			
0.4	60	0.0167	2.62		Shallow Concentrated Flow, Paved Kv= 20.3 fps			

6.4 180 Total

Subcatchment P-5: Central east area to DB2

Runoff = 0.37 cfs @ 12.10 hrs, Volume= 0.027 af, Depth> 1.54"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=2.95"

Area (sf)	CN	Description
2,758	74	>75% Grass cover, Good, HSG C
4,623	98	Paved parking & roofs
1,732	70	Woods, Good, HSG C
9,113	85	Weighted Average
4,490		Pervious Area
4,623		Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.8	100	0.0800	0.29		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.00"
0.1	10	0.0167	1.94		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.4	66	0.0167	2.62		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps

6.3 176 Total

Subcatchment P-6: South Area to DB2

Runoff 0.71 cfs @ 12.07 hrs, Volume= 0.049 af, Depth> 1.15" =

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=2.95"

A	Area (sf)	CN [Description						
	10,347	74 >	4 >75% Grass cover, Good, HSG C						
	5,500	98 F	Paved parking & roofs						
	1,024		75% Grass cover, Good, HSG C						
	<u>5,388</u>	70 \	<u> Voods, Go</u>	od, HSG C	· · · · · · · · · · · · · · · · · · ·				
	22,259		Veighted A						
	16,759		Pervious Ar						
	5,500	[mpervious	Area					
		0		.					
Tc	0	Slope		Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
0.9	80	0.0330	1.56		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 3.00"				
1.5	20	0.1000	0.23		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.00"				
1.5	185	0.0200	2.12		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
3.9	285	Total							

Subcatchment P-7: South Central area to DB2

Runoff 0.61 cfs @ 12.12 hrs, Volume= 0.049 af, Depth> 2.20" =

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=2.95"

Area (sf)	CN	Description
2,278	74	>75% Grass cover, Good, HSG C
9,433	98	Paved parking & roofs
11,711	93	Weighted Average
2,278		Pervious Area
9,433		Impervious Area

11/12/2008

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Type III 24-hr 2-Year Rainfall=2.95" Page 8 C 11/12/2008

_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	8.6	100	0.0300	0.19		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	0.2	33	0.0250	3.21		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	8.8	133	Total			·

Subcatchment P-8: South Central area to DB2

Runoff = 1.37 cfs @ 12.07 hrs, Volume= 0.098 af, Depth> 2.02"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=2.95"

8,246	74	>75% Gras	s cover, Go	od, HSG C			
7,521	98	Paved park	ing & roofs				
8,135	100	Det Basin	-				
1,502	100	Rain Garde	n				
25,404	91	Weighted A	verage				
8,246		Pervious Ar	Pervious Area				
17,158		Impervious	Impervious Area				
Length			Capacity	Description			
	7,521 8,135 <u>1,502</u> 25,404 8,246 17,158	7,521 98 8,135 100 <u>1,502 100</u> 25,404 91 8,246 17,158 Length Slop	7,521 98 Paved park 8,135 100 Det Basin <u>1,502 100 Rain Garde</u> 25,404 91 Weighted A 8,246 Pervious Ar 17,158 Impervious Length Slope Velocity	7,52198Paved parking & roofs8,135100Det Basin1,502100Rain Garden25,40491Weighted Average8,246Pervious Area17,158Impervious AreaLengthSlopeVelocityCapacity	7,52198Paved parking & roofs8,135100Det Basin1,502100Rain Garden25,40491Weighted Average8,246Pervious Area17,158Impervious AreaLengthSlopeVelocityCapacityDescription		

5.0

Direct Entry,

Reach E-CP: Control Point-Stream at PL

Inflow Area =	7.748 ac, Inflow Depth > 0.87"	for 2-Year event
Inflow =	4.66 cfs @ 12.36 hrs, Volume=	0.563 af
Outflow =	4.66 cfs @ 12.36 hrs, Volume=	0.563 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Reach P-CP: Control Point - Stream at PL

Inflow Area =	7.748 ac, Inflow Depth > 1.13"	for 2-Year event
Inflow =	4.62 cfs @ 12.32 hrs, Volume=	0.733 af
Outflow =	4.62 cfs @ 12.32 hrs, Volume=	0.733 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Pond DB1: Detention Basin #1

Inflow Area =	0.615 ac, Inflow Depth > 1.85"	for 2-Year event
Inflow =	1.15 cfs @ 12.14 hrs, Volume=	0.095 af
Outflow =	0.40 cfs @ 12.50 hrs, Volume=	0.069 af, Atten= 66%, Lag= 21.2 min
Primary =	0.40 cfs @ 12.50 hrs, Volume=	0.069 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 93.23' @ 12.50 hrs Surf.Area= 2,100 sf Storage= 1,850 cf

Plug-Flow detention time= 172.3 min calculated for 0.068 af (72% of inflow) Center-of-Mass det. time= 83.1 min (900.2 - 817.1)

Volume	Inve	ert Avail.Sto	rage Storage	Description	
#1	92.2	20' 5,1	03 cf Custon	Stage Data (Prismatic) Listed below (Recal	c)
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	
92.2	20	1,553	0	0	
92.8	30	1,824	1,013	1,013	
93.0	00	1,953	378	1,391	
94.(00	2,602	2,278	3,668	
94.5	50	3,136	1,435	5,103	
Device	Routing	Invert	Outlet Device	9S	
#1	Primary	94.25'	6.0' long x 1	.0' breadth Broad-Crested Rectangular Wei	r
).20 0.40 0.60 0.80 1.00 1.20 1.40 1.60	
			2.50 3.00		
				h) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.1	28 3.31
			3.30 3.31 3.		
#2	Primary	92.10'		long Culvert CMP, projecting, no headwall	Ke= 0 900
	. may	02.10		= 91.73' S= 0.0051 '/' Cc= 0.900	, 110-01000
				ncrete pipe, straight & clean	
#3	Device 2	92.80'		fice/Grate C= 0.600	
#3	Device 2	92.00	0.0 Vert. Of	HCe/Grate C= 0.000	
Primary	OutFlow	Max=0.40 cfs (@ 12.50 hrs H	W=93.23' (Free Discharge)	

-1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

-2=Culvert (Passes 0.40 cfs of 2.36 cfs potential flow)

1-3=Orifice/Grate (Orifice Controls 0.40 cfs @ 2.22 fps)

Pond DB2: Detention Basin #2

Inflow Area =	2.123 ac, Inflow Depth > 1.57"	for 2-Year event
Inflow =	3.69 cfs @ 12.09 hrs, Volume=	0.277 af
Outflow =	0.77 cfs @ 12.54 hrs, Volume=	0.256 af, Atten= 79%, Lag= 27.2 min
Primary =	0.77 cfs @ 12.54 hrs, Volume=	0.256 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 90.40' @ 12.54 hrs Surf.Area= 4,437 sf Storage= 5,173 cf

Plug-Flow detention time= 175.8 min calculated for 0.256 af (92% of inflow)

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Volume	Inve	rt Avail.Sto	rage Storage	Description	
#1	89.0	0' 17,72	22 cf Custom	NStage Data (Pr	ismatic) Listed below (Recalc)
Flourtin		Crut Area	Inc. Otoria	Curre Charge	
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	
89.0)0	3,003	0	0	
90.0	00	3,981	3,492	3,492	
91.0)0	5,124	4,553	8,045	
.92.0	00	6,884	6,004	14,049	
92.2		7,500	1,798	15,847	
92.5		7,500	1,875	17,722	
		.,	.,	,.==	
Device	Routing	Invert	Outlet Device	s	
#1	Primary	88.90'	12.0" x 10.0	Iona Culvert	CPP, square edge headwall, Ke= 0.500
	,				150 '/' Cc= 0.900 n= 0.012
#2	Device 1	89.00'		fice/Grate C=	
#3	Device 1	89.95'		fice/Grate C=	
#4	Primary	92.20'			ad-Crested Rectangular Weir
	1 minuty	02.20	U		0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00	0.20 0.40 0.00	0.00 1.00 1.20 1.40 1.00 1.00 2.00
				h) 0 60 0 70 0	
					75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.	32	
Drimary	OutFlow	Max-0 77 ofs (の 12 54 bre "H	W=90 40' (Free	Discharge)

Center-of-Mass det. time= 137.0 min (958.7 - 821.7)

Primary OutFlow Max=0.77 cfs @ 12.54 hrs HW=90.40' (Free Discharge) -1=Culvert (Passes 0.77 cfs of 3.78 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.27 cfs @ 5.43 fps) **3=Orifice/Grate** (Orifice Controls 0.50 cfs @ 2.28 fps)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Runoff b	9.00-24.00 hrs, dt=0.05 hrs, 481 points by SCS TR-20 method, UH=SCS +Trans method - Pond routing by Stor-Ind method
Subcatchment E-1: Existing Conditions	Runoff Area=337,494 sf Runoff Depth>1.92" Flow Length=570' Tc=23.1 min CN=74 Runoff=10.95 cfs 1.242 af
Subcatchment P-1: West Area	Runoff Area=218,209 sf Runoff Depth>2.08" Flow Length=351' Tc=19.8 min CN=76 Runoff=8.21 cfs 0.869 af
Subcatchment P-2: Central east area	Runoff Area=8,669 sf Runoff Depth>2.09" Tc=5.0 min CN=76 Runoff=0.49 cfs 0.035 af
Subcatchment P-3: Northeast Area	Runoff Area=26,786 sf Runoff Depth>3.24" Flow Length=330' Tc=10.0 min CN=89 Runoff=1.98 cfs 0.166 af
Subcatchment P-4: East area to infiltrat	ion trench Runoff Area=15,343 sf Runoff Depth>2.50" Flow Length=180' Tc=6.4 min CN=81 Runoff=1.00 cfs 0.073 af
Subcatchment P-5: Central east area to	DB2 Runoff Area=9,113 sf Runoff Depth>2.86" Flow Length=176' Tc=6.3 min CN=85 Runoff=0.68 cfs 0.050 af
Subcatchment P-6: South Area to DB2	Runoff Area=22,259 sf Runoff Depth>2.33" Flow Length=285' Tc=3.9 min CN=79 Runoff=1.47 cfs 0.099 af
Subcatchment P-7: South Central area t	to DB2 Runoff Area=11,711 sf Runoff Depth>3.65" Flow Length=133' Tc=8.8 min CN=93 Runoff=0.98 cfs 0.082 af
Subcatchment P-8: South Central area t	to DB2 Runoff Area=25,404 sf Runoff Depth>3.45" Tc=5.0 min CN=91 Runoff=2.29 cfs 0.168 af
Reach E-CP: Control Point-Stream at Pl	L Inflow=10.95 cfs 1.242 af Outflow=10.95 cfs 1.242 af
Reach P-CP: Control Point -Stream at P	L Inflow=10.45 cfs 1.477 af Outflow=10.45 cfs 1.477 af
Pond DB1: Detention Basin #1	Peak Elev=93.70' Storage=2,913 cf Inflow=1.98 cfs 0.166 af Outflow=0.76 cfs 0.139 af
Pond DB2: Detention Basin #2	Peak Elev=91.19' Storage=9,037 cf Inflow=6.72 cfs 0.507 af Outflow=1.59 cfs 0.469 af
	96 ac Runoff Volume = 2.784 af Average Runoff Depth = 2.16" Pervious Area = 13.736 ac 11.35% Impervious Area = 1.759 ac

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Subcatchment E-1: Existing Conditions

Runoff = 10.95 cfs @ 12.33 hrs, Volume= 1.242 af, Depth> 1.92"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.45"

A	rea (sf)	CN I	Description			
	96,180	78	Netlands			
	92,521	74 :	>75% Gras	s cover, Go	ood, HSG C	
	5,881			Pavement		
1	42,912	70	Noods, Go	od, HSG C		_
3	37,494		Neighted A			
3	331,613		Pervious Ar	+		
	5,881	1	mpervious	Area		
+				0		
Tc	Length	Slope		Capacity	Description	
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)		
6.7	60	0.0200	0.15		Sheet Flow,	
					Grass: Short n= 0.150 P2= 3.00"	
4.8	280	0.0375	0.97		Shallow Concentrated Flow,	
					Woodland Kv= 5.0 fps	
11.6	230	0.0174	0.33		Shallow Concentrated Flow,	
					Forest w/Heavy Litter Kv= 2.5 fps	
23.1	570	Total				

Subcatchment P-1: West Area

Runoff = 8.21 cfs @ 12.28 hrs, Volume= 0.869 af, Depth> 2.08"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.45"

 Area (sf)	CN	Description
 96,180	78	Wetlands
23,514	74	>75% Grass cover, Good, HSG C
13,949	98	Paved parking & roofs
 84,566	70	Woods, Good, HSG C
218,209	76	Weighted Average
204,260		Pervious Area
13,949		Impervious Area

Type III 24-hr 10-Year Rainfall=4.45" Page 13 LC 11/12/2008

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	8.4	89	0.0250	0.18		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	1.5	62	0.0200	0.71		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	9.9	200	0.0180	0.34		Shallow Concentrated Flow,
_						Forest w/Heavy Litter Kv= 2.5 fps
	19.8	351	Total			

Subcatchment P-2: Central east area

Runoff = 0.49 cfs @ 12.08 hrs, Volume= 0.035 af, Depth> 2.09"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.45"

A	rea (sf)	CN	Description			_
	7,924	74	>75% Gras	s cover, Go	ood, HSG C	
	745	98	Paved park	ing & roofs	S	
	8,669	76	Weighted A	verage		
	7,924	7,924 Pervious Area				
	745 Impervious Area			Area		
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment P-3: Northeast Area

Runoff = 1.98 cfs @ 12.14 hrs, Volume= 0.166 af, Depth> 3.24"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.45"

CN	Description				
79	50-75% Grass cover, Fair, HSG C				
100	Det Basin				
98	Paved parking & roofs				
70	Woods, Good, HSG C				
89	Weighted Average				
	Pervious Area				
	Impervious Area				
	79 100 98 70				

Northern Avenue Housing-Active				ive	Type III 24-hr 10-Year Rainfall=4.45"		
			ire Desig		Page 14		
HydroCA	D® 8.00	<u>s/n 00075</u>	2 © 2006	HydroCAD S	Software Solutions LLC 11/12/2008		
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
8.6	100	0.0300	0.19		Sheet Flow,		
					Grass: Short n= 0.150 P2= 3.00"		
1.4	230	0.0330	2.72		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps		
10.0	330	Total			Glassed Walerway IV= 15.0 lps		
10.0	000	rotai					
		Su	bcatchm	ent P-4: I	East area to infiltration trench		
Runoff	=	1.00 cfs	s@ 12.1	0 hrs, Volu	ume= 0.073 af, Depth> 2.50"		
			nod, UH=S nfall=4.45		Span= 0.00-24.00 hrs, dt= 0.05 hrs		
A	rea (sf)	CN D	escription				
	3,068				bod, HSG C		
	5,529			ing & roofs			
	6,746			od, HSG C			
	15,343 9,814		Veighted A ervious Ar				
	5,529		npervious				
	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u> 5.8	<u>(feet)</u> 100	(ft/ft) 0.0800	<u>(ft/sec)</u> 0.29	(cfs)	Sheet Flow,		
5.0	100	0.0000	0.29		Grass: Short $n = 0.150$ P2= 3.00"		
0.2	20	0.0180	2.01		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
0.4	60	0.0167	2.62		Shallow Concentrated Flow, Paved Kv= 20.3 fps		
6.4	180	Total					
			Subcato	hment D_/	5: Central east area to DB2		
		•	oubcatc				
Runoff	=	0.68 cfs	s@ 12.0	9 hrs, Volu	me= 0.050 af, Depth> 2.86"		
Runoff b	V SCS TH	R-20 meth	nod. UH=S	SCS. Time S	Span= 0.00-24.00 hrs, dt= 0.05 hrs		
			nfall=4.45				
A	rea (sf)	CN D	escription				
	2,758				bod, HSG C		
	4,623	98 P	aved park	ing & roofs			
	1,732			od, HSG C			
	9,113		/eighted A				
	4,490 Pervious Area						

4,623 Impervious Area

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Type III 24-hr 10-Year Rainfall=4.45" Page 15 LC <u>11/12/2008</u>

_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	5.8	100	0.0800	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	0.1	10	0.0167	1.94		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
	0.4	66	0.0167	2.62		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
_	6.3	176	Total			

Subcatchment P-6: South Area to DB2

Runoff = 1.47 cfs @ 12.06 hrs, Volume= 0.099 af, Depth> 2.	Runoff =	ff = 1.47 cfs @	12.06 hrs,	Volume=	0.099 af,	Depth>	2.33"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.45"

A	rea (sf)	CN [Description					
	10,347	74 >	74 >75% Grass cover, Good, HSG C					
	5,500		Paved parking & roofs					
	1,024		>75% Grass cover, Good, HSG C					
	5,388	<u>70 V</u>	Woods, Good, HSG C					
	22,259	79 Weighted Average						
	16,759		Pervious Ar					
	5,500	Impervious Area						
		~ .		• •				
Tc	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)				
0.9	80	0.0330	1.56		Sheet Flow,			
					Smooth surfaces $n=0.011$ P2= 3.00"			
1.5	20	0.1000	0.23		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.00"			
1.5	185	0.0200	2.12		Shallow Concentrated Flow,			
					Grassed Waterway Kv= 15.0 fps			
3.9	285	Total						

Subcatchment P-7: South Central area to DB2

Runoff = 0.98 cfs @ 12.12 hrs, Volume= 0.082 af, Depth> 3.65"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.45"

Area (sf)	CN	Description
2,278	74	>75% Grass cover, Good, HSG C
9,433	98_	Paved parking & roofs
11,711	93	Weighted Average
2,278		Pervious Area
9,433		Impervious Area

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Type III 24-hr 10-Year Rainfall=4.45" Page 16 LC 11/12/2008

	Tc (min)	Length (fe <u>et)</u>	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	8.6	100	0.0300	0.19		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	0.2	33	0.0250	3.21		Shallow Concentrated Flow,
-						Paved Kv= 20.3 fps
	8.8	133	Total			

Subcatchment P-8: South Central area to DB2

Runoff = 2.29 cfs @ 12.07 hrs, Volume= 0.168 af, Depth> 3.45"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.45"

A	rea (sf)	CN	Description				
	8,246	74	>75% Gras	s cover, Go	od, HSG C		
	7,521	98	Paved park	ing & roofs			
	8,135	100	Det Basin	-			
<u>.</u>	1,502	100	Rain Garden				
	25,404	91	Weighted Average				
	8,246		Pervious Area				
	17,158 Impervious Area						
Тс	Length	Slope		Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)			
5.0					Direct Entry		

5.0

Direct Entry,

Reach E-CP: Control Point-Stream at PL

Inflow Area	a =	7.748 ac, Inflow D)epth > 1.92"	for 10-Year event	
Inflow	=	10.95 cfs @ 12.33	hrs, Volume=	1.242 af	
Outflow	=	10.95 cfs @ 12.33	hrs, Volume=	1.242 af, Atten= 0%,	Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Reach P-CP: Control Point -Stream at PL

Inflow Are	a =	7.748 ac, Inflow Depth > 2.29"	for 10-Year event
Inflow	=	10.45 cfs @ 12.29 hrs, Volume=	1.477 af
Outflow	=	10.45 cfs @ 12.29 hrs, Volume=	1.477 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Pond DB1: Detention Basin #1

Inflow Area =	0.615 ac, Inflow Depth > 3.24"	for 10-Year event
Inflow =	1.98 cfs @ 12.14 hrs, Volume=	0.166 af
Outflow =	0.76 cfs @ 12.45 hrs, Volume=	0.139 af, Atten= 62%, Lag= 18.5 min
Primary =	0.76 cfs @ 12.45 hrs, Volume=	0.139 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 93.70' @ 12.45 hrs Surf.Area= 2,406 sf Storage= 2,913 cf

Plug-Flow detention time= 131.5 min calculated for 0.139 af (83% of inflow) Center-of-Mass det. time= 66.0 min (867.3 - 801.3)

Volume	Inve	rt Avail.Sto	rage Storag	ge Description		
#1	92.2	0' 5,1	03 cf Custor	om Stage Data (Prismatic) Listed below (Recalc)		
Elevetic		Curf Area	Ino Store	Cum Store		
Elevatio		Surf.Area	Inc.Store	Cum.Store		
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)		
92.2	20	1,553	0	0		
92.8	30	1,824	1,013	1,013		
93.0	00	1,953	378	1,391		
94.0	00	2,602	2,278	3,668		
94.5		3,136	1,435	5,103		
		-,	.,	-,		
Device	Routing	Invert	Outlet Devic	ces		
#1	Primary	94.25'	6.0' long x	1.0' breadth Broad-Crested Rectangular Weir		
	,			0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00		
			2.50 3.00			
				ish) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31		
			3.30 3.31 3			
#0	Drimory	00 10				
#2	Primary	92.10'		0' long Culvert CMP, projecting, no headwall, Ke= 0.900		
				rt= 91.73' S= 0.0051 '/' Cc= 0.900		
				Concrete pipe, straight & clean		
#3	Device 2	92.80'	6.0" Vert. O	Drifice/Grate C= 0.600		

Primary OutFlow Max=0.76 cfs @ 12.45 hrs HW=93.70' (Free Discharge)

-1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

-2=Culvert (Passes 0.76 cfs of 3.13 cfs potential flow)

1-3=Orifice/Grate (Orifice Controls 0.76 cfs @ 3.88 fps)

Pond DB2: Detention Basin #2

Inflow Area	=	2.123 ac, Inflow Depth > 2.86"	for 10-Year event
Inflow	=	6.72 cfs @ 12.08 hrs, Volume=	0.507 af
Outflow	=	1.59 cfs @ 12.50 hrs, Volume=	0.469 af, Atten= 76%, Lag= 24.8 min
Primary	=	1.59 cfs @ 12.50 hrs, Volume=	0.469 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 91.19' @ 12.50 hrs Surf.Area= 5,454 sf Storage= 9,037 cf

Plug-Flow detention time= 136.1 min calculated for 0.469 af (93% of inflow)

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Avail.Storage Storage Description Volume Invert #1 89.00' 17,722 cf Custom Stage Data (Prismatic) Listed below (Recalc) Elevation Surf.Area Inc.Store Cum.Store (feet) (cubic-feet) (cubic-feet) (sq-ft) 3.003 89.00 0 0 3.981 3.492 3.492 90.00 91.00 5,124 4,553 8.045 92.00 6,884 6,004 14,049 92.25 7.500 1.798 15.847 92.50 7,500 1.875 17.722 Device Routing Invert **Outlet Devices** 12.0" x 10.0' long Culvert CPP, square edge headwall, Ke= 0.500 #1 Primary 88.90' Outlet Invert= 88.75' S= 0.0150 '/' Cc= 0.900 n= 0.012 #2 Device 1 89.00' **3.0" Vert. Orifice/Grate** C= 0.600 #3 Device 1 89.95' **7.0" Vert. Orifice/Grate** C= 0.600 #4 Primary 92.20' 6.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Center-of-Mass det. time= 97.7 min (904.1 - 806.4)

Primary OutFlow Max=1.59 cfs @ 12.50 hrs HW=91.19' (Free Discharge)

-1=Culvert (Passes 1.59 cfs of 5.06 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.34 cfs @ 6.91 fps)

L-3=Orifice/Grate (Orifice Controls 1.25 cfs @ 4.68 fps)

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	00-24.00 hrs, dt=0.00 y SCS TR-20 method Trans method - Po	d, UH=SCS	-Ind method
Subcatchment E-1: Existing Conditions	Flow Length≕570' Tc		,494 sf Runoff Depth>3.59" Runoff=20.77 cfs 2.320 af
Subcatchment P-1: West Area	Flow Length=351' To		,209 sf Runoff Depth>3.80" Runoff=15.14 cfs 1.587 af
Subcatchment P-2: Central east area			,669 sf Runoff Depth>3.81" 6 Runoff=0.89 cfs 0.063 af
Subcatchment P-3: Northeast Area	Flow Length=330' T		,786 sf Runoff Depth>5.21" 9 Runoff=3.11 cfs 0.267 af
Subcatchment P-4: East area to infiltration			,343 sf Runoff Depth>4.34" 1 Runoff=1.72 cfs 0.127 af
Subcatchment P-5: Central east area to			,113 sf Runoff Depth>4.77" 5 Runoff≕1.11 cfs 0.083 af
Subcatchment P-6: South Area to DB2	Flow Length=285'		,259 sf Runoff Depth>4.13" 9 Runoff≕2.60 cfs 0.176 af
Subcatchment P-7: South Central area to			,711 sf Runoff Depth>5.67" 3 Runoff=1.49 cfs 0.127 af
Subcatchment P-8: South Central area to			,404 sf Runoff Depth>5.44" 1 Runoff=3.52 cfs 0.265 af
Reach E-CP: Control Point-Stream at PL			Inflow=20.77 cfs 2.320 af Outflow=20.77 cfs 2.320 af
Reach P-CP: Control Point -Stream at Pl	-		Inflow=18.20 cfs 2.609 af Outflow=18.20 cfs 2.609 af
Pond DB1: Detention Basin #1	Peak Elev=94.2	25' Storage=4,363	cf Inflow=3.11 cfs 0.267 af Outflow=1.04 cfs 0.239 af
Pond DB2: Detention Basin #2	Peak Elev=92.19	' Storage=15,401 c	f Inflow=10.99 cfs 0.841 af Outflow=2.21 cfs 0.783 af
Total Runoff Area = 15.49	6 ac Runoff Volum	e = 5.015 af Ave	rage Runoff Depth = 3.88"

88.65% Pervious Area = 13.736 ac 11.35% Impervious Area = 1.759 ac

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Subcatchment E-1: Existing Conditions

Runoff = 20.77 cfs @ 12.32 hrs, Volume= 2.320 af, Depth> 3.59"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"

 A	rea (sf)	CN I	Description		·				
	96,180	78 \	78 Wetlands						
	92,521	74 >	74 >75% Grass cover, Good, HSG C						
	5,881								
 **********	42,912	70 \	<u>Noods, Go</u>	od, HSG C					
	37,494		Neighted A						
3	31,613	-	Pervious A	+ + + +					
	5,881	1	mpervious	Area					
Тс	Length	Slope	Velocity	Capacity	Description				
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	-				
6.7	60	0.0200	0.15		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.00"				
4.8	280	0.0375	0.97		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
11.6	230	0.0174	0.33		Shallow Concentrated Flow,				
 					Forest w/Heavy Litter Kv= 2.5 fps				
23.1	570	Total							

23.1 570 Total

Subcatchment P-1: West Area

Runoff = 15.14 cfs @ 12.27 hrs, Volume= 1.587 af, Depth> 3.80"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"

 Area (sf)	CN	Description					
 96,180	78	Wetlands					
23,514	74	>75% Grass cover, Good, HSG C					
13,949	98	Paved parking & roofs					
 84,566	70	Woods, Good, HSG C					
 218,209	76	Weighted Average					
204,260		Pervious Area					
13,949		Impervious Area					

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Type III 24-hr 100-Year Rainfall=6.50" Page 21

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	8.4	89	0.0250	0.18		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	1.5	62	0.0200	0.71		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	9.9	200	0.0180	0.34		Shallow Concentrated Flow,
-						Forest w/Heavy Litter Kv= 2.5 fps
	19.8	351	Total			

Subcatchment P-2: Central east area

Runoff	=	0.89 cfs @	12.08 hrs,	Volume=	0.063 af, Depth> 3.81"
--------	---	------------	------------	---------	------------------------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"

A	rea (sf)	CN	Description				
	7,924	74	>75% Gras	s cover, Go	bod, HSG C		
	745	98	Paved park	ing & roofs			
	8,669	76	Weighted Average				
	7,924		Pervious Area				
	745		Impervious	Area			
Тс	Length	Slope	e Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)			
5.0					Direct Entry,		

Subcatchment P-3: Northeast Area

Runoff = 3.11 cfs @ 12.14 hrs, Volume= 0.267 af, Depth> 5.21"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"

Area (sf)	CN	Description					
11,211	79	50-75% Grass cover, Fair, HSG C					
4,511	100	Det Basin					
9,302	98	Paved parking & roofs					
1,762	70	Woods, Good, HSG C					
26,786	89	Weighted Average					
12,973		Pervious Area					
13,813		Impervious Area					

Prepare	d by The	e Berksh	sing-Act ire Design 2 © 2006 I	n Group	Type III 24-hr 100-Year Rainfall=6.50" Page 22 Software Solutions LLC 11/12/2008		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
8.6	100	0.0300	0.19		Sheet Flow,		
1.4	230	0.0330	2.72		Grass: Short n= 0.150 P2= 3.00" Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps		
10.0	330	Total					
	Subcatchment P-4: East area to infiltration trench						
Runoff	=	1.72 cfs	s@ 12.1	0 hrs, Volu	ime= 0.127 af, Depth> 4.34"		
			nod, UH=S ainfall=6.50		Span= 0.00-24.00 hrs, dt= 0.05 hrs		
A	rea (sf)	CN D	escription				
	3,068			•	bod, HSG C		
	5,529 6,746			ing & roofs od, HSG C			
	15,343 9,814 5,529	81 V P	Veighted A Pervious Ar mpervious	verage ea			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
5.8	100	0.0800	0.29		Sheet Flow,		
0.2	20	0.0180	2.01		Grass: Short n= 0.150 P2= 3.00" Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps		
0.4	60	0.0167	2.62		Shallow Concentrated Flow, Paved Kv= 20.3 fps		
6.4	180	Total					
			Subcatc	hment P-	5: Central east area to DB2		
Runoff	. =	1.11 cfs	s@ 12.0	9 hrs, Volu	me= 0.083 af, Depth> 4.77"		
	Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"						

Area (sf	<u> </u>	Description				
2,758	3 74	4 >75% Grass cover, Good, HSG C				
4,623	3 98	Paved parking & roofs				
1,732	2 70	0 Woods, Good, HSG C				
9,113		Weighted Average				
4,490		Pervious Area				
4,623	3	Impervious Area				

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	5.8	100	0.0800	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	0.1	10	0.0167	1.94		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
	0.4	66	0.0167	2.62		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
_	6.2	176	Total			

6.3 176 Total

Subcatchment P-6: South Area to DB2

Runoff = 2.60 cfs @ 12.06 hrs, Volume= 0.176 af, Depth> 4.13"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"

	A	rea (sf)	CN I	Description								
-		10,347	74 :	>75% Gras	s cover, Go	bod, HSG C						
		5,500	98 I	Paved parking & roofs								
		1,024		>75% Grass cover, Good, HSG C								
		5,388	70	Woods, Good, HSG C								
		22,259	79	Neighted A	verage							
		16,759		Pervious Ar								
		5,500		mpervious	Area							
	_		~		• •							
	Tc	Length	Slope		Capacity	Description						
	(min)	(feet)	(ft/ft)	······	(cfs)							
	0.9	80	0.0330	1.56		Sheet Flow,						
						Smooth surfaces $n= 0.011 P2= 3.00"$						
	1.5	20	0.1000	0.23		Sheet Flow,						
						Grass: Short n= 0.150 P2= 3.00"						
	1.5	185	0.0200	2.12		Shallow Concentrated Flow,						
_						Grassed Waterway Kv= 15.0 fps						
_	3.9	285	Total									

Subcatchment P-7: South Central area to DB2

Runoff = 1.49 cfs @ 12.12 hrs, Volume= 0.127 af, Depth> 5.67"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"

Area (sf)	CN	Description
2,278	74	>75% Grass cover, Good, HSG C
9,433	98	Paved parking & roofs
11,711	93	Weighted Average
2,278		Pervious Area
9,433		Impervious Area

Northern Avenue Housing-Active Prepared by The Berkshire Design Group					<i>Type III 24-hr 100-Year Rainfall=6.50"</i> Page 24	
					Software Solutions LLC 11/12/2008	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
8.6	100	0.0300	0.19		Sheet Flow,	
0.2	33	0.0250	3.21		Grass: Short n= 0.150 P2= 3.00" Shallow Concentrated Flow, Paved Kv= 20.3 fps	
8.8	133	Total				
Type III 2	Subcatchment P-8: South Central area to DB2 Runoff = 3.52 cfs @ 12.07 hrs, Volume= 0.265 af, Depth> 5.44" Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.50"					
A	rea (sf)		Description			
	8,246				ood, HSG C	
	7,521			ing & roofs		
	8,135 100 Det Basin					
<u> </u>	1,502		Rain Garde			
	25,404		Veighted A			
	8,246		Pervious Ar			
	17,158	Į	mpervious	Area		
То	To Longth Slope Velocity Canacity Description					

Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	· · · · · · · · · · · · · · · · · · ·

5.0

Direct Entry,

Reach E-CP: Control Point-Stream at PL

Inflow Are	ea =	7.748 ac, Inflow Depth > 3 .	59" for 100-Year event
Inflow	=	20.77 cfs @ 12.32 hrs, Volum	ne= 2.320 af
Outflow	=	20.77 cfs @ 12.32 hrs, Volun	ne= 2.320 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Reach P-CP: Control Point -Stream at PL

Inflow Area =	7.748 ac, Inflow Depth > 4.04 "	for 100-Year event
Inflow =	18.20 cfs @ 12.28 hrs, Volume=	2.609 af
Outflow =	18.20 cfs @ 12.28 hrs, Volume=	2.609 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Pond DB1: Detention Basin #1

Inflow Area =	0.615 ac, Inflow Depth > 5.21"	for 100-Year event
Inflow =	3.11 cfs @ 12.14 hrs, Volume=	0.267 af
Outflow =	1.04 cfs @ 12.49 hrs, Volume=	0.239 af, Atten= 66%, Lag= 21.1 min
Primary =	1.04 cfs @ 12.49 hrs, Volume=	0.239 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 94.25' @ 12.48 hrs Surf.Area= 2,873 sf Storage= 4,363 cf

Plug-Flow detention time= 112.6 min calculated for 0.239 af (90% of inflow) Center-of-Mass det. time= 63.1 min (851.5 - 788.4)

Volume	Inve	ert Avail.Sto	rage Storage	e Description			
#1	92.2	0' 5,1	03 cf Custor	3 cf Custom Stage Data (Prismatic) Listed below (Recalc)			
–) <i>(</i>)		0 ()					
Elevatio		Surf.Area	Inc.Store	Cum.Store			
(fee	<u>et)</u>	(sq-ft)	(cubic-feet)	(cubic-feet)			
92.2	20	1,553	0	0			
92.8	30	1,824	1,013	1,013			
93.0	00	1,953	378	1,391			
94.(00	2,602	2,278	3,668			
94.5	50	3,136	1,435	5,103			
		,	,	-,			
Device	Routing	Invert	Outlet Devic	es			
#1	Primary	94.25'	6.0' long x	1.0' breadth Broad-Crested Rectangular We	eir		
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00				
			2.50 3.00				
			Coef. (Englis	Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31			
			3.30 3.31 3.32				
#2	Primary	92.10'		long Culvert CMP, projecting, no headwal	ll. Ke= 0.900		
	,,		Outlet Invert= $91.73'$ S= $0.0051 '/$ Cc= 0.900				
			n = 0.011 Concrete pipe, straight & clean				
#3 Device 2 92.80'			rifice/Grate C= 0.600				
	201100 2	02.00					
Drimany	Primary OutFlow Max-1 04 cfs @ 12.40 brs HW-04.25' (Free Discharge)						

Primary OutFlow Max=1.04 cfs @ 12.49 hrs HW=94.25' (Free Discharge) -1=Broad-Crested Rectangular Weir (Weir Controls 0.00 cfs @ 0.14 fps) -2=Culvert (Passes 1.04 cfs of 3.84 cfs potential flow) -3=Orifice/Grate (Orifice Controls 1.04 cfs @ 5.28 fps)

Pond DB2: Detention Basin #2

Inflow Are	ea =	2.123 ac, Inflow Depth > 4.75"	for 100-Year event
Inflow	=	10.99 cfs @ 12.08 hrs, Volume=	0.841 af
Outflow	=	2.21 cfs @ 12.52 hrs, Volume=	0.783 af, Atten= 80%, Lag= 26.6 min
Primary	=	2.21 cfs @ 12.52 hrs, Volume=	0.783 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 92.19' @ 12.52 hrs Surf.Area= 7,352 sf Storage= 15,401 cf

Plug-Flow detention time= 123.6 min calculated for 0.783 af (93% of inflow)

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Type III 24-hr 100-Year Rainfall=6.50" Page 26 11/12/2008

Center-of-Mass det. time= 87.4 min (880.9 - 793.5)

Volume	Inver	t Avail.Stor	rage Storage	Description		
#1	89.00)' 17,72	22 cf Custom	n Stage Data (Prismatic) Listed below (Recalc)		
Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
89.0		3,003	0	0		
90.0	00	3,981	3,492	3,492		
91.0	00	5,124	4,553	8,045		
92.0	00	6,884	6,004	14,049		
92.2	25	7,500	1,798	15,847		
92.5	50	7,500	1,875	17,722		
Device	Routing	Invert	Outlet Device	es		
#1	Primary	88.90'		long Culvert CPP, square edge headwall, Ke= 0.500		
				= 88.75' S= 0.0150 '/' Cc= 0.900 n= 0.012		
#2	Device 1	89.00'		ifice/Grate $C=0.600$		
#3	Device 1	89.95'		ifice/Grate $C= 0.600$		
#4	Primary	92.20'	~	.0' breadth Broad-Crested Rectangular Weir		
			· · ·	0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00		
			2.50 3.00			
				h) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31		
			3.30 3.31 3.3	32		
Primary OutFlow Max=2.21 cfs @ 12.52 hrs HW=92.19' (Free Discharge)						

Primary OutFlow Max=2.21 cfs @ 12.52 hrs HW=92.19' (Free Discharge)

-2=Orifice/Grate (Orifice Controls 0.41 cfs @ 8.43 fps)

-3=Orifice/Grate (Orifice Controls 1.80 cfs @ 6.72 fps)

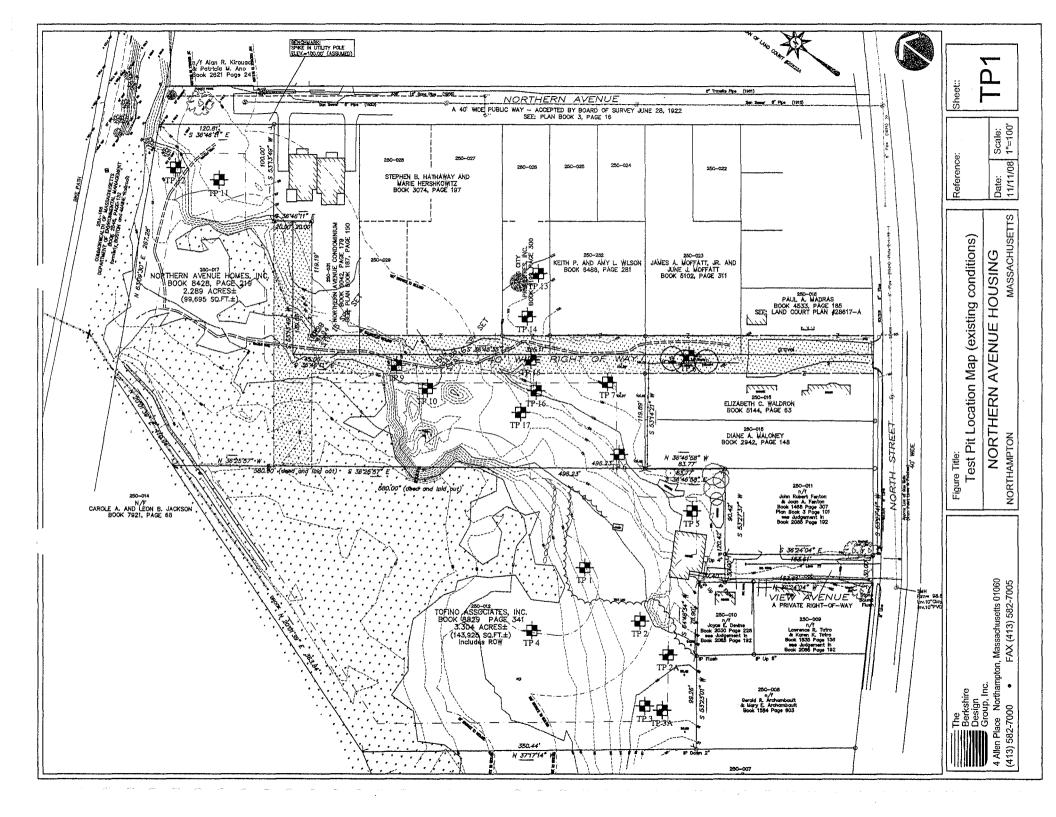
-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

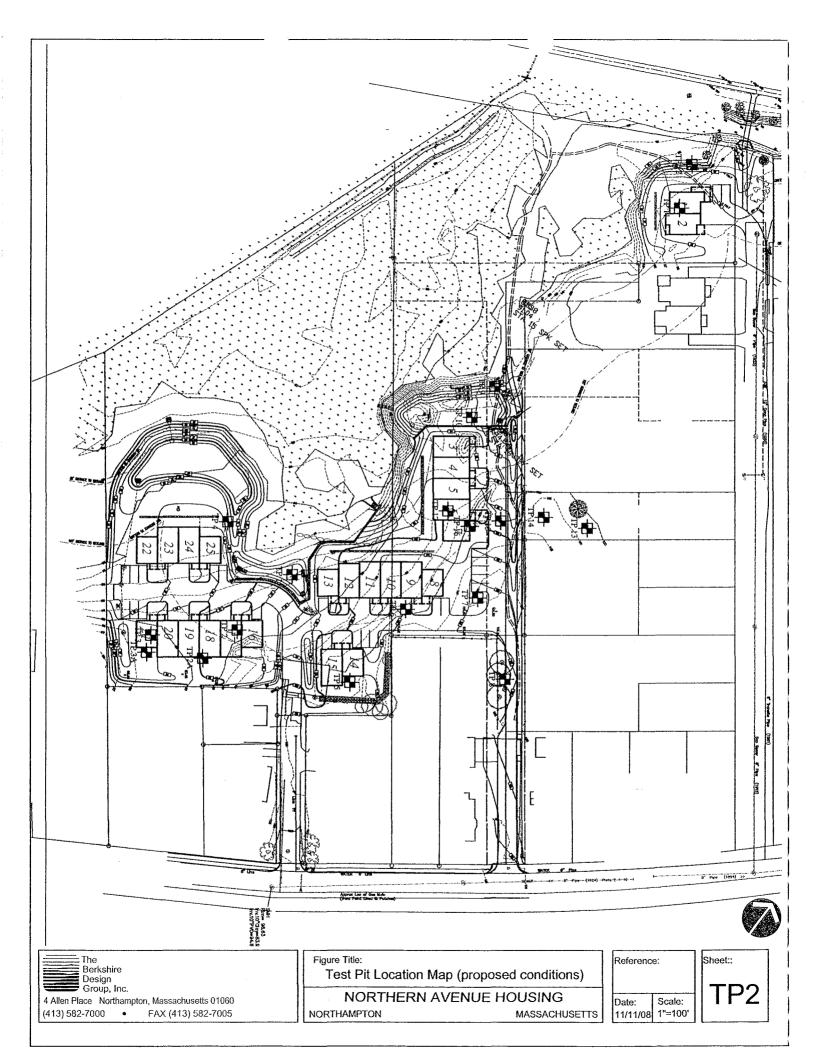
Northampton, Massachusetts

Stormwater Drainage Report Appendix

Appendix B – Soil Test Pit Information

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	Test	Pits					
Performed By M.D'Urso, The Berkshire	Design Gro	oup V	Vitnesse	ed By:			
Deep Hole Number TP 1	Date: 01/0	5/07 T	īme:	9:15am	Weather	Clear 10	F
Location (identify on site plan) _ See Plan	n						
Land Use Lawn Area	_ Slope (%)	See I	Plan	Surface	e Stones	n/o	
Vegetation grass & some trees							
Landform							
Position on Landscape (sketch on back)				<u></u>		·····	
Distances from: See Plan	-	1	During				m .,
Open Water Body Possible Wet Area		eet eet	Draina				Feet
Drinking Water Well		eet	Propert Other	Line			Feet

DEEP OBSERVATION HOLE LOG *							
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)		
0-9"	A	VFSL	10YR3/3	5Y 4/6 <5%	Massive, Friable, roots		
9"-21"	B _w	VFSL	2.5Y4/4	5YR4/6 >10% @18"	Massive, Friable		
21"-53"	C ₁	VFSL/ Loam	5Y5/2	5YR4/6 >35%	Massive, friable, stratified FS & Loam, some smearing, somewhat firm		
53"-80"	C ₂	SL	10YR4/4	2.5YR3/6 >35% throughout	Massive, friable, sloughing		

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) glaciolacustrine		Depth to Bedrock:	> 80"	
Depth to Groundwater: Standing Water in the Hole:	57" @ 15 minutes	Weeping from	m Pit Face:	55"
Estimated Seasonal High Ground Water: 18"				

Percolation Test:

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

Performed By M.D'Urso, The Berksh	ire Design Grou	p Witness	sed By:		
Deep Hole Number TP 2	Date: 01/05/	07 Time:	9:40am	Weather	Clear 10 F
Location (identify on site plan)See F	Plan				
Land Use Wooded	Slope (%)	See Plan	Surfac	e Stones	n/o
Vegetation Norway Spruce				m.,	
Landform					
Position on Landscape (sketch on bac	k)				
Distances from: See Plan					
Open Water Body	Fee	et Draina	age way		Feet
Possible Wet Area	Fee	et Prope	erty Line		Feet
Drinking Water Well	Fee	t Other	·		

	DEEP OBSERVATION HOLE LOG *							
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)			
0-12"	A	VFSL	10YR3/3	5Y 4/6 <5%	Massive, Friable, some roots, apparent fill at south end of TP down to 36"			
12"-19"	B _w	VFSL	2.5Y4/4	5YR4/6 >10% @18"	Massive, Friable			
19"-45"	C ₁	VFSL/ Loam	5Y5/2	5YR4/6 >35%	Massive, friable, some smearing, somewhat firm, excavation collapsed			

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) glaciolacustrine		Depth to Bedrock:	> 45"
Depth to Groundwater: Standing Water in the Hole:	40"	Weeping fro	m Pit Face:

Estimated Seasonal High Ground Water: 18"

Percolation Test:

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

	<u> </u>	est Pit	S				
Performed By M.D'Urso, The Berk	shire Desig	n Group	Witness	sed By:			
Deep Hole Number TP 2A	Date:	10/31/07	Time:	9:00am	Weather	P-Cloudy	/ 40 F
Location (identify on site plan)	Plan						
Land Use Wooded	Slop	e (%) <u>Se</u>	e Plan	Surfac	e Stones	n/o	
Vegetation Norway Spruce							
Landform							
Position on Landscape (sketch on ba	ack)						
Distances from: See Plan							
Open Water Body		Feet	Draina	age way			Feet
Possible Wet Area		Feet	Prope	rty Line			Feet
Drinking Water Well		Feet	Other				

	DEEP OBSERVATION HOLE LOG *							
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)			
0-10"	A	VFSL	10YR3/3	5Y 4/6 <5%	Massive, Friable, some roots			
10"-30"	B _w	VFSL	2.5Y4/4	5YR4/6 >10% @22"	Massive, Friable, roots to 21"			
30"-70"	C ₁	VFSL/ Loam	5Y5/2	5YR4/6 >35%	Massive, friable, some smearing, somewhat firm, excavation collapsed, fine sand in lower 12"			

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) glaciolacustrine	Depth to Bedrock: > 70"
Depth to Groundwater: Standing Water in the Hole:66" @ 10 minutes	Weeping from Pit Face: 66" (rapid)
Estimated Seasonal High Ground Water: 22"	

Percolation Test: Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

	-	Test Pit					
Performed By M.D'Urso, The Berk	shire Desi	gn Group	Witness	sed By:			
Deep Hole Number TP 3	Date:	01/05/07	Time:	10:10am	Weather	Clear 10 F	•
Location (identify on site plan) _See	e Plan						
Land Use Wooded	Slo	pe (%) <u>Se</u>	e Plan	Surface	e Stones	n/o	
Vegetation Norway Spruce							
Landform						<u> </u>	
Position on Landscape (sketch on b	ack)					<u></u>	
Distances from: See Plan							
Open Water Body		Feet	Draina	age way		F	eet
Possible Wet Area		Feet	Prope	rty Line		F	eet
Drinking Water Well		Feet	Other		•		

	DEEP OBSERVATION HOLE LOG *							
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)			
0-9"	A	VFSL	10YR3/3		Massive, Friable, roots			
9"-15"	B _w	VFSL	2.5Y4/4		Massive, Friable, roots			
15"-50"	C ₁	VFSL/ Loam	5Y5/2	5YR4/6 >15% @ 20"	Massive, friable, sloughing, stratified FSL & Fine Sand			
50"-65"	C ₂	Fine Sand	10YR4/4	2.5YR3/6 >35% throughout	Massive, friable, sloughing			

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) glaciolacustrine	Depth to Bedrock: > 65"
Depth to Groundwater: Standing Water in the Hole:61"	Weeping from Pit Face: 55"
Estimated Seasonal High Ground Water: 20"	
Percolation Test:	

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

	Test Pit	S		
Performed By M.D'Urso, The Berkshire	e Design Group	Witnessed By:		
Deep Hole Number TP 3A D	Date: 10/31/08	Time: 9:30am	Weather	Clear 10 F
Location (identify on site plan) _ See Plan	n			
Land Use _ Wooded	_ Slope (%) _Se	e Plan Surfac	ce Stones	n/o
Vegetation Norway Spruce		· · · · · · · · · · · · · · · · · · ·		
Landform			····	
Position on Landscape (sketch on back)	<u> </u>			
Distances from: See Plan	_			
Open Water Body	Feet	Drainage way		Feet
Possible Wet Area	Feet	Property Line		Feet
Drinking Water Well	Feet	Other		
DEEP OB	SERVATION	NHOLELOG *	······································	

Depth from	Soil Horizon	Soil Texture	Soil Color	Soil Mottling	Other (Structure Stance Bouldon
Surface(Inches)	HUNZUN	(USDA)	(Munsell)		(Structure, Stones, Boulders, Consistency, % Gravel)
0-7"	A	VFSL	10YR3/3		Massive, Friable, roots
7"-15"	Bw	VFSL	2.5Y4/4		Massive, Friable, roots
15"-70"	C ₁	VFSL/ Loam	5Y5/2	5YR4/6 >15% @ 30"	Massive, friable, roots down to 20", sloughing, stratified FSL & Fine Sand, fine sand at pit bottom, excavation collapsed

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) _glaciolacustrir	ne		Depth to Bedrock: > 70"	
Depth to Groundwater: Standing Water in t	he Hole:	67" @ 5 minutes	Weeping from Pit Face:	64" (moderate)
Estimated Seasonal High Ground Water:	30"			

Percolation Test:

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

	<u>Test Pi</u>	ts		
Performed By M.D'Urso, The Berk	shire Design Group	Witnessed By:		
Deep Hole Number TP 4	Date: 01/05/07	Time: 4:00pm	Weather	Cloudy 10 F
Location (identify on site plan) _ See	e Plan			· · · · · · · · · · · · · · · · · · ·
Land Use Wooded	Slope (%)S	See Plan Surface	Stones	<u>n/o</u>
Vegetation Norway Spruce				
Landform				
Position on Landscape (sketch on ba	ack)	· ···		
Distances from: See Plan				
Open Water Body	Feet	Drainage way		Feet
Possible Wet Area	Feet	Property Line		Feet
Drinking Water Well	Feet	Other		
				· · · · · · · · · · · · · · · · · · ·
DEEP	OBSERVATIO	N HOLE LOG *		

Depth from	Soil Horizon	Soil Texture (USDA)	Soil Color	Soil Mottling	Other (Structure, Stones, Boulders,
Surface(Inches)	HUIIZUII		(Munsell)		Consistency, % Gravel)
0-5"	A	VFSL	10YR3/3	5Y 4/6 <5%	Massive, Friable, roots
5"-15"	B _w	VFSL	2.5Y4/4	5YR4/6 <5% @18"	Massive, Friable, Roots down to 18"
15"-65"	C ₁	FSL	5Y5/2	5YR4/6 >10% @28"	Massive, friable, stratified FSL & Fine Sand, some smearing, somewhat firm

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

 Parent Material (geologic)
 glaciolacustrine
 Depth to Bedrock:
 > 65"

 Depth to Groundwater:
 Standing Water in the Hole:
 51"
 Weeping from Pit Face:
 48"

 Estimated Seasonal High Ground Water:
 28"
 28"
 28"

Percolation Test:

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

	1	Test Pit.	5				
Performed By M.D'Urso, The Be	erkshire Desig	n Group	Witness	ed By:			
Deep Hole Number TP 5	Date:	01/05/07	Time:	3:00pm	Weather	Clear 1	0 F
Location (identify on site plan)	See Plan						
Land Use Lawn Area	Slop	e (%) <u>Se</u>	e Plan	Surfac	e Stones	n/o	
Vegetation grass					<u></u>	<u> </u>	
Landform							
Position on Landscape (sketch or	n back)						
Distances from: See Plan							
Open Water Body		Feet	Draina	age way			Feet
Possible Wet Area		Feet	Prope	rty Line			Feet
Drinking Water Well		Feet	Other				

		DEEP C	DBSERVA	TION HOLE I	_OG *
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-9"	A	VFSL	10YR3/3		Massive, Friable, roots
9"-21"	B _w	VFSL	2.5Y4/4		Massive, Friable
21"-107"	C ₁	VFSL/ Loam	5Y5/2	5YR4/6 >10% @60"	Massive, friable, no cobbles or gravel, stratified VFSL & Fine Sand, some smearing,

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) glaciolacustrine	·····	Depth to Bedrock: > 107"	
Depth to Groundwater: Standing Water in the Hole:	92"	Weeping from Pit Face: 92"	
Estimated Seasonal High Ground Water: 60"			

Percolation Test:

Depth to Perc:	45"	
Start Pre-Soak	12":	3:14
End Pre-Soak	12":	3:36 (8 gals used)
Time at 12":		3:36
Time at 9":		3:42
Time at 6":		4:00
Time (9"-6"):		18 minutes
Rate:		6 min/inch

Drinking Water Well

	<u>Test Pi</u>	ts		
Performed By M.D'Urso, The Berkshire	e Design Group	Witnessed By:		
Deep Hole Number TP 6	Date: 01/05/07	Time: 11:10am	Weather	Clear 10 F
Location (identify on site plan) See Pla	n			
Land Use Wooded	_ Slope (%) _S	ee Plan Surfac	e Stones	n/o
Vegetation Mixed deciduous and everg	green			
Landform				
Position on Landscape (sketch on back)				
Distances from: See Plan				
Open Water Body	Feet	Drainage way		Feet
Possible Wet Area	Feet	Property Line		Feet

Feet

Other

DEEP OBSERVATION HOLE LOG * Depth from Soil Soil Texture Soil Color Soil Mottling Other Surface(Inches) (USDA) (Structure, Stones, Boulders, Horizon (Munsell) Consistency, % Gravel) 0-8" 10YR3/3 Α Forest Massive, Friable, roots Mat 8"-29" VFSL 2.5Y4/4 Massive, Friable Bw 29"-88" FSL 5YR4/6 Distinct C_1 5Y5/2 Massive, friable, stratified FSL and Fine Sand, roots throughout, >5% @38" sloughing

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) _ G	aciolacustrine		Depth to Bedrock:	> 88"	
Depth to Groundwater: Standing	ng Water in the Hole:	79"	Weeping from	n Pit Face:	67" (slow)
Estimated Seasonal High Grou	und Water: 38"				

Percolation Test: Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

	<u>Test Pit</u>	<u>'S</u>		
Performed By M.D'Urso, The Berkshire	Design Group	Witnessed By:		
Deep Hole Number TP 7	Date: 01/05/07	Time: 11:45am	Weather	Clear 10 F
Location (identify on site plan) See Plan	n			
Land Use Wooded	_ Slope (%) _Se	e Plan Surfac	e Stones	n/o
Vegetation Mixed deciduous and everg	reen			
Landform				
Position on Landscape (sketch on back)				
Distances from: See Plan				
Open Water Body	Feet	Drainage way		Feet
Possible Wet Area	Feet	Property Line		Feet
Drinking Water Well	Feet	Other _		

DEEP OBSERVATION HOLE LOG *						
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)	
0-8"	A	Forest Mat	10YR3/3		Massive, Friable, roots	
8"-19"	B _w	VFSL	2.5Y4/4		Massive, Friable	
19"-90"	C ₁	FSL	2.5Y5/3	5YR4/6 Distinct >5% @58"	Massive, friable, stratified FSL and Fine Sand, roots down to 31", sloughing	

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic)Glaciolacustrine		Depth to Bedrock: > 90"	
Depth to Groundwater: Standing Water in the Hol	:84"	Weeping from Pit Face:	
Estimated Seasonal High Ground Water: 58"			

Percolation Test:

Depth to Perc:	46"	
Start Pre-Soak	12":	12:18
End Pre-Soak	12":	12:33 (18 gals used)
Time at 12":		12:33
Time at 9":		12:36
Time at 6":		12:41
Time (9"-6"):		5 minutes
Rate:		< 2 min/inch

			<u>Tes</u>	<u>st Pits</u>		
Performed By	M.D'Urs		-	roup Witnessed	By:	
Deep Hole Nu	mber T	28	Date: 01/	05/07 Time: 1	:45pm Weather	P-cloudy 10 F
Location (iden	ntify on site	plan) See	Plan			
Land Use _O	ld roadway	/	Slope (%	6) See Plan	Surface Stones	n/o
Vegetation	Mixed deci	duous and ev	ergreen		-	
Landform						
						· · · · · · · · · · · · · · · · · · ·
Distances from			<u></u>			
•	n Water Bo	ody		Feet Drainage	way	Feet
	sible Wet A	rea		Feet Property	Line	Feet
Drini	king Water			Feet Other	·	······
		DEEP (DBSERV	TION HOLE L	.OG *	
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Othe (Structure, Ston	
		(00001)			Consistency,	% Gravel)
0-15"	Fill				Roadway bed, sti fill/C1 interface	
					colo	
15"-95"	C ₁	VFSL	2.5Y4/4	5YR4/6 Distinct	Massive, Friable	
				>5% @60"	and Fine	Sand
				600		
*1000000						
	2 HOLES F	REQUIRED AT	EVERY PROP	OSED DISPOSAL AR	EΑ	
Parent Material (g	eologic) <u>G</u>	alaciolacustrine		Depth	to Bedrock: > 108"	
Depth to Groundw	vater: Standi	ng Water in the H	lole: <u>90"</u>		Weeping from Pit Face	e:69" (slow)
Estimated Seasor	nal High Grou	ind Water: 60	n		·····	
Percolation Te	ct.					
Depth to Perc:				Note: Th	us test pit was	performed for
Start Pre-Soak	12":	2:10		investigat	ion of general soil	conditions and
End Pre-Soak		2:25 (10 gals u	sed)		ot be used for purp	
Time at 12": Time at 9":		2:25 2:30			d/or soil suitability wage disposal.	assessments for
Time at 6":		2:36				<u></u>
Time (9"-6"):		6 minutes				
Rate:		2 min/inch				

Performed By M.D'Urso, The Berkshire Design Group Witnessed By:	
Deep Hole Number TP 9 Date: 01/05/07 Time: 1:20pm Weather P-cloud	/ 10 F
Location (identify on site plan) See Plan	
Land Use Old roadway Slope (%) See Plan Surface Stones n/o	
Vegetation Mixed deciduous and evergreen	
Landform	
Position on Landscape (sketch on back)	
Distances from: See Plan	
Open Water Body Feet Drainage way	Feet
Possible Wet Area Feet Property Line	Feet
Drinking Water Well Feet Other	

DEEP OBSERVATION HOLE LOG *						
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)	
0-42"	Fill				Silty sand, debris, concrete, brick	

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic)	Depth to Bedrock: > 42"
Depth to Groundwater: Standing Water in the Hole: 36"	Weeping from Pit Face:
Estimated Seasonal High Ground Water: 36"	

Percolation Test: Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

٢

	, 	<u>Test Pit</u>	S				
Performed By M.D'Urso, The Berk	shire Desi	gn Group	Witness	sed By:			
Deep Hole Number TP 10	Date:	01/05/07	Time:	1:30pm	Weather	P-cloud	y 10 F
Location (identify on site plan) _Se	e Plan			. <u>.</u>			
Land Use wooded	Slo	oe (%) <u>Se</u>	e Plan	Surfac	e Stones	n/o	
Vegetation Mixed deciduous and	evergreen						
Landform							
Position on Landscape (sketch on b	ack)			·····			
Distances from: <i>See Plan</i> Open Water Body Possible Wet Area Drinking Water Well	· · · · · · · · · · · · · · · · · · ·	Feet Feet Feet		age way rty Line			Feet Feet

DEEP OBSERVATION HOLE LOG *							
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)		
0-65"	Fill				Silty sand, debris, concrete, brick		
* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA							
Parent Material (g	eologic)			Dept	th to Bedrock: > 65"		

Depth to Groundwater: Standing Water in the	Hole: 6	0"	Weeping from Pit Face:	58"	
Estimated Seasonal High Ground Water: 58	8"				

Percolation Test: Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

			Test	t Pits				
Performed By			-	•		•		
)6/07	Time:	9:00am	Weather	P-cloudy 10 F
Location (identify on site plan) See Plan								
Land Use w) <u>See</u>	Plan	Surfac	e Stones _	n/o
Vegetation _	Mixed decio	luous and ev	ergreen					
Landform	· · · · · · · · · · · · · · · · · · ·							
Position on La			:k)					
Distances from	n: <i>See Pla</i> n Water Bo		c	Foot	Drainag			Feet
•	sible Wet A	rea	F	Feet	Property	v Line		Feet
Drink	king Water	Well		Feet	Other	·		
		DEEP (DBSERVA	TION	HOLE	LOG *		
	• • • • • • • • •							
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil	Mottling	(S	Othe tructure, Ston	
0-25"	Fill ₁	FSL	Brwn				Consistency, lassive, Fri	% Gravel)
0-23	ГШ <u>1</u>	I OL	DIWII			IV IV	1055176, 1 11	able, 10015
25"-105"	Fill ₂	FSL	Drk. Brwn			10% (cobbles and	d gravel, some
	1							oris @ 100"
* MINIMUM OF	2 HOLES R	EQUIRED AT	EVERY PROPO	OSED DI	SPOSAL A	REA		
Parent Material (g	realogic)				Den	th to Bedroc	:k: > 105"	
Depth to Groundw		o Water in the I	lole: 96"					e: 92" (rapid)
Estimated Seasor								
	-							
Percolation Te Depth to Perc:				:	Note: 7	This test	pit was	performed for
Start Pre-Soak					investiga	tion of g	eneral soil	conditions and
End Pre-Soak	12":							poses related to
Time at 12": Time at 9":						nd/or soll ewage disp	-	assessments for
Time at 6":								
Time (9"-6"): Rate:								
12440.								

7	est Pits	5				
Performed By M.D'Urso, The Berkshire Desig	n Group	Witnesse	d By:			
Deep Hole Number TP 12 Date:	01/06/07	Time:	9:00am	Weather	P-cloud	y 10 F
Location (identify on site plan) See Plan						
Land Use wooded Slop	e (%) <u>Se</u>	e Plan	Surfac	e Stones	n/o	
Vegetation Mixed deciduous and evergreen						
Landform						
Position on Landscape (sketch on back)						
Distances from: See Plan						
Open Water Body	Feet	Drainag	e way			Feet
Possible Wet Area	Feet	Propert	y Line			Feet
Drinking Water Well	Feet	Other				

		DEEP (DBSERVA	TION HOLE L	_OG *
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
0-36"	Fill	FSL	Brwn		Loose, Friable, some stones, asphalt
36"-46"	Ap/Bw	FSL	Drk. Brwn/ Brown		10% cobbles and gravel, some glass and debris @ 100"
46"-64"	C ₁	FSL	5Y5/2	5YR4/6 Distinct >5% @38"	Massive, friable, stratified FSL and Fine Sand, roots throughout, sloughing

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic)		Depth to Bedrock:	> 64"	
Depth to Groundwater: Standing Water in the Hole:	55"	Weeping fro	m Pit Face:	50"
Estimated Seasonal High Ground Water:				

Percolation Test:Depth to Perc:Start Pre-Soak12":End Pre-Soak12":Time at 12":Time at 9":Time at 6":

investigation of general soil conditions and should not be used for purposes related to Title 5 and/or soil suitability assessments for on-site sewage disposal.

Note: This test pit was performed for

Time (9"-6"): Rate:

Test Pits

Performed By M.D'Urso, The Be		Witnessed By:					
Deep Hole Number TP 13	Date: 10/31/07	Time: <u>11:50am</u>	Weather	P-Cloudy 45 F			
Location (identify on site plan) _S	ee Plan						
Land Use Wooded	Slope (%)	e Plan Surfa	e Stones	n/o			
Vegetation Mixed deciduous and evergreen							
Landform							
Position on Landscape (sketch on	back)						
Distances from: See Plan							
Open Water Body	Feet	Drainage way		Feet			
Possible Wet Area	Feet	Property Line		Feet			
Drinking Water Well	Feet	Other					

DEEP OBSERVATION HOLE LOG *								
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)			
0-4"	A	FSL			Topsoil, Grass, roots			
4"-15"	B _w	VFSL	2.5Y4/4		Massive, Friable			
15"-68"	C ₁	LS	2.5Y5/3	5YR4/6 Distinct >5% @54"	Massive, friable, some stratified FSL and Fine Sand, roots down to 24", sloughing			
68"-108"	C ₂	LS	5Y4/2	7.5YR5/6 >10% throughout	Mass, firm, some smearing			
108"-114"	C ₃	SL	5Y4/2	7.5YR5/6 >10% throughout	Mass, firm, smearing, wet, pockets of loam			

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic)	Glaciolacustrine	Depth to Bee	drock: > 114"
Depth to Groundwater: Star	nding Water in the Hole:	Wee	ping from Pit Face:
Estimated Seasonal High G	round Water: 54"		

Percolation Test:

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

Test Pits

Performed By M.D'Urso, The Berksl	nire Desig	gn Group	Witness	sed By:			
Deep Hole Number TP 14	Date:	10/31/07	Time:	10:45am	Weather	P-Cloudy 45	F
Location (identify on site plan) See	Plan			•••			
Land Use Wooded	Slo	pe (%) _S	ee Plan	Surface	e Stones	n/o	
Vegetation Mixed deciduous and ev	ergreen						
Landform							
Position on Landscape (sketch on bac	:k)						
Distances from: See Plan							
Open Water Body		Feet	Draina	age way 🔄		Feet	t
Possible Wet Area		Feet	Prope	rty Line		Fee	t
Drinking Water Well		Feet	Other			· · · · · · · · · · · · · · · · · · ·	

DEEP OBSERVATION HOLE LOG *							
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)		
0-8"	A	Forest Mat	10YR3/3		Massive, Friable, roots		
8"-19"	B _w	VFSL	2.5Y4/4		Massive, Friable		
19"-87"	C ₁	FLS	2.5Y5/3	5YR4/6 Distinct >5% @75"	Massive, friable, some stratified FSL and Fine Sand, roots down to 24", sloughing		
87-112"	C ₂	FLS	5Y4/2	7.5YR5/6 >10% (from excavator bucket)	Mass, firmer than C1, Wet, smearing		

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) Glaciolacustrine		Depth to Bedrock: > 112"	
Depth to Groundwater: Standing Water in the Hole:	n/o	Weeping from Pit Face: _	n/o
Estimated Seasonal High Ground Water: 75"			

Percolation Test:

Depth to Perc:	42"	
Start Pre-Soak	12":	11:01
End Pre-Soak	12":	11:16 (18 gals used)
Time at 12":		11:16
Time at 9":		11:18
Time at 6":		11:21
Time (9"-6"):		3 minutes
Rate:		< 2 min/inch

	Test	<u>Pits</u>			
Performed By M.D'Urso, The Berkshin	re Design Gro	oup Witnes	sed By:		
Deep Hole Number TP 15	Date: 10/3	1/07 Time:	1:00pm	Weather	P-Cloudy 45 F
Location (identify on site plan)See Pl	an				
Land Use Wooded	Slope (%)	See Plan	Surface	e Stones	n/o
Vegetation Mixed deciduous and even	rgreen				
Landform					
Position on Landscape (sketch on back)				
Distances from: <i>See Plan</i> Open Water Body Possible Wet Area Drinking Water Well	F		age way erty Line		Feet

DEEP OBSERVATION HOLE LOG *								
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)			
0-20"	Fill				Massive, Friable, roots			
20"-64"	C ₁	FLS	2.5Y5/3	5YR4/6 Distinct >5% @68"	Massive, friable, some stratified FSL and Fine Sand, roots down to 24", sloughing			
64"-106"	C ₂	FLS	5Y4/2	7.5YR5/6 >10% (from excavator bucket)	Mass, firmer than C1, Wet, smearing			

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) Glaciolacustrine		_ Depth to Bedrock: _> 106"	
Depth to Groundwater: Standing Water in the H	ole: <u>n/o</u>	Weeping from Pit Face:	n/o
Estimated Seasonal High Ground Water:68"			

Percolation Test:

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:

Test Pits								
Performed By M.D'Urso, The Berks	Performed By M.D'Urso, The Berkshire Design Group Witnessed By:							
Deep Hole Number TP 16	Date: 10	/31/07	Time:	12:50am	Weather	P-Cloudy 45 F	=	
Location (identify on site plan) See	Plan							
Land Use Wooded	Slope (?	%) <u>Se</u>	e Plan	Surface	e Stones	n/o		
Vegetation Mixed deciduous and ev	rergreen							
Landform								
Position on Landscape (sketch on bad	ck)							
Distances from: <i>See Plan</i> Open Water Body Possible Wet Area Drinking Water Well	······	Feet Feet Feet		ige way rty Line		Feet		

DEEP OBSERVATION HOLE LOG *								
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)			
0-31"	Fill		-		Fill over 2" thick macadam layer @ 31"			
31"-50"	C ₁	FSL	10YR5/8		Massive, friable, some stratified FSL and Fine Sand, roots down to 24", sloughing			
50"-90"	C ₂	LS	5Y4/2	7.5YR5/6 >10% throughout	Mass, firm, some smearing			

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) Glaciolacustrine		D	epth to Bedrock: > 90"	<u> </u>
Depth to Groundwater: Standing Water in the	Hole:	n/o	Weeping from Pit Face:	n/o
Estimated Seasonal High Ground Water: 5	50"			

Percolation Test: Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12":

Time at 9": Time at 6": Time (9"-6"): Rate:

Test Pits

Performed By M.D'Urso, The E	Berkshire Design Group	Witnessed By:		
Deep Hole Number TP 17	Date: 10/31/07	Time: 1:30pm	Weather	P-Cloudy 45 F
Location (identify on site plan) _	See Plan			
Land Use Wooded	Slope (%) <u>Se</u>	<u>e Plan</u> Surfa	ce Stones	n/o
Vegetation Mixed deciduous a	nd evergreen			
Landform	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		
Position on Landscape (sketch c	on back)			
Distances from: See Plan				
Open Water Body	Feet	Drainage way		Feet
Possible Wet Area	Feet	Property Line		Feet
Drinking Water Well	Feet	Other		

DEEP OBSERVATION HOLE LOG *								
Depth from Surface(Inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)			
0-46"	Fill	Silty Sand			Few bricks, cobbles, plastic, roots (new growth)			
46"-59"	C ₁	LS	2.5Y5/3	5YR4/6 Distinct >10% throughout	Massive, friable, some stratified FSL and Fine Sand, roots down to 24", sloughing			
59"-108"	C ₂	SL	5Y4/2	7.5YR5/6 >35% throughout	Massive, firm, some pockets of loam, smearing, wet @ bottom			

* MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DISPOSAL AREA

Parent Material (geologic) Glaciolacustri	ne		Depth to Bedrock: > 108"	
Depth to Groundwater: Standing Water in t	he Hole:	6" @ 30 minutes	Weeping from Pit Face:	95"
Estimated Seasonal High Ground Water:	54"			

Percolation Test:

Depth to Perc: Start Pre-Soak 12": End Pre-Soak 12": Time at 12": Time at 9": Time at 6": Time (9"-6"): Rate:



Northampton, Massachusetts

Stormwater Drainage Report Appendix

Appendix C – TSS Removal Summary

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Appendix

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INSTRUCTIONS:

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Treatment Train 1 for P-3 В С D Е F **TSS** Removal Starting TSS Amount Remaining BMP¹ Rate¹ Removed (C*D) Load* Load (D-E) Calculation Worksheet Deep Sump and Hooded Catch Basin 0.25 1.00 0.25 0.75 Removal Infiltration Basin 0.80 0.75 0.60 0.15 0.00 0.15 0.00 0.15 TSS 0.00 0.15 0.00 0.15 0.00 0.15 0.00 0.15 Separate Form Needs to be Completed for Each Total TSS Removal = Outlet or BMP Train 85% Northern Avenue, Northampton, MA Project: Prepared By: Brian Darnold *Equals remaining load from previous BMP (E) Date: 11/11/2008 which enters the BMP Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed

1. From MassDEP Stormwater Handbook Vol. 1

Mass. Dept. of Environmental Protection

Version 1, Automated: Mar. 4, 2008

Horn Avenue The JOB Landscape Architecture Berkshire SHEET NUMBER OF Civil Engineering Design CALCULATED BY BLD DATE Planning Group, Inc. CHECKED BY DATE Urban Design SCALE 4 Allen Place Environmental Services Northampton, Massachusetts 01060 Water Qualit Standard 4 HydrochD (DB1) Water Quality Basin Detertion Infiltration Rusin Imperirous area Flowing to DBA = Subcatchment P-3 = 9.307.5FDwa= 9,302-54 DSin 388cf F Provided Volume = 1:013 cf SachyarocaD calculations For DB1 cumulitivestorage up to elevention 92.80' 1,013 cf >388cF ~

Northern Avenue Housing-Active Prepared by The Berkshire Design Group HydroCAD® 8.00 s/n 000752 © 2006 HydroCAD Software Solutions LLC

Inflow Are	a =	0.615 ac, Inflow Depth > 1.85" for 2-Year event
Inflow	=	1.15 cfs @ 12.14 hrs, Volume= 0.095 af
Outflow	=	0.40 cfs @ 12.50 hrs, Volume= 0.069 af, Atten= 66%, Lag= 21.2 min
Primary	=	0.40 cfs @ 12.50 hrs, Volume= 0.069 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 93.23' @ 12.50 hrs Surf.Area= 2,100 sf Storage= 1,850 cf

Plug-Flow detention time= 172.3 min calculated for 0.068 af (72% of inflow) Center-of-Mass det. time= 83.1 min (900.2 - 817.1)

Volume	Inver	t Avail.Stora	age Storage	e Description
#1	92.20	o' 5,103	3 cf Custor	m Stage Data (Prismatic) Listed below (Recalc)
	_			
Elevatio	on S	Surf.Area	Inc.Store	Cum.Store
(fee	et)	(sq-ft) (cubic-feet)	(cubic-feet)
92.2	20	1,553	0	0_
	30	1,824	1,013	0 1.013
93. (1,953	378	1,391
94.0	00	2,602	2,278	3,668
94.5		3,136	1,435	5,103
Device	Routing	Invert	Outlet Devic	ces
#1	Primary	94.25'	6.0' long x 1	1.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet)	0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00	
			Coef. (Englis	sh) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3	•
#2	Primary	92.10'		D' long Culvert CMP, projecting, no headwall, Ke= 0.900
		•====		t = 91.73' S= 0.0051 '/' Cc= 0.900
				oncrete pipe, straight & clean
#3	Device 2			rifice/Grate C= 0.600
#5	Device 2	92.00		
Primany		Max-0.40 cfs @	12 50 hrs H	HW=93.23' (Free Discharge)
E rminal y	Out IOW I	101-0.40 CIS @	12.00 113 1	THE DISCHARGE

-1=Broad-Crested Rectangular Weir (Controls 0.00 cfs) -2=Culvert (Passes 0.40 cfs of 2.36 cfs potential flow)

1-3=Orifice/Grate (Orifice Controls 0.40 cfs @ 2.22 fps)

INSTRUCTIONS:

9

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

Deen Sumn an

В

BMP¹

3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Treatment Train 2 for P-2, P-4, and P-5

D

Starting TSS

Load*

Ε

Amount

Removed (C*D)

С

TSS Removal

Rate¹

Jee	Catch Basin	0.25	1.00	0.25	0.75		
oval orkshe	Rain Gardén	0.90	0.75		0.00		
	Ham Garden A	0.90	0.75	0.68	0.08		
Removal on Works		0.00	0.08	0.00	0.08		
TSS culatio		0.00	0.08	0.00	0.08		
T Calcul		0.00	0.08	0.00	0.08		
		93%	Separate Form Needs to be Completed for Each Outlet or BMP Train				
Project: Northern Avenue, Northampton, MA							
	Prepared By:	Brian Darnold		*Equals remaining load from	n previous BMP (E)		
Non-automate		1,1/11/2008		which enters the BMP			

Version 1, Automated: Mar. 4, 2008

F

Remaining

Load (D-E)

v

Mass. Dept. of Environmental Protection

must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1 **INSTRUCTIONS:**

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

3. After BMP is selected, TSS Removal and other Columns are automatically completed.

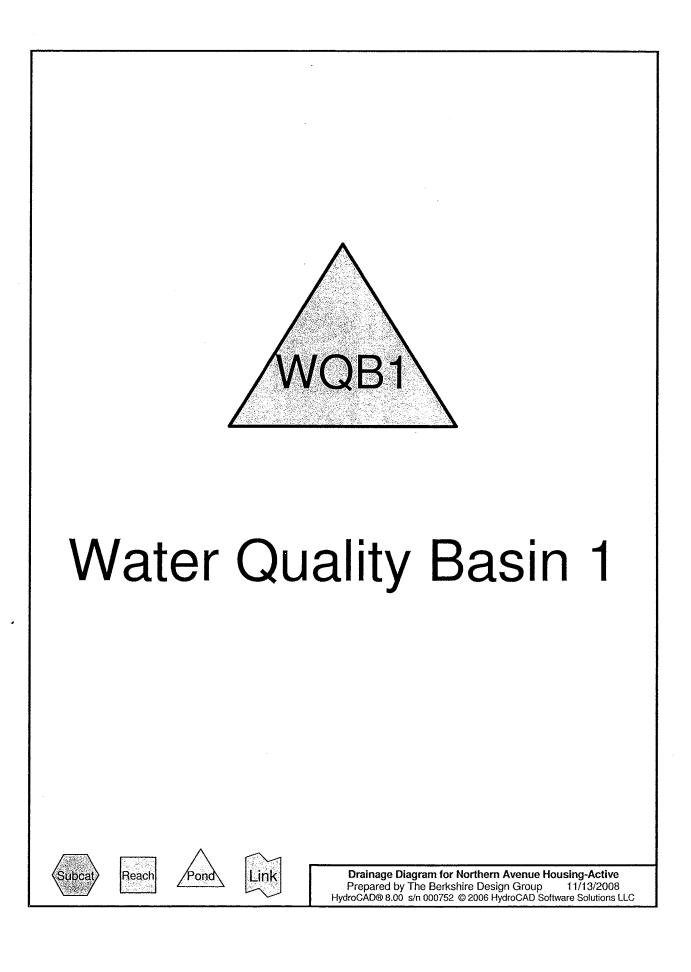
Location: Treatment Train 3 for P-8 Ε F С В D **TSS Removal** Starting TSS Amount Remaining BMP¹ Rate¹ Load* Removed (C*D) Load (D-E) **Calculation Worksheet** Rain Garden 0.90 1.00 0.90 0.10 **TSS Removal** 0.00 0.10 0.00 0.10 0.00 0.10 0.00 0.10 0.00 0.10 0.00 0.10 0.00 0.10 0.00 0.10 Separate Form Needs to be Completed for Each Total TSS Removal = **Outlet or BMP Train** 90% Project: Northern Avenue, Northampton, MA Prepared By: Brian Darnold *Equals remaining load from previous BMP (E) Non-automated TSS Calculation Sheet which enters the BMP must be used if Proprietary BMP Proposed

1. From MassDEP Stormwater Handbook Vol. 1

v

Mass. Dept. of Environmental Protection

JOB Northern Avenue The Berkshire Landscape Architecture SHEET NUMBER OF Civil Engineering Design DATE 11/11/08 CALCULATED BY BC Planning Group, Inc. CHECKED BY DATE Urban Design SCALE NTS 4 Allen Place Environmental Services Northampton, Massachusetts 01060 Water Quality standard " How CAD /WQB1 Water Quility Busin Bain Garden Impervices area flowing to two B1 = "Subcatchment P-S 5 529 sf 4,623 of 6,206 5 17,10354 Required waterpushity volume = Dwax AImp Dug = Offin (Noncritical area, londis not LUHPPK, norapidinf. eate) AIMP = 16,614 5 F Required water quality volume = (0.5:1) + (11+)+ 17,103 st = 713 cF Water quality basin volume = 738 cf 738cf>713cf > See WQB1 in Hypero(AD Fur Volume *See Appendix A For HydrocaD data including subcatchment and busin



Northern Avenue Housing-ActiveTypePrepared by The Berkshire Design GroupHydroCAD® 8.00 s/n 000752 © 2006 HydroCAD Software Solutions LLC

Type III 24-hr 100-Year Rainfall=6.50" Page 2 LLC 11/13/2008

Pond WQB1: Water Quality Basin 1

Routing by Stor-Ind method Peak Elev= 0.00' @ 0.00 hrs Surf.Area= 0 sf Storage= 0 cf

Plug-Flow detention time= (not calculated) Center-of-Mass det. time= (not calculated)

Volume	Invert	Avail.	Storage	Storage	Description	
#1	92.00'		738 cf	Custom	Stage Data (Prism	atic) Listed below (Recalc)
Elevation (feet)		.Area (sq-ft)		c-feet)	Cum.Store (cubic-feet)	
92.00 92.70		893 1,215		0 738	0 738	

INSTRUCTIONS:

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Treatment Train 4 for P-6 and P-7 Ε В С D F **TSS Removal** Starting TSS Amount Remaining BMP¹ Rate¹ Load* Removed (C*D) Load (D-E) Calculation Worksheet Deep Sump and Hooded Catch Basin 0.25 1.00 0.25 0.75 **TSS Removal** Proprietary Treatment 0.77 Practice 0.75 0.58 0.17 0.00 0.17 0.00 0.17 0.00 0.17 0.00 0.17 0.00 0.00 0.17 0.17 Separate Form Needs to be Completed for Each Total TSS Removal = Outlet or BMP Train 83% Project: Northern Avenue, Northampton, MA Prepared By: Brian Darnold

*Equals remaining load from previous BMP (E) which enters the BMP

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1

Mass. Dept. of Environmental Protection

Version 1, Automated: Mar. 4, 2008

Stormwater Technology: Stormceptor (Hydro Conduit, formerly CSR New England Pipe)

Revised February 2003

The Stormceptor Fact Sheet is one in a series of fact sheets for stormwater technologies and related performance evaluations, which are undertaken by the Massachusetts STrategic Envirotechnology Partnership (STEP).

A summary of the STEP evaluation entitled, *Technology Assessment, Stormceptor CSR New England Pipe*, January 1998 is provided in this fact sheet. When a more thorough understanding of a system is required, the full *Technology Assessment* should be reviewed. Copies are available for downloading from the STEP Web site (www.stepsite.org/progress/reports) or by contacting the STEP Program (Phone: 617/626/1197, FAX: 617/626/1180, email: linda.benevides@state.ma.us). The information in this fact sheet is subject to future updates as additional performance information becomes available.

Description/Definition

Stormceptor is a prefabricated, underground unit that separates oils, grease, and sediment from stormwater runoff when installed with an existing or new pipe conveyance system. The unit is divided into two chambers-a treatment and a flow bypass chamber. During typical storm events, runoff is directed by the inflow weir through a drop pipe into the lower treatment chamber where sediment, oil, and grease are separated from the flow by gravity. The bypass chamber is designed to convey excess stormwater, which overtops the inflow weir, through the system without treatment.

Equipment and Sizing

The on-line Stormceptor units are available in eight sizes ranging from six and twelve feet in diameter with capacities of 900 to 7200 gallons. Since issuing the STEP assessment in 1998, the manufacturer has expanded the Stormceptor product line to include a storm drain inlet (STC 450i) and three units (Models STC 11000, STC 13000, and STC16000). These systems are not included in the STEP evaluation. Users and decision-makers may require additional field test results and new data for these new systems in order to accept performance ratings, particularly if they are higher than those reported in the STEP technology assessment and this fact sheet.

Stormceptor units are available in either precast concrete or fiberglass for special applications. Concrete units are pre-engineered for HS-20 min. traffic loading at the surface. Fiberglass units can be used in areas where

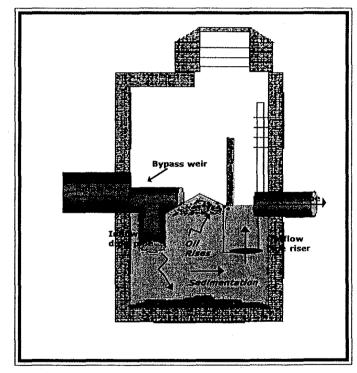


Figure 1. Stormceptor operation during average flow conditions.

there is a potential for oil and chemical spills.

Performance/Effectiveness

The system is designed to provide separation of sediment, oil, and grease from stormwater by routing runoff into a low-turbulence environment where solids settle and oils float out of solution. The system sizing is based on the drainage area, historical rainfall data, and



the solids removal efficiency required. It is recommended that the system be used in combination with other stormwater controls to conform with the Massachusetts Stormwater Management Policy and standards.

An Imperial Model STC 2000 (equivalent to the Model STC 2400) in Edmonton, Canada treats flow from a 9.8 acre commercial parking lot. This system was monitored during four storm events in 1996 and shown to have an average total suspended solids (TSS) removal efficiency of 52 percent. In designing a system to achieve a comparable removal efficiency, the relationship between system size and impervious drainage area should be considered, as detailed in Table 1 and the Technology Assessment Report.

A Model STC 1200 in Westwood, Massachusetts treats flow from 0.65 acres consisting of a paved truck loading area at a manufacturing facility. The unit was monitored for six storm events in 1997, but only four events had measurable TSS influent concentrations. Of these four events, the average TSS removal efficiency was calculated to be 77 percent, which is less than the 80 percent removal targeted by the manufacturer.

Based on these field monitoring results, and when the unit sizing follows the guidance in Table 1, removal efficiencies between 52 percent and 77 percent may be achieved where installations have similar rainfall and land use characteristics as those reviewed for the STEP evaluation. It is recommended that additional field research and new data be evaluated to validate performance ratings higher than those verified by STEP.

	Model Number	Maximum Imper 77% TSS remov	al 52% TSS remo
9	STC 900	0.45	0.9
	STC 1200	0.7	1.45
	STC 1800	1.25	2.55
	STC 2400	1.65	3.35
	STC 3600	2.6	5.3
	STC 4800	3.6	7.25
	STC 6000	4.6	9.25
	STC 7200	5.55	11.25

Table 1: Adapted from the Stormceptorsizing for TSS removal in the STEP

Technology Assessment. Notes: 1) On some sites, the maximum impervious area may need to be reduced to achieve these TSS removal rates. 2) The terms "critical area sizing" (to achieve 77 percent TSS removal) and "treatment train sizing" (for 52 percent removal) are no longer used by the manufacturer, but unit sizing is still applicable.

Specific performance claims for oil and grease were not evaluated by STEP. However, total petroleum hydrocarbons (TPH) were analyzed during the Westwood study. Results indicated that the unit was effective in capturing oils.

Technology Status

The Stormceptor system provides greater solids separation and higher TSS removal efficiencies than oil and grit separators. Stormceptor systems are among the category of hydrodynamic separators, which are flowthrough devices with the capacity to settle or separate grit, oil, sediment, or other pollutants from stormwater. According to the U.S. Environmental Protection Agency, "Hydrodynamic separators are most effective where the materials to be removed from runoff are heavy particulates - which can be settled - or floatables - which can be captured, rather than solids with poor settleability or dissolved pollutants."

Although Stormceptor appears to remove sediment, grit, oil, and grease as claimed by the manufacturer, additional research is needed to determine how much sediment moves through the system untreated. The field studies evaluated for the STEP assessment predate the Stormwater Best Management Practice Demonstration Tier II Protocol (2001), which is applicable in Massachusetts and other states in the Technology Acceptance Reciprocity Partnership (TARP), to ensure quality controlled studies that can be shared among participating states. Therefore, interstate reciprocity is not available to the manufacturer, based on performance claims that were evaluated by STEP in 1998. If the TARP Protocol requirements are fulfilled in the future, the manufacturer could pursue reciprocal verification for Stormceptor systems in participating TARP states. More information on the TARP Protocol is available on the following Web site: www.dep.state.pa.us/dep/deputate/pollprev/ techservices/tarp.

Applications/Advantages

- Stormceptor systems identified in Table 1 should be used in combination with other BMPs to remove 80 percent of the average annual load of TSS (DEP Stormwater Policy Standard 4). Systems may be well suited for pretreatment in a mixed component system designed for stormwater recharge.
- Performance data show that Stormceptor may provide TSS removal rates in the range of 52 percent to 77 percent when sized according to Table 1. Higher TSS removal rates were achieved during low flow, low intensity storms with less than one third of an inch of runoff. Also, by reducing the impervious drainage area,

relative to the system size, the STEP Technology Assessment Report indicated that higher removal efficiencies may be achievable. However, STEP recommends collection of additional data "representing a varied set of operating conditions over a realistic maintenance cycle to verify TSS removal rates greater than 80 percent."

- ♦ The Stormceptor system is suitable for new and retrofit applications. For retrofit applications, it should not take the place of a catch basin for the systems that have been verified. Also, for retrofit applications, it should be installed in lateral lines and not main trunk lines.
- The system is particularly well suited in constricted areas and where space is limited.
- It also is suitable for use in areas of high potential pollutant loads (DEP Stormwater Policy Standard 5), where it may be used effectively in capturing and containing oil and chemical spills. Web site: www.state.ma.us/dep/ brp/stormwtr/stormpub.htm.

Considerations/Limitations

- Systems are not expected to provide significant nutrient (nitrogen and phosphorus) or fecal coliform removal.
- ♦ The systems are not recommended for use in critical areas, such as public drinking water supplies, certified vernal pools, public swimming beaches, shellfish growing areas, cold water fisheries, and some Areas of Critical Environmental Concern (ACECs), except as a pretreatment device for BMPs that have been approved by DEP for use in critical areas. The structural BMPs approved for use in critical areas are described in Standard 6 of the Stormwater Management Policy, www.state.ma.us/dep/brp/stormwtr/stormpub.htm.
- There is a limited set of useful data for predicting the relationship between treatment efficiency and loading rates. Removal efficiencies have not been demonstrated for all unit sizes.
- Further research is needed to determine how much TSS bypasses the treatment chamber during certain, higher velocity storm events which recur less frequently.
- Systems require regular maintenance to minimize the potential for washout of the accumulated sediments.

Reliability/Maintenance

All BMPs require scheduled, routine maintenance to ensure that they operate as efficiently as possible. Although maintenance requirements are site specific, a general relationship between cleaning needs and depths of sediment has been established by the manufacturer. Inspection of the Stormceptor interior should be done after major storm events, particularly in the first year of operation. It is recommended that material in the treatment chamber be pumped out by a vacuum truck semiannually, or when the sediment and pollutant loads reach about 15 percent of the total storage. If the unit is used for spill containment, it should be pumped after the event is contained. Typical cleaning costs were estimated by the manufacturer in 1998 to be \$250, with disposal costs averaging \$300 to \$500. The expected life of a system has been estimated to be 50 to 100 years.

Sediment Depths Indicating Required Maintenan				
Model Number	Sediment Depth (feet)			
STC 900	0.5			
STC 1200	0.75			
STC 1800	1			
STC 2400	1			
STC 3600	1.25			
STC 4800	1			
STC 6000	1.5			
STC 7200	1.25			

Table 2: The Stormceptor system clean out is based on 15 percent of the sediment storage volume in the unit.

References

Winkler, E.S. 1998. "Technology Assessment, Stormceptor." University of Massachusetts, Amherst, MA. *STEP Web site:* www.stepsite.org/progress/reports

Massachusetts Department of Environmental Protection and Office of Coastal Zone Management. 1997. "Stormwater Management Handbooks, Volumes One and Two." Boston, MA. *Handbooks Web site:* www.state.ma.us/dep/brp/ stormwtr/stormpub.htm.

"Performance of a Proprietary Stormwater Treatment Device: The Stormceptor. The Practice of Watershed Protection: Article 120. Thomas. R. Schueler and Heather K. Holland editors. 2000. Ellicott City, MD.

United States Environmental Protection Agency. "Storm Water Technology Fact Sheet Hydrodynamic Separators." EPA 832-F-99-017.

Stormceptor Web sites: www.rinkermaterials.com/ stormceptor

TARP Web site: www.dep.state.pa.us/dep/deputate/ pollprev/techservices/tarp.

Stormceptor Sizing Table

Version 3.0.0

Selec	ted Rainfall Station	Part	Particle Size Distribution		
State Name	MASSACHUSETTS	Diameter (um)	Percent (%)	Velocity (ft/s)	
ID #	KNIGHTVILLE DAM 3985	20	20.0	0.0013	
Elev. (ft) Latitude	630 N 42 deg 17 min	60	20.0	0.0052	
Longitude	W 72 deg 52 min	150	20.0	0.0351	
Site Parameters		400	20.0	0.2116	
		2000	20.0	0.9416	
Total Area (a Imperviousn Impervious A	ess (%) 47	Note : Sizing Results vary with particle size distribution. BMP comparisons must use the same particle size distribution. Please call (800) 909-7763 for sizing with other distributions			

Stormceptor Sizing Table				
Stormceptor Model	% Runoff Treated	% TSS Removal		
STC 450i	97.0	84.2		
STC 900	99.3	90.1		
STC 1200	99.3	90.3		
STC 1800	99.3	90.6		
STC 2400	99.9	92.8		
STC 3600	99.9	93.4		
STC 4800	100.0	94.9		
STC 6000	100.0	95.2		
STC 7200	100.0	96.1		
STC 11000	100.0	97.4		
STC 13000	100.0	97.5		
STC 16000	100.0	98.0		

Comments :

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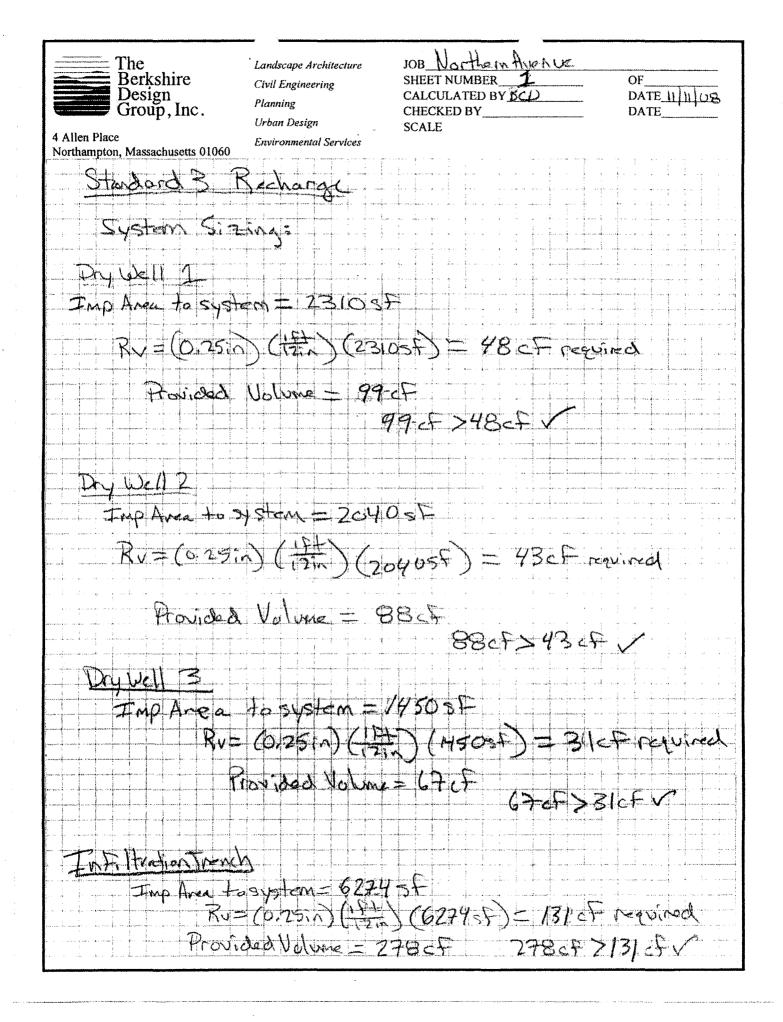
Northampton, Massachusetts

Stormwater Drainage Report Appendix

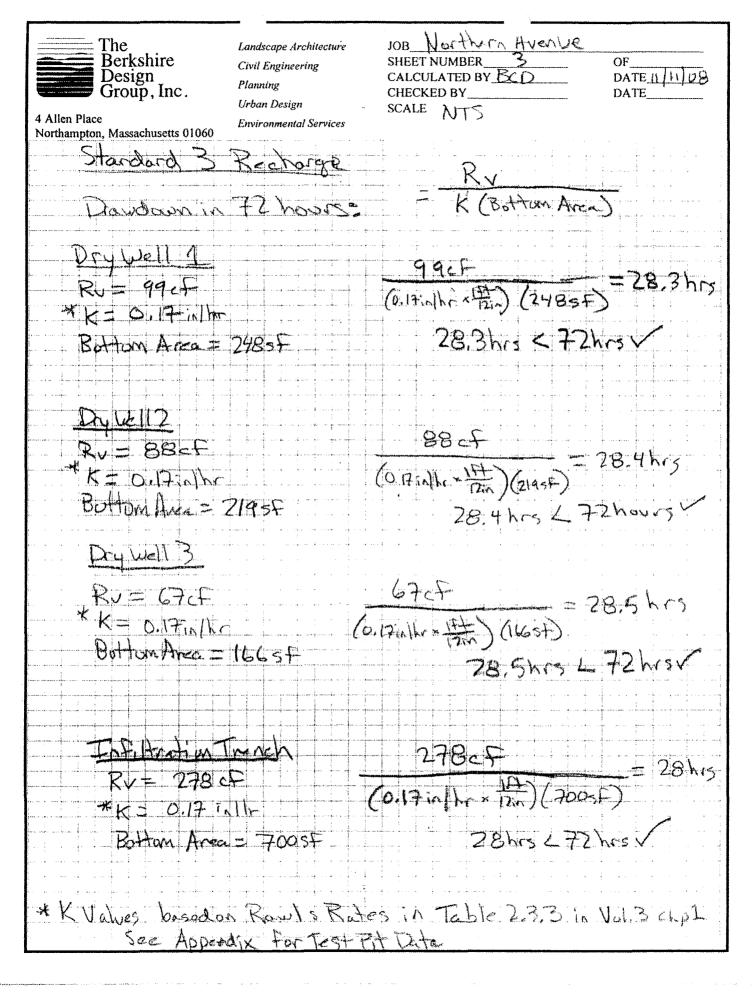
Appendix D – Standard 3 Recharge Calculations

Appendix

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Northern Buenve The JOB Landscape Architecture Berkshire SHEET NUMBER OF Civil Engineering Design Group, Inc. CALCULATED BY RD DATE WINDS Planning CHECKED BY DATE Urban Design SCALE 4 Allen Place Environmental Services Northampton, Massachusetts 01060 Dry Well 4 ImpArea to system= 758sf Rv= (0.25:n) (15) (758-5) 16 of regulard Provided volume = 3247 32 CF X 16 CF V (Detention Basin #1) Infiltration Basin area to system = 9,302 st Impervious Ru= (0.25in) (121-) (9,302 st) = 194 cf Provided volume = 1/013 cf. See HydroCAD calculations for DB1 storage UP to 92.80 1013, F> 194 cf v



JOB Norther A NEAVE The Landscape Architecture Berkshire OF Civil Engineering Design Group, Inc. DATE 11/11/08 CALCULATED BY Planning CHECKED BY DATE Urban Design SCALE NTS 4 Allen Place Environmental Services Northampton, Massachusetts 01060 Landown in 72 hours Dry Well 4 324 $R_{v} = 32 cF$ (0.17 1.1h - 212 (803F) = 28,2hrs K=0,17 1,14 Bottom Area = 80st 28.2hrs 472hrsv randown in 72 hours (Detertion Basin 1) In Filtration Basin Ry= 1,0Bcf $K = 0, l \neq in lhr$ LOBEF Botton Area = 1553 Contrin the attend 46 hrs Albert 72

The Berkshire Design Group, Inc. 4 Allen Place Northampton, Massachusetts 01060	Landscape Architecture Civil Engineering Planning Urban Design Environmental Services	JOB <u>Hortheen twen ve</u> SHEET NUMBER <u>S</u> CALCULATED BY <u>BCO</u> CHECKED BY SCALE	OF DATE_ <u>II</u>]] U9 DATE
Standard & - Re Required Recharges		Ex Empervious Area	
Impervious Arc	a= 56,6025f	and a second	
$R_{x} = (0.25)$	$) \times (121) \times 1$	56,602sF = 1180cF To (OBI) InFilization Besin	
Total Imp Area Sar	r to infiltratio	n systems: Dry Well = =	7585F 2310 st
		Dry Well 3 = Dry Well 3 = Enfl Heation Trench	1,450 st
100× 22,1345€			22,134 F
56,60235	- >1.10.7 39.10%	6 of impervious infi < 65% standard 3 met	Notfully
		Ønly to massi m	im attert
		SeeWestSl	et->

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Northampton, Massachusetts

Stormwater Drainage Report Appendix

<u>Appendix E – Proposed Stormwater Management</u> <u>System Operation & Maintenance Plan</u>

Proposed Stormwater Management System Operation & Maintenance Plan

During Construction

The Contractor shall be responsible for inspection and maintenance during construction.

At all times, siltation fabric fencing, stakes and hay bales sufficient to construct a sedimentation control barrier a minimum of 50 feet long will be stockpiled on the site in order to repair established barriers which may have been damaged or breached.

An inspection of all erosion control and stormwater management systems shall be conducted by the Contractor at least once a week and during all rain storms until the completion of construction. In case of any noted breach or failure, the Contractor shall immediately make appropriate repairs to any erosion control system and notify the engineer of any problems involving stormwater management systems.

A rain storm shall be defined as all or one of the following:

- Any storm in which rain is predicted to last for twelve consecutive hours or more.
- Any storm for which a flash flood watch or warning is issued.
- Any single storm predicted to have a cumulative rainfall of greater than one-half inch.
- Any storm not meeting the previous three thresholds but which would mark a third consecutive day of measurable rainfall.

The Contractor shall also inspect the erosion control and stormwater management systems at times of significant increase in surface water runoff due to rapid thawing when the risk of failure of erosion control measures is significant.

In such instances as remedial action is necessary, the Contractor shall repair any and all significant deficiencies in erosion control systems within two days.

The Conservation Commission shall be notified of any significant failure of stormwater management systems and erosion and sediment control measures and shall be notified of any release of pollutants to a water body (stream, brook, pond, etc.).

Operation & Maintenance Plan

The Contractor shall remove the sediment from behind the fence of the sedimentation control barrier when the accumulated sediment has reached one-half of the original installed height of the barrier.

Post-Construction

Stormwater Management System Owner:

The Owner,

Tofino Associates, Inc. 31 Campus Plaza Road Hadley, MA 01035

shall own the stormwater management system.

Party Responsible for Operation & Maintenance:

The Owner,

Tofino Associates, Inc. 31 Campus Plaza Road Hadley, MA 01035

shall operate and maintain the stormwater management system.

Inspection & Maintenance Schedule:

1) Street Sweeping

Street and parking area sweeping shall take place twice annually.

2) Rain Garden

A rain garden/bioretention area has been incorporated into the stormwater system to remove pollutants within the stormwater runoff. Both the pre-treatment stone diaphragm system and bioretention areas should be inspected monthly for sediment build-up, litter and debris, structural damage and standing water. Inspect soil and repair eroded areas within the bioretention system monthly and re-mulch void areas as needed. Treat diseased vegetation as needed. Remove and replace dead vegetation twice per year (spring and fall). Remove invasive species as needed to prevent them from spreading into the bioretention area. Replace mulch every two years in the early spring. In the winter, it is important to ensure that snow is not plowed into the rain garden as this will cause the runoff to bypass the system without proper treatment. 3) **Detention Basins** (The following recommendations follow the MADEP Stormwater Policy guidelines.)

Inspections

- a. Initial six months of use.
 Examine for stabilization and function, including determination of the duration of water standing in the basin, any sediment erosion, excessive compaction of soils, or low spots.
- b. Twice per year.
 Examine basin for the following: differential settlement, cracking, erosion, leakage, or tree growth on embankments, condition of riprap, sediment accumulation, and health of turf where applicable.

Any adverse conditions noted during any inspections shall be addressed by repair or reconsideration of design components.

Mowing and General Maintenance

Occasional mowing (1-2 times per year min.) shall be performed on the side slopes and basin bottom where turf is present. Accumulated grass clippings and/or organic matter and trash and debris shall be removed. Any clogged surface areas can be loosened by deep tilling; tilled areas must be immediately revegetated. Tilling may be used in this manner for no more than two consecutive maintenance periods. Thereafter, sediment in the clogged areas shall be removed, liner material replaced, and revegetation established.

Dredging/Sediment Removal

Accumulated sediment shall be removed from the basin at five (5) year intervals, or as required to maintain the function of the stormwater management system as designed. During this process and until the disturbed sediment has settled, the outlet pipe shall be sealed so as to minimize the risk of conveying sediment beyond the basin.

4) Grassed Swales

Swales shall be mowed at least once per growing season to prevent establishment of woody growth and other undesirable plants that inhibit proper performance. Grass vegetation should not be cut shorter than 4". It is important not to engage in excessive mowing operations, as this keeps the grass too short and decreases the efficiency of the vegetation to reduce runoff borne sediments and velocities.

Sediment and debris shall be removed manually at least once per year before the vegetation is adversely impacted.

5) Hooded Catch Basin and/or Drain Manhole with Sump

Oil and water separators should be inspected at least four times per year and cleaned annually or more often if required. Oil and sediments should be removed and disposed of in accordance with local, state and federal guidelines and regulations. In the case of an oil or bulk pollutant release, the system must be cleaned immediately following the spill and the proper authorities notified.

6) Stormwater Treatment Chambers

The Stormwater Treatment System requires minimal routine maintenance; however, it is important that the system be properly inspected and cleaned when necessary in order to function at its best. The rate at which the system collects pollutants will depend more heavily on site activities than the size of the unit, e.g. heavy winter sanding will cause the grit chamber to fill more quickly, but regular sweeping will slow accumulation. The water quality treatment system shall consist of **Storm***ceptor* or equal treatment chambers. For more detail of how the **Storm***ceptor* should be maintained see the **Storm***ceptor* Owner Manual.

7) Dry Wells

Dry wells basins have been incorporated into the stormwater system for the site to specifically receive roof runoff and, therefore, are not expected to receive large amounts of bulk sediments. Proper maintenance of roof gutters that drain to the system will help to protect the integrity of the infiltration basins. Sediments and debris should be removed and disposed of in accordance with local, state and federal guidelines and regulations.

8) Snow Removal & Management Plan

General

The stormwater management system is designed to accommodate volumes from snow melt. Since plowed snow from paved surface may contain salts, sediment, Northampton, MA

oils and various pollutants, all snow melt from vehicular areas on the site shall be routed through the drainage system or removed from the site.

Principles

1. The Owner shall provide a copy of this plan and a schedule or vehicle rotation scheme to plowing contractors such that plowing may occur in an efficient manner. This may be altered based on employee schedules or severity or frequency of snow events.

2. No such snow shall be dumped or stockpiled directly into any resource area or its buffer area or within any area such that untreated snow melt may enter a resource area.

3. Snow removed from the site shall be disposed of such that it or its melt will have no adverse effect on other resource areas.

4. The use of sand or deicing materials shall not be excessive. The Owner is encouraged to utilize alternative eco-friendly solutions throughout the site.

5. The Conservation Commission and DPW shall be notified where a violation of this plan occurs.

6. See Figure 1 on the following page for a graphic depicting the snow stockpiling plan.

Northern Avenue Northampton, MA

Operation & Maintenance Plan

16 15 1 R 5 SNOW STORAGE AREA N 3648'55 153.86 5 532737 ŤŻ. 13 -40 111 VIEW A A PRIVATE B 1 SNOW STORAGE AREA 17 25 Í8 24 19 PCL SS I 20 23 22 21 SNOW STORAGE AR 8 ^{11,12}

Figure 1 – Snow Stockpiling Plan

NORTHERN AVENUE HOUSING - Stormwater Infrastructure

Inspection Schedule:

FORM TO BE COMPLETED PER SCHEDULE PRESENTED IN OPERATION & MAINTENANCE PLAN

Inspector:	
Date:	

Time:

Inspector's Qualifications:

Days Since Last Rainfall:

Amount of Last Rainfall (inches):

Catch Basins

СВ	Is Surface Runoff Being Directed to Catch Basins Properly	Are Sediment Traps Installed at Catch Basin Inlets	Are Catch Basin Outlet Hoods Installed and Working Properly	Depth of Sediment in Basin Sump	Are Any Correction Measures Required
CB#1					
CB#2					
CB#3					
CB#4					
CB#5					
CB#6					
<u></u>				· · · · · · · · · · · · · · · · · · ·	

Maintenance Required:

To Be Performed By:

On or Before:

STRUCTURAL CONTROLS -CON'T

Stormwater Treatment Chambers

SWTC	Is Surface Runoff Being Directed Through SWTS Properly	Depth of Sediment in Basin Sump	Are Any Correction Measures Required
SWTC		·	
#1		-	
L	L I		

Maintenance Required:

To Be Performed By:	On or Before:

Bioretention Area

Structure	Is Structure Working Properly	Depth of Sediment in Structure	Are Any Correction Measures Required	Additional Notes
Stone/Grass Pretreatment				
Rain Garden				

Maintenance Required:

To Be Performed By:	On or Before:

Grassed Swale

Structure	Is Structure Working Properly	Depth of Sediment in Structure	Are Any Correction Measures Required	Additional Notes
Grass swale				

Maintenance Required:

To Be Performed By:	On or Before:

Is Stormwater Entering Basin Correctly	Is Stormwater Being Detained and Discharged Properly	Depth of Sediment in Spreader	Is Rip-Rap Stabilization Properly Installed & Maintained	Is There Any Evidence of Erosion Or unintended Flow Patterns

Stormwater Detention Basin 1

Maintenance Required:

To Be Performed By:	On or Before:
TO BE FERIORINED BY.	

Stormwater Detention Basin 2

Is Stormwater Entering Basin Correctly	Is Stormwater Being Detained and Discharged Properly	Depth of Sediment in Spreader	Is Rip-Rap Stabilization Properly Installed & Maintained	Is There Any Evidence of Erosion Or unintended Flow Patterns

Maintenance Required:

To Do Doute una od Davi	On an Defense
To Be Performed By:	On or Before:

OTHER CONTROLS

List Other Miscellaneous Controls and Observations

Item	Describe Failure/Inadequate Control	Describe Recommended Remedy
	· · · · · · · · · · · · · · · · · · ·	
	·	
· · · · · · · · · · · · · · · · · · ·		
		· · · ·

Maintenance Required:

To Be Performed By:	On or Before:

- -

Northampton, Massachusetts

Stormwater Drainage Report Appendix

Appendix F – Long Term Pollution Prevention Plan

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Long Term Pollution Prevention Plan

This plan was developed in compliance with the Massachusetts Department of Environmental Protection Stormwater requirements.

Good Housekeeping

The proposed site is designed to maintain high water quality treatment for all runoff. A general maintenance plan has been prepared and will be followed in a strict and complete manner as required.

Spill Prevention Plan

No hazardous materials are will be stored on site. However the following spill prevention plan will be incorporated into the Long Term Pollution Prevention Plan:

- Manufacturers' recommended methods for spill cleanup will be clearly posted and site personnel will be made aware of the procedures and the location of the information and cleanup supplies.
- Materials and equipment necessary for spill cleanup will be kept in the on-site material storage area. Equipment and materials will include, but is not limited to, brooms, dust pans, mops, rags, gloves, goggles, kitty litter, sand, sawdust and plastic and metal trash containers specifically for this purpose.
- All spills will be cleaned up immediately after discovery.
- The spill area will be kept well ventilated and personnel will wear appropriate protective clothing to prevent injury from contact with a hazardous substance.
- Spills of toxic or hazardous material will be reported, regardless of size, to the Massachusetts Department of Environmental Protection at 888-304-1133.
- Should a spill occur, the spill prevention plan will be adjusted to include measures to prevent another spill and to cleanup up the spill should another occur. A description of the spill, along with the causes and cleanup measures will be included in the updated spill prevention plan.
- The construction superintendent responsible for daily operation on the construction site will be the spill prevention and cleanup coordinator. The superintendent will designate at least three site personnel to receive spill prevention cleanup and training. These individuals will each become responsible for a particular phase of prevention and cleanup. The names of responsible spill personnel will be posted in the material storage area and in the on-site job trailer.

Stormwater BMP Maintenance

A full stormwater operation and maintenance plan has been prepared (see Appendix D of this report) in order to ensure that the system will function properly throughout the year.

Landscape and Lawn Maintenance

Routine mowing and associated maintenance of all landscape features will occur weekly or as needed to prevent excessive growth and debris from occurring on site.

Long Term Pollution Prevention Plan

Solid Waste Management

Solid waste is handled on site and will comply with all requirements on a local, state, and federal level.

Parking/Road Area Maintenance

Street sweeping shall occur annually A full snow management plan has been prepared (see Appendix D) to prevent dirty snow and salt from entering the drainage system.

Training of Staff

All personnel on site will be well briefed on all requirements for implementing the Long Term Pollution Prevention Plan.

Emergency Contact for Implementing Long Term Pollution Prevention Plan

Tofino Associates, Inc. 31 Campus Plaza Rd Hadley, MA 01035 413 256 0321 Northampton, Massachusetts

Stormwater Drainage Report Appendix

<u>Appendix G – Stormwater Pollution Prevention</u> <u>Plan</u>



Stormwater Pollution Prevention Plan

Prepared in compliance with City of Northampton Stormwater Management Permit

Northern Avenue Housing

Northern Avenue and North Street Northampton, Massachusetts

November 11, 2008

Prepared by:

The Berkshire Design Group, Inc.

4 Allen Place, Northampton, Massachusetts 01060

Prepared For: Tofino Associates, Inc. 31 Campus Plaza Road Hadley, MA 01035

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SITE & PROJECT DESCRIPTION

Project Name and Location

Northern Avenue Housing 56 Northern Avenue Northampton MA 01060

Applicant/Owner Name and Address:

Tofino Associates, Inc. 31 Campus Plaza Road Hadley, MA 01035

Notification – Prior To Construction:

General Contractor/Operator:

To Be Determined

City of Northampton Department of Public Works 30 Locust Street Northampton, MA 01060

Mr. Douglas McDonald NPDES Coordinator Phone: 413-587-1582

Existing Zoning & Land Use & Site Area

The project parcel is zoned URB district and is located on the west side of Northern Avenue and north of North Street. The site currently contains a large wetland area to the west, with woods, grassed, and small roadway areas throughout the rest of site. The overall curve number in existing conditions is 74 and water flows in a westerly direction through the wetlands and to a small river located at the southwest portion of the property line (see figure 1 on page 3). The total area of the site is approximately 6 acres, of which approximately 3.4 acres will be disturbed by construction activities.

Proposed Project

The proposed development includes 25 new housing units and associated parking areas, driveways, and sidewalks, utilities, landscape features and stormwater management system. A large wetland area exists on the west part of the site and will not be disturbed as a result of construction.

Stormwater management will consist of catch basins, manholes, stormwater treatment chambers, 2 surface drainage detention basins (see attached plan EC1), dry wells, an infiltration trench, a rain garden and temporary erosion control devices during construction. Stormwater discharge will flow into the wetlands as it does in existing conditions.

Soil disturbing activities will include: installation of erosion and sediment controls; tree removal and grubbing; grading; excavation for building foundation, utility trenches, and landscape features, and site grading; installation of retaining walls, curbs, fences/guardrails, light pole foundations; paving of driveways, walkways and parking areas; and preparation for final seeding and planting.

Runoff Coefficient

Drainage calculations for this project, developed using the SCS TR20 method, resulted in an SCS overall curve number (CN) of 80 for the proposed project site.

Sequence of Major Construction Activities

The general order of construction activities at the site will be as follows:

- 1. Hold preconstruction meeting at least one week prior to start of construction
- 2. Install haybale/silt fence barrier around down slope side of construction area and wetlands and as directed in the Erosion and Sediment Control Plan, Figure 2
- 3. Install stabilized construction entrances
- 4. Clear and grub for sedimentation basins
- 5. Construct detention basins and swales to be used as temporary sedimentation basins during construction activities
- 6. Convey overland flow directly to sedimentation basins until stormwater infrastructure is constructed
- 7. Continue clearing and grubbing
- 8. Stockpile topsoil
- 9. Install utilities, storm drainage structures and basins, and curbs.
- 10. Protect stormwater structure inlets with sediment control devices.
- 11. Install building foundations and construct buildings
- 12. Grade and apply gravel base to driveways, walkways, and roadways
- 13. Complete grading and install paving
- 14. Install permanent seeding and plantings
- 15. Remove sediments accumulated in sedimentation basin and in front of haybale/silt fence barrier
- 16. Remove haybale/silt fence barrier and reseed areas disturbed by its removal
- 17. Remove temporary sedimentation basin outlet piping. Grade and seed areas as specified on the grading and utility plans.
- 18. Clean and flush all drainage structures and lines
- 19. Schedule post construction conference and inspection

Name of Receiving Waters

The site ultimately to a stream which flows to Market Street Brook which is piped parallel to the railroad tracks all the way to the Old Mill River near the Waste Water Treatment Plant off of Hockanum Road. Please see figure 1 below depicting the stream flow direction.



Figure 1

CONTROLS DURING CONSTRUCTION

November 11, 2008

Erosion and Sediment Controls

General Sedimentation Control Practices

The following general erosion and sediment controls will be utilized during construction in order to maintain local water quality:

- 1. Erosion control barriers will be installed prior to clearing and excavation work.
- 2. Grading and other soil disturbance will be done so as to minimize erosion during wet seasons.
- 3. A temporary sedimentation basin with required controls will be constructed early in the project to allow the basin to treat runoff prior to discharging from the site.
- 4. Sediment will periodically be removed from behind sediment trapping devices and from within the temporary sedimentation basin.
- 5. The clearing of natural vegetation will be minimized; remaining natural vegetation will be protected from nearby construction to the greatest degree possible.
- 6. Staging and soil stockpile areas shall have a haybale/siltation fence or other approved barrier installed immediately downgradient of such areas.
- 7. Designated temporary dewatering basins will be used for dewatering.
- 8. Disturbed areas will be stabilized as soon as possible after construction.
- 9. Maintenance and cleaning of construction vehicles and equipment will take place in designated staging areas only.

Stabilization Practices

The following stabilization practices will be utilized during construction in order to maintain local water quality:

- 1. Temporary stabilization: temporary seeding, mulching or other suitable stabilization measures will be utilized to protect disturbed areas and stockpiles during prolonged construction periods.
- 2. Permanent stabilization: areas disturbed by construction will be permanently stabilized by paving with concrete or bituminous concrete, by installation of plant material, or by seeding and mulching with seed mix as described in the project specifications. Seeded areas will be covered with straw mulch or biodegradable netting in order to protect surface until seed germination.

Structural Practices

The following structural erosion and sediment controls will be utilized during construction in order to maintain local water quality:

- 1. Sediment Barriers: silt barriers will be installed along the downslope edge of areas of work.
 - Sediment will be removed from behind silt fence when it reaches half the original height of the fence.
 - Fences will be inspected weekly and both before and after storm events. Repairs and replacement will take place as necessary.
- 2. Dewatering Basins/collectors: Dewatering basins/collectors will be constructed where required prior to excavation activities. These basins will act to settle suspended solids from pumped groundwater.
 - Dewatering Basins and collectors will be sized according to the amount of groundwater encountered at a particular location.
 - Dewatering Basins will utilize a perforated standpipe wrapped in filter fabric for discharge
- 3. Catch Basin Filters: Filters consisting of anchored haybales and filter fabric fence, embedded 4-6" in the ground, will surround each existing and proposed catch basin. Filter fabric will also be installed under each inlet grate.
 - Filters will be placed around each catch basin prior to paving or planting.
 - Sediment will be removed when it reaches half of the original height of the filter.
 - Filter fabric under the inlet grate will be monitored and replaced as required.
 - Filters will be removed only after upgradient areas have been permanently stabilized.
- 4. Dust Control: Dust control will be maintained by sprinkler or water truck during construction to minimize sediment transport and maintain air quality at an acceptable level.
- 5. Roadway Stabilization: Until final paving takes place, project roadways and parking areas will be stabilized by grading with clean gravel. Emergency access and service roadways will be maintained as clean gravel surfaces. A temporary Stabilized Construction Access will be constructed prior to the start of excavation work.

Stormwater Management

A system for stormwater management has been designed for this project. The system, designed by a professional engineer, utilizes curbs and gutters, catch basins, a stormwater treatment chamber, a rain garden, an infiltration trench, dry wells, and 2 surface detention basins to reduce total suspended solids (TSS) in excess of 80% and ensure that peak flows for 2-, 10-, and 100-

year storms remain at or near their estimated historic levels. Water from the project site will be discharged to the wetlands on the west part of the site as it does in existing conditions.

A maintenance plan for the stormwater management system has also been developed. The maintenance plan includes removal of oil and sediment from hooded catch basins, removal of oil and sediment from stormwater treatment chambers, clearing of debris for all basins, and annual sweeping of drives and parking lots.

Other Controls

Waste Disposal

Waste Materials: Waste materials will be collected and stored in a lidded metal dumpster rented from a licensed solid waste management company. All trash and construction debris will be stored in the dumpster. The dumpster will be emptied at least twice a week, or more if necessary, and disposed of in accordance with local, state and federal regulation. No construction waste materials will be buried on site. Notices stating these procedures will be posted in the job trailer. Site personnel will be instructed in these procedures and site construction supervisor(s) will ensure that the procedures are followed.

Hazardous Waste: Hazardous waste will be disposed of in the manner specified by local, state and federal regulation or by the manufacturer. Site personnel will be instructed in these procedures and site construction supervisor(s) will ensure that the procedures are followed.

Sanitary Waste: Sanitary waste will be collected from portable units a minimum of three times per week by a licensed sanitary waster contractor and disposed of in accordance with local, state and federal regulation.

Off-Site Vehicle Tracking

A stabilized construction entrance will be provided to help reduce tracking of sediments off the site. Stone will be used, which will be large enough not to become embedded in truck tires, at the entrance. The paved street adjacent to the construction entrance will be swept daily to reduce mud, dirt or sediment tracked from the site. Dump trucks hauling material to and from the site will be covered by tarps as necessary.

Timing of Controls

As indicated in the Sequence of major Activities, the haybale/silt fence barrier, stabilized construction entrance and sedimentation basin will be constructed prior to clearing or grading of any other portions of the site. No excavation or dewatering activities will take place in an area until appropriate dewatering basins or sediment control structures have been installed. Areas where construction activity temporarily ceases for more than 21 days will be stabilized with temporary seed and mulch within 14 days of the last disturbance. Once construction activity ceases permanently in an area that area will be stabilized with plant material or pavement as

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indicated in the plans. After the entire site is stabilized, the accumulated sediment will be removed from the sediment basin.

MAINTENANCE AND INSPECTION PROCEDURES

Erosion and Sediment Control Inspection and Maintenance Practices

The following inspection and maintenance practices will be utilized in this project to maintain sediment and erosion controls:

- All control measures will be inspected weekly (at a minimum) and following any storm event of 0.5 inches or greater.
- All measures will be maintained in good working order; if a repair is necessary, it will be initiated within 24 hours of report.
- Contractor will stockpile on site or make available all equipment, materials (e.g. filter fabric, haybales, crushed stone, etc.) and labor necessary to make emergency erosion control improvements within four hours if necessary.
- Built-up sediment will be removed from silt fence when it has reached one-third the height of the fence.
- Silt fence will be inspected for depth of sediment, tears, to verify that fabric is securely attached to the stakes and to verify that stakes are firmly in the ground.
- Sediment basin(s) will be inspected for depth of sediment, and accumulated sediment will be removed when it reaches 10 percent of the design capacity or at the end of the job.
- Temporary and permanent seeding will be inspected for bare spots, washouts and healthy growth.
- A maintenance inspection report will be made after each inspection.
- The site contractor will select one or more individuals who will be responsible for inspections, maintenance and repair activities and for completing inspection and maintenance reports.
- Individuals selected for inspection and maintenance responsibilities will receive training in all inspection and maintenance practices necessary for keeping the on-site erosion and sediment controls in good working order.

Non-Stormwater Discharges

It is expected that the following non-stormwater discharges will occur from the site during the construction period:

- Water from water line flushings.
- Pavement wash waters (where no spills or leaks of toxic or hazardous chemicals have occurred.
- Uncontaminated groundwater from dewatering excavations.
- Water from washing the exterior of construction vehicles.

Non-stormwater discharges will be directed to stabilized surfaces or the detention basin prior to discharge. Exterior washing and rinsing of vehicles will take place more than 100 feet from wetlands or waterways.

Inventory for Pollution Prevention Plan

Asphalt Cleaning solvents Concrete Detergents Fertilizers Gravel

Masonry block Metal studs Paints (enamel and latex) Petroleum-based products Solvents Wood

Spill Prevention

All employees will be instructed regarding the following spill prevention practices. Notice of these practices will be posted in the job trailer, and the site construction supervisor will hold responsibility for ensuring that the procedures are followed.

Material Management Practices

The following material management practices will be used to reduce the risk of spills or other accidental exposure of materials and substances to stormwater runoff:

Good Housekeeping

The following good housekeeping practices will be followed on-site during the construction period:

An effort will be made to store only enough product to do the job.

All materials stored on-site will be stored in a neat, orderly manner in their appropriate containers and, if possible, under a roof or other enclosure.

Products will be kept in their original containers with the original manufacturer's label. Substances will not be mixed with one another unless recommended by the manufacturer. Whenever possible, all of a product will be used up before disposing of the container.

Manufacturer's recommendations for proper used and disposal will be followed.

The site superintendent will inspect daily to ensure proper use and disposal of material on-site.

Hazardous Products

The following practices will reduce the risks associated with hazardous materials (e.g. petroleum products, solvents, etc.):

- Products will be kept in original containers unless they are not resealable.
- Original labels and material safety data sheets (MSDS) will be retained; they contain important product information.
- A copy of the Material Safety Data Sheet (MSDS) for each product used in construction will be kept in the job trailer.
- If surplus product must be disposed of, manufacturer' or local- and state-recommended methods for proper disposal will be followed.

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Product Specific Practices

Petroleum Products: All on-site vehicles will be monitored for leaks and will receive regular preventative maintenance to reduce the chance of leakage. Petroleum products will be stored in tightly sealed, clearly labeled containers. Any asphalt substances used on-site will be applied according to the manufacturer's recommendations. No vehicle refueling or maintenance will take place within 100 feet of a wetland or waterway. No petroleum-based or asphalt substances will be stored within 100 feet of a wetland or waterway.

Fertilizers: Fertilizers used will be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer will be worked into the soil to limit exposure to stormwater. Unused fertilizer will be stored in a covered shed. The contents of any partially used bags of fertilizer will be transferred to a sealable plastic bin to avoid spills. No fertilizers will be stored within 100 feet of a wetland or waterway.

Solvents, Paints and Other Hazardous Substances: All containers will be tightly sealed when not required for use. Excess material will not be discharged to the storm sewer system but will be properly disposed of according to manufacturers' instruction or local and state regulations. No solvents, paints or other hazardous substances will be stored within 100 feet of a wetland or waterway.

Concrete Trucks: Concrete trucks will not be allowed to wash out or discharge surplus concrete or drum wash water on the site.

Spill Control Practices

In addition to the good housekeeping and material management practices discussed in the previous sections of this plan, the following practices will be followed for spill prevention and cleanup:

- Manufacturers' recommended methods for spill cleanup will be clearly posted and site personnel will be made aware of the procedures and the location of the information and cleanup supplies.
- Materials and equipment necessary for spill cleanup will be kept in the on-site material storage area. Equipment and materials will include, but is not limited to, brooms, dust pans, mops, rags, gloves, goggles, kitty litter, sand, sawdust and plastic and metal trash containers specifically for this purpose.
- All spills will be cleaned up immediately after discovery.
- The spill area will be kept well ventilated and personnel will wear appropriate protective clothing to prevent injury from contact with a hazardous substance.
- Spills of toxic or hazardous material will be reported, regardless of size, to the Massachusetts Department of Environmental Protection at 888-304-1133.
- Should a spill occur, the spill prevention plan will be adjusted to include measures to prevent another spill and to cleanup up the spill should another occur. A description of

the spill, along with the causes and cleanup measures will be included in the updated spill prevention plan.

• The construction superintendent responsible for daily operation on the construction site will be the spill prevention and cleanup coordinator. The superintendent will designate at least three site personnel to receive spill prevention cleanup and training. These individuals will each become responsible for a particular phase of prevention and cleanup. The names of responsible spill personnel will be posted in the material storage area and in the on-site job trailer.

November 11, 2008 DERAL, STATE AND LOCAL

CERTIFICATION OF COMPLIANCE WITH FEDERAL, STATE AND LOCAL REGULATIONS

This stormwater pollution prevention plan reflects State of Massachusetts requirements for stormwater management and sediment and erosion control as established by the *Wetlands Protection Act* (310 CMR 10.00) and by the Department of Environmental Protection *Stormwater Management Policy*. To ensure compliance, this plan was prepared in consultation with the following publications:

Commonwealth of Massachusetts, Department of Environmental Protection. *Stormwater Management Policy*. November 1997.

Commonwealth of Massachusetts, Department of Environmental Protection. Wetlands Protection Act Regulations: 310 CMR 10.00 for Administering M.G.L. Chapter 31, Section 40. November 1997.

Commonwealth of Massachusetts, Department of Environmental Protection and Office of Coastal Zone Management. *Stormwater Management, Volume One: Stormwater Policy Handbook.* March 1997.

Commonwealth of Massachusetts, Department of Environmental Protection and Office of Coastal Zone Management. *Stormwater Management, Volume Two: Stormwater Technical Handbook*. March 1997.

United States Environmental Protection Agency. Storm Water Management For Construction Activities, Developing Pollution Prevention Plans And Best Management Practices, Summary Guidance. October 1992.

POLLUTION PREVENTION PLAN CERTIFICATION

I certify under penalty of law that this document and all attachments were prepared under my direction in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Signed: _____

CONTRACTOR'S CERTIFICATION

I certify under penalty of law that I understand the terms and conditions of the general National Pollutant Discharge Elimination System (NPDES) permit that authorizes the stormwater discharges associated with industrial activity from the construction site identified as part of this certification.

Signature	Company	Responsible For
	Tel:	
	Tel:	
	Tel:	

SWPPP-INSPECTION AND MAIN, ENANCE REPORT FORM

Northern Avenue

STORMWATER POLLUTION PREVENTION PLAN INSPECTION AND MAINTENANCE REPORT FORM

Northern Avenue

Inspection Schedule: FORM TO BE COMPLETED EVERY 7 DAYS (General Permit Section 3.10 Inspections)

Inspector:

Date:

Time:

Inspector's Qualifications:

Days Since Last Rainfall:

Amount of Last Rainfall (inches):

STABILIZATION MEASURES

Area of Site	Date Since Last Disturbed	Date of Next Disturbance	Stabilized? (Yes/No)	Stabilized With	Condition
Access Drive					

Stabilization Required:

To Be Performed By:

STRUCTURAL CONTROLS

Entrance Tracking Pad

Is Sediment Tracking Pad Catching Sediment Before Collector Road	Is Gravel Clean or Filled With Sediment	Is Tracking Pad Width and Length Adequate to be Effective	Does Tracking Pad Require Replacement/Maintenance

Maintenance Required:

To Be Performed By:	On or Before:

.

SWPPP-INSPECTION AND MAIN LENANCE REPORT FORM

СВ	Is Surface Runoff Being Directed to Catch Basins Properly	Are Sediment Traps Installed at Catch Basin Inlets	Are Catch Basin Outlet Hoods Installed and Working Properly	Depth of Sediment in Basin Sump	Are Any Correction Measures Required
CB#1					
CB#2					-
CB#3					
CB#4					
CB#5					
CB#6					
CB#7					
	· ·				

Catch Basins

Maintenance Required:

To Be Performed By:

On or Before:

STRUCTURAL CONTROLS -CON'T

Stormwater Treatment Chambers

SWTC	Is Surface Runoff Being Directed Through SWTC Properly	Depth of Sediment in Basin Sump	Are Any Correction Measures Required
SWTC #1		······································	

Maintenance Required:

To Be Performed By:	On or Before:

Bioretention Area/ Infiltration Trench

Structure	Is Structure Working Properly	Depth of Sediment in Structure	Are Any Correction Measures Required	Additional Notes
Rain Garden				
Infiltration Trench				

Maintenance Required:

To Be Performed By:	On or Before:	

Stormwater Detention Basin 1

Is Stormwater Entering Basin Correctly	Is Stormwater Being Detained and Discharged Properly	Depth of Sediment in Spreader	Is Rip-Rap Stabilization Properly Installed & Maintained	Is There Any Evidence of Erosion Or unintended Flow Patterns

Maintenance Required:

To Be Performed By:	On or Before:	

Stormwater Detention Basin 2

Is Stormwater Entering Basin Correctly	Is Stormwater Being Detained and Discharged Properly	Depth of Sediment in Spreader	Is Rip-Rap Stabilization Properly Installed & Maintained	Is There Any Evidence of Erosion Or unintended Flow Patterns

Maintenance Required:

To Be Performed By:	On or Before:

a

OTHER CONTROLS

List Other Miscellaneous Controls and Observations

Item	Describe Failure/Inadequate Control	Describe Recommended Remedy
		<u>}</u>

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RECOMENDED MODIFICATION(S) TO SWPPP

CHANGES REQUIRED TO THE POLLUTION PREVENTION PLAN

REASONS FOR CHANGES:

MISCELLANEOUS COMMENTS:

INSPECTOR'S CERTIFICATION:

Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete.

Signature:	Date:	

TRAFFIC IMPACT STUDY North Street Condos Northampton, MA

Kohl Construction Hadley, MA

October 14, 2008



-

Fuss & O'Neill, Inc. 78 Interstate Drive West Springfield, MA 01089



TRAFFIC IMPACT STUDY Proposed Retail Development Great Barrington, MA

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TRAFFIC IMPACT STUDY Proposed Retail Development Great Barrington, MA

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Intersection Capacity Analysis Worksheets - Weekday Afternoon Peak Hour



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SUMMARY SHEET

As an aid to reviewers, this Summary Sheet has been included to outline the various study parameters utilized in this report. Although a full explanation of the study methodologies is included in the text of the report, this summary can serve as a useful reference for reviewers.

<u>APPLICANT</u>: Kohl Construction

<u>DEVELOPMENT SIZE/TYPE</u>: 25 Units - Residential Condominium/Townhome

<u>APPLICATIONS</u>: City of Northampton Planning Board

BUILD YEAR: 2013 (2008 +5 years)

BACKGROUND TRAFFIC GROWTH FACTOR: 1% - based on available MassHighway continuous count data

<u>TRAFFIC COUNTS</u>: Data Inc. – October 1, 2008 (Turning Movement Counts) Data Inc. – October 1-2, 2008 (Automatic Traffic Recorders)

<u>PEAK HOURS ANALYZED</u>: Morning Peak Hour – 8:00am to 9:00am Afternoon Peak Hour – 4:15pm to 5:15pm

<u>EXPECTED TRIP GENERATION</u>: Morning Peak Hour – 17 total trip ends Afternoon Peak Hour – 19 total trip ends

<u>CAPACITY ANALYSIS</u>: Technique – 2000 Highway Capacity Manual Execution – Synchro Professional Software, Version 7.0

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1.0 INTRODUCTION

1.1 <u>Purpose of Report and Study Objectives</u>

The following report summarizes the site traffic impact assessment for the development of condominium/townhomes on North Street and Northern Avenue in Northampton. The proposed development will be composed of 25 new dwelling units. This report presents the results of a field investigation, traffic counts, and analysis of the estimated traffic to be generated by the proposed project.

1.2 Project Overview

The proposed redevelopment site is located northeast of downtown Northampton. The proposed condominium/townhomes will be located on the northwest side of North Street. Twenty-three units will access North Street via View Avenue, a private way and a proposed driveway also accessing North Street. Two of the units will be located at the end of Northern Avenue. The parcel is currently undeveloped.

The study area is primarily a residential area surrounding North Street. North Street connects King Street, on the east end to Bates Street and Day Avenue, on the west end. This study focused on the intersections and driveway used by the proposed development and major intersection at either end of North Street, where new trips will be most concentrated.

2.0 EXISTING CONDITION

2.1 <u>Site of Development</u>

A locus map of the site location and the surrounding area is provided in <u>Appendix B, Figure 1</u>. The property is zoned Urban Residential. Existing land uses surrounding the study area are:

- Single and Multi-Family housing surrounding the site.
- o Industrial Park to the northeast
- o Central Business District of Northampton to the southwest

Currently the proposed location for the condominium/townhomes is undeveloped.

2.2 Adjacent Roadway Network

The study area of influence includes North Street and Northern Avenue that provide access to the site and the surrounding roadway network.

North Street is a collector roadway that runs northeast-southwest through the study area. Pavement width for North Street is 26 feet in the vicinity of the site. North Street is a 2-lane roadway, without lane delineation, which is under the jurisdiction of the City of Northampton. At the time the traffic count was conducted North Street carried an average daily traffic (ADT) of approximately 4,025 vehicles per day in the vicinity of the site.



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Northern Avenue is a dead-end local road under the jurisdiction of the City of Northampton. Pavement width is 20 feet, which includes approximately 8 feet used for on-street parking on the northeast side of the street.

The PVTA does not have a bus route directly passing the site on North Street. There are bus stops within a half mile of the site, however. Sidewalks are provided on both North Street and Northern Avenue.

2.3 <u>Study Area Intersections</u>

The intersections analyzed for this study consist of the following:

- 1. King St (Route 5) / North Street
- 2. North Street / Market Street
- 3. North Street / Northern Avenue
- 4. North Street, Bates Street and Day Avenue

The intersection of King Street, Summer Street and North Street is signalized and actuated with 2 phases. The southbound approach has two lanes, a through lane and a shared through/left turn lane. The northbound approach has a through lane and right turn lane. The eastbound approach, Summer Street, is one-way entering the intersection with a left lane and a shared through/right turn lane. The westbound approach, North Street, has a shared left/right turn lane.

The intersection of North Street and Market Street is one-way stop sign controlled. The eastbound approach, North Street, is stop controlled and has a shared right/left turn lane. The north and southbound approaches are free flowing. The southbound approach, North Street, operates with a through lane and right turn lane. The northbound approach, Market Street, has a single shared left turn/through lane.

The intersection of North Street and Northern Avenue is one-way stop sign controlled. The North Street moves are free flowing while Northern Avenue is stop controlled. Each approach has a single lane shared for all related moves.

The intersection of North Street, Bates Street and Day Avenue is three-way stop controlled. Each approach has a single lane shared for all movements.

2.4 Traffic Volumes, and Counts

The greatest potential for traffic impact on the roadway network by the proposed development will occur during the weekday morning and afternoon peak hour, the period when traffic demand on North Street is typically at its highest level. In order to determine the traffic impact of the proposed development on adjacent street traffic, weekday morning and afternoon peak period manual turning movement counts were conducted in October at the four existing intersections in the study area. The traffic count data collected indicates that the weekday morning peak hour is 8:00am to 9:00am and the afternoon peak hour is 4:15pm to 5:15pm.



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These peak hours was subsequently analyzed for impacts. The existing traffic volumes for these peak hours are shown in <u>Appendix C</u>.

24 hour automatic traffic recorder data was also collected on October 1-2, 2008 on North Street southeast of Northern Avenue. Copies of the ATR traffic data are included in <u>Appendix D</u> of this report.

3.0 BACKGROUND TRAFFIC CONDITIONS

3.1 Growth Rate and Analysis Periods

The proposed project is expected to be completed and fully occupied before the year 2013 (five year projection). Future traffic conditions were estimated by applying a growth factor to all peak hour turning movement traffic volumes to account for regional growth characteristics such as other developments, increasing population, vehicle ownership, workers per household and increased travel mileage. In order to determine a reasonable growth rate for the background traffic volumes within the study area, count data were obtained from MassHighway for Routes 5 and 10 in the vicinity of the site for the years 2002 through 2006.

The count data showed an overall decline in traffic volume over the period data was recorded. Therefore, a growth factor of 1% increase was assumed for this study to be conservative. The data also indicated the month of October has higher than average month traffic volumes. The count data for this study was not adjusted (lower) for the average month.

3.2 <u>Background Developments</u>

There were no other programmed developments anticipated to be completed during the analysis period that would impact traffic within the study area at the time of this study.

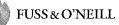
3.3 Estimated Volumes

The raw count data for each of the count location were graphically applied to the study area network. The resulting volumes are used as the Base conditions for the traffic estimates. The weekday morning and afternoon 2008 Base condition traffic volume estimates are given in <u>Appendix B, Fig 2</u>. To determine the estimated traffic volumes at the time the project is expected to be fully constructed and occupied the base 2008 volumes were increased with a 1% growth rate for five years to year 2013. This volume estimate provides the 2013 No-Build condition. The weekday morning and afternoon 2013 No-Build condition traffic volume estimates are given in <u>Appendix B, Fig 3</u>.

4.0 PROPOSED CONDITIONS

4.1 Development and Site Access

The proposed development consists of 25 condominium/townhomes. The units are attached in groups with between 2 and 6 units in each group. Seventeen of the dwelling units will have attached garages plus driveway parking space. The remaining units will have driveway surface parking areas and additional visitor parking areas are provided throughout the site.



Two units are isolated on Northern Avenue and will have a driveway at the end of the street. The other 23 units will access the site to and from North Street via two existing private right-ofways to access North Street. The existing right-of-ways will be reconstructed to accommodate site traffic. The first is an unaccepted street View Avenue. View Avenue will serve as both an entrance and exit to the site. The second is a gravel driveway located between Northern Avenue and View Avenue. The on site portion of this driveway will be restricted to one-way exiting the site only.

4.2 <u>Trip Generation</u>

The expected site generated traffic volume was calculated using existing empirical data from the Institute of Transportation Engineers (ITE) publication <u>Trip Generation</u>, 7th edition, 2003. This publication is an industry-accepted resource for determining trip generation.

Trip generation estimated for the proposed developments were estimated based on the total number of proposed dwelling units. The land use for this development is LUC: 230 Residential Condominium/Townhome.

Based on ITE rates the proposed development is estimated to produce 198 new vehicle trips over a typical 24-hour period on weekdays. During the Weekday Morning peak hour the proposed development is estimated to generate 17 new trips and 19 new trips during the Weekday Afternoon peak hour. <u>Table 1</u> presents the daily weekday trip estimates and weekday afternoon trip estimates.

	TABLE 1 l Condominium/Townhou	20
		se
Development 11	ip Generation Estimates	
	N	Jew Vehicle Trips
Weekday (24 Hour)		
	Entering:	99
	Exiting:	99
	Total:	198
Weekday AM Peak Hour of Adjacent Street Ti	affic Entering: Exiting:	3 14
	Total:	17
Weekday PM Peak Hour of Adjacent Street Tr		
Weekday PM Peak Hour of Adjacent Street Tr	Entering:	13
Weekday PM Peak Hour of Adjacent Street Tr		13

4.3 <u>Trip Distribution</u>



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The distribution of new trips accessing the site was applied to the local road network based on consideration of the existing local traffic distribution and the layout of the adjacent roadway network. Arrival and departure distributions of site traffic were first estimated based on existing patterns at Northern Avenue and then subsequent intersection to the limits of the study area. The estimated trips were split between the three access points to the site the Site Driveway, View Avenue and Northern Avenue. The splits were based on the internal circulation and site layout. The one-way driveway will serve 52% of the trips leaving the site. View Avenue will serve 40% of the trips leaving the site and 92% of the trips entering the site. The two units on Northern Avenue comprise about 8% of the site traffic entering and leaving.

4.4 <u>Combined Volumes</u>

The 2013 Build condition traffic estimates were calculated by adding the site traffic to the projected No-Build traffic volumes. The 2013 Build condition traffic volumes are given in <u>Appendix B, Figure 4</u>. The estimated trip generation and trip distribution used for determining the Build condition traffic volumes are included in <u>Appendix B, Figure 3</u>.

5.0 ANALYSIS

5.1 Accident Review

An analysis to determine crash rate per intersection was prepared to review the level of safety at the study area intersections. Accident data was obtained from MassHighway for each of the study area intersections. The records were gathered for the most recent 3 years of available data, 2004 through 2006. The crash rates, expressed as "crashes per Million Entering Vehicles" (MEV), were determined using the turning movement counts and average number of crashes during the three-year period. A summary of the accident data and resulting crash rates is provided in <u>Appendix A, Table A-1</u>.

The crash rate is a measurement used by MassHighway that compares the number of crashes to the number of vehicles passing through a particular intersection. A crash rate at or below the regional average for a similar facility is an indication that there is likely no unusually hazardous condition or predominant safety factor influencing the frequency of crashes at a location. The crash rates were determined to be below the District 2 average with the exception of the King Street, Summer Street and North Street intersection. The elevated experience on King Street could be a result of the lack of a separate southbound left turn phase and also the offset east and west legs of the intersection.

5.2 Intersection Capacity Analyses

Capacity analyses for both signalized and un-signalized intersections were conducted using Synchro Professional Software, version 7.0.

Level of Service has been determined by the methodology of the "2000 Highway Capacity Manual" published by the Transportation Research Board to describe the operating condition of an intersection. LOS is a measure of the Control Delay experienced by stopped vehicles at an intersection, which is rated on a scale from A to F, with each letter grade assigned a range of delay values in seconds per vehicle. LOS A describes a free flowing condition of very low delay



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(less than 10 seconds per vehicle), and LOS F describes a congested condition where delays will exceed 50 seconds per vehicle at an unsignalized intersection. Control Delay measures the time accumulated when a motorist approaches an intersection including the initial deceleration, queue move-up time, stopped delay, and final acceleration delay. Therefore, intersections with longer Control Delay times are less acceptable to most drivers.

For unsignalized intersection capacity analyses, LOS provides a description of the delay and operational characteristics of the movements from the minor street (usually stop sign controlled) and left turns from the major street into the minor street. Major street through and right turn vehicles typically experience very little delay. Therefore, they are not rated with a LOS at unsignalized intersections.

Using the above referenced methodologies, weekday morning and afternoon peak hour capacity analyses were conducted at the <u>signalized</u> intersection of King Street (U.S. Route 5 and State Route 10), Summer Street and North Street.

Weekday morning and afternoon peak hour capacity analyses were also conducted at the following <u>un-signalized</u> intersections:

- North Street and Market Street
- North Street & Northern Avenue
- North Street, Bates Street and Day Avenue
- o North Street & View Avenue
- North Street & the Site Driveway

Existing (2008) and Future No Build (2013) Capacity Conditions:

During the weekday morning and afternoon peak hours the LOS at the signalized intersection of King Street, Summer Street and North Street will be LOS C or better. The exception is the westbound approach from North Street. The morning peak hour is expected to operate at LOS E under the No-Build condition. The afternoon peak hour is expected to operate at LOS D under the No-Build condition.

During the weekday morning and afternoon peak hours the LOS at the unsignalized intersections will be LOS C or better under both the Base and No-Build conditions. The exception is the westbound approach from North Street.

Build (2013) Capacity Conditions:

During both the morning and afternoon peak hours the added site traffic is not expected to result in changes to the LOS. Slight increases in delay from site traffic are not significant enough to decrease the LOS letter grade. The new site accesses at View Avenue and the Site driveway will operate at LOS B or better under the Build condition.

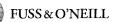
The summarized results of the capacity analysis are provided in <u>Tables 2 - 5</u>. The capacity analysis worksheets are provided in <u>Appendices E & F</u>.

		2008 E	xisting	2013 Bu	- • •	2013 Build	
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS
King Street (U.S. Route 5) &	k North Street/Su	immer Street					
Summer Street	EB L	24.8	С	24.5	С	24.4	С
	EB T/R	24.4	С	24.1	С	24.1	C
North Street	WB L/R	52.8	D	60.6	Е	65.2	Е
King Street	NB T	9.0	А	9.8	А	10.0	А
	NB R	6.3	А	6.7	А	6.8	А
	SB L/T	9.3	А	10.2	В	10.4	В
OVERALL		20.5	С	22.7	С	24.0	С

TABLE 2 WEEKDAY MORNING PEAK HOUR INTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

TABLE 3WEEKDAY MORNING PEAK HOURUNSIGNALIZED INTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

· · · · · · · · · · · · · · · · · · ·		2007 E:	xisting	2013 Bu		2013 H	Build
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS
North Street & Market Stree	et						
North Street	EB L/R	17.5	С	19.3	С	19.7	С
Market Street	NB L	6.5	А	6.6	Α	6.6	Α
North Street & Northern Av	venue						
North Street	NB L/T	0.2	А	0.2	Α	0.2	А
Northern Avenue	EB L/R	9.7	A	9.7	А	9.9	А
North Street & Bates Street	/Day Avenue						
North Street	NB L/R	8.5	А	8.7	Α	8.7	А
Bates Street	EB T/R	9.4	А	9.6	Α	9.6	Α
Day Avenue	WB L/T	8.4	А	8.6	А	8.6	Α
North Street & View Avenue	e						
View Avenue	EB L/R	-	-	-	-	10.0	А
North Street	NB L/T	-	-	-	-	0.1	Α
North Street & Site Drivewa	ıy						
	EB L/R	<u> </u>			-	9.9	A



	· · · · · · · · · · · · · · · · · · ·	2008 E	xisting	2013 Bu	- • •	2013 Build		
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS	
King Street (U.S. Route 5 ar	nd Route 10) & N	orth Street/S	ummer			[
Street								
Summer Street	EB L	37.5	D	35.0	С	34.6	С	
	EB T/R	23.0	С	22.6	С	22.6	С	
North Street	WB L/R	44.4	D	48.8	D	49.1	D	
King Street	NB T	8.1	А	9.0	А	9.1	Α	
	NB R	5.0	А	5.4	А	5.5	А	
	SB L/T	7.4	А	8.5	А	8.6	А	
OVERALL		19.1	В	20.8	С	21.0	С	

TABLE 4WEEKDAY AFTERNOON PEAK HOURINTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

TABLE 5WEEKDAY AFTERNOON PEAK HOURUNSIGNALIZED INTERSECTION CAPACITY ANALYSIS: LEVEL OF SERVICE SUMMARY

		2008 E:	xisting	2013 Bu		2013 Build	
Intersection	Movement	Delay	LOS	Delay	LOS	Delay	LOS
North Street & Market Stree	et						
North Street	EB L/R	18.9	С	21.1	С	21.1	С
Market Street	NB L	7.7	А	7.8	А	7.8	А
North Street & Northern Av	venue						
North Street	NB L/T	0.3	А	0.3	Α	0.3	А
Northern Avenue	EB L/R	10.5	В	10.7	В	10.7	В
North Street & Bates Street,	/Day Avenue						
North Street	NB L/R	8.0	А	8.0	А	8.1	А
Bates Street	EB T/R	10.6	В	11.0	В	11.1	В
Day Avenue	WB L/T	8.4	А	8.5	А	8.6	А
North Street & View Avenue	e						
View Avenue	EB L/R	-	-	-	-	10.9	В
North Street	NB L/T	-	-	-	-	0.3	А
North Street & Site Drivewa	ıy	1					<u></u>
	EB L/R		-		-	10.8	B



5.3 <u>Findings</u>:

With regard to impacts due to added site traffic, there will not be a noticeable impact to operation at the existing intersections. The two proposed site accesses, View Avenue and the Site Driveway, will operate safely and efficiently.

Sight distance viewing to the north and south along North Street at both proposed access points, View Avenue and the Site Driveway, is adequate.

6.0 CONCLUSIONS AND RECOMMENDATIONS

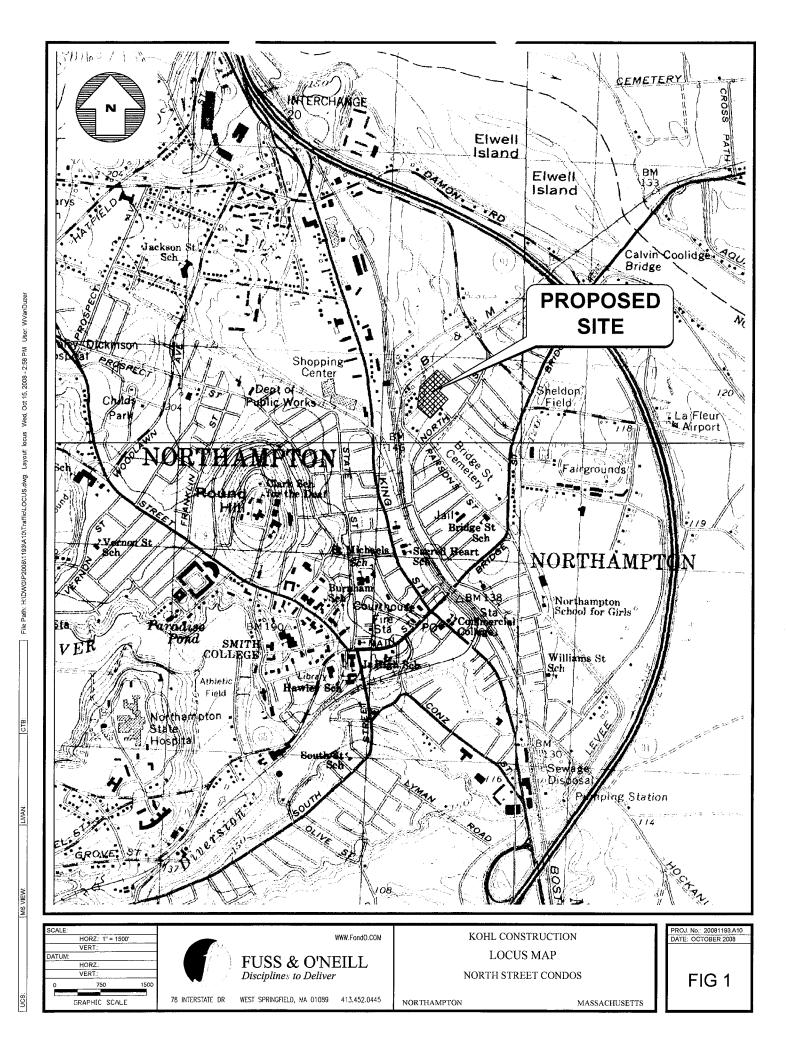
The study indicates that completion and occupancy of the proposed development will generate 17 new entering and exiting vehicle trips per hour at the site during the weekday morning peak and 19 new entering and exiting vehicle trips per hour in the weekday afternoon peak.

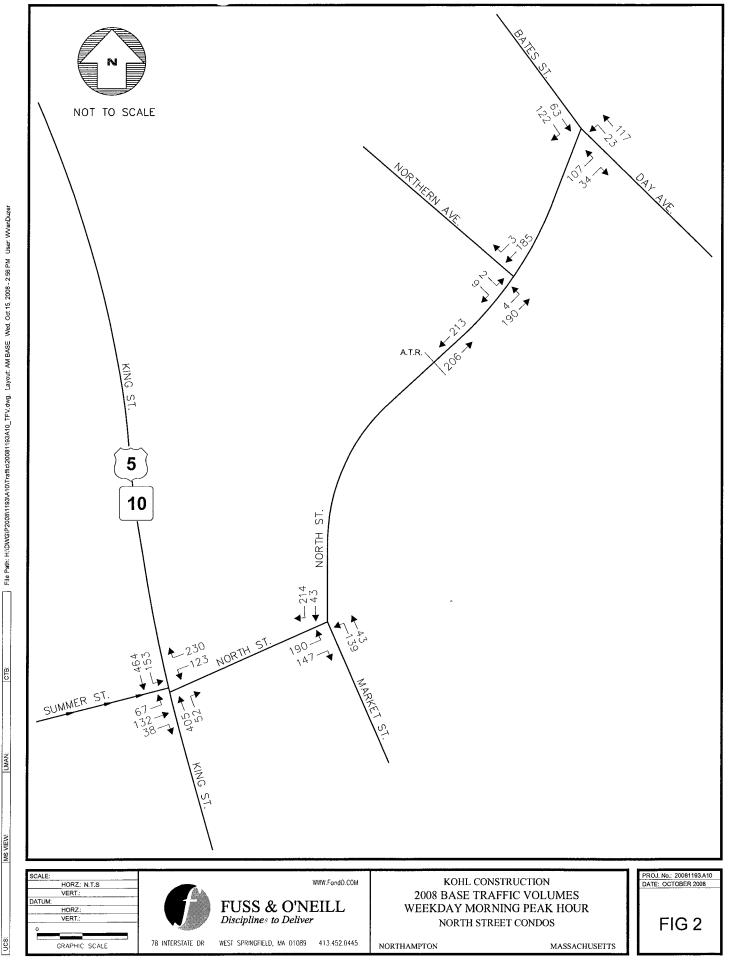
The additional traffic generated by the proposed project will result in incremental increase in peak period traffic volumes on North Street that will have minimal impact on traffic operations. The site access intersections with North Street are designed to provide safe and efficient traffic operations and the turning movements can be accommodated without consideration of off-site improvements.

TABLE A-1 ACCIDENT DATA SUMMARY - 2004 THROUGH 2006 STUDY AREA INTERSECTIONS

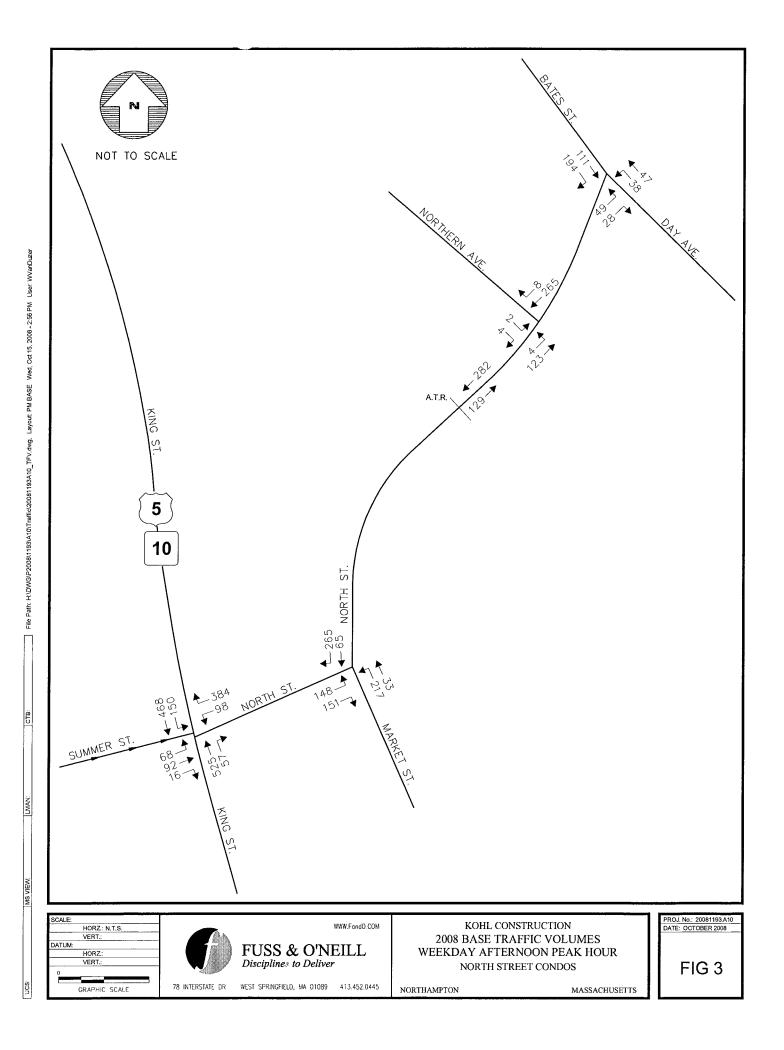
Criteria	Summer Street, North Street and King Street	North Street and Market Street	North Street and Northern Ave	Bates Street, North Street and Day Ave
YEAR				
2004	9	1	0	0
2005	16	2	0	0
2006	4	Q	Q	Q
Total	29	3	0	0
Average No. of Crashes	9.67	1.00	0.00	0.00
Crash Rate	1.43	0.31	0.00	0.00
TYPE				
Angle	13	2	0	0
Rear-End	7	0	0	0
Head-On	0	0	0	0
Sideswipe	3	0	0	0
Unknown/Other	<u>6</u>	1	Q	<u>0</u>
Total	29	3	0	0
SEVERITY				
Property Damage Only	19	2	0	0
Non-fatal Injury	9	1	0	0
Fatality	0	0	0	0
Unknown/Other	1	Q	Q	Q
Total	29	3	0	0
WEATHER				
Clear	14	1	0	. 0
Rain	2	0	0	0
Snow/Ice	2	1	0	0
Clouds	9	1	0	0
Fog	0	0	0	0
Unknown/Other	2	Q	Q	Q
Total	29	3	0	0
TIME				
Weekday 7:30 AM - 9:30 AM	2	0	0	0
Weekday 3:30 PM - 5:30 PM	6	0	0	0
Other	21	<u>3</u>	٥	<u>0</u>
Total	29	3	0	0

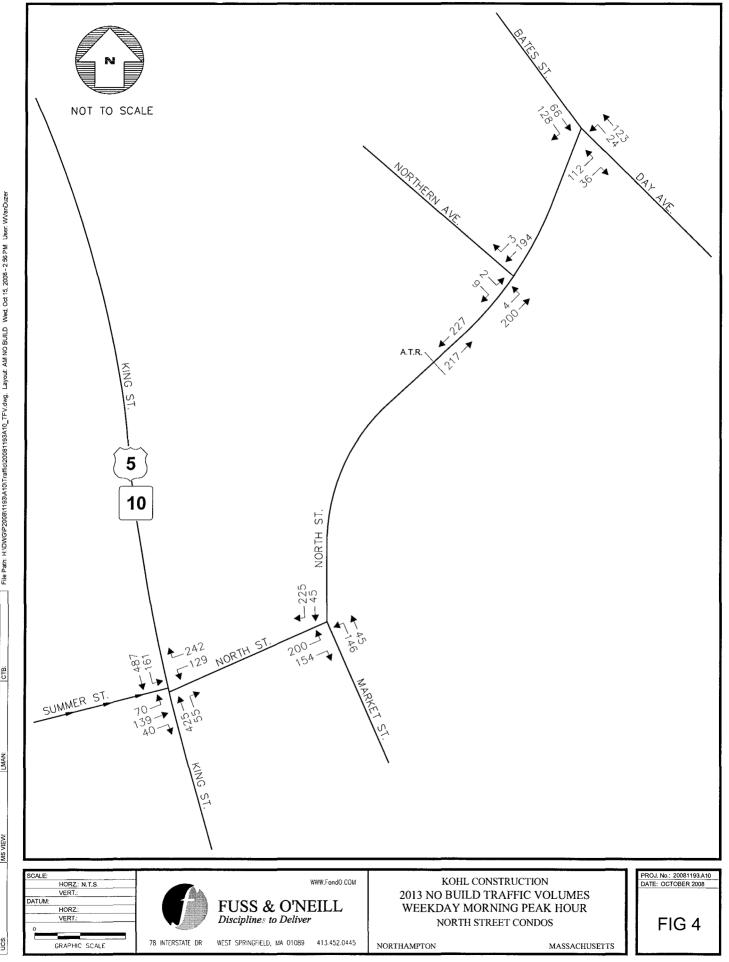
District #2 Average Crash Rates: 0.94 Signalized Intersections 0.85 Unsignalized Intersections





LMAN: MS VIEW:

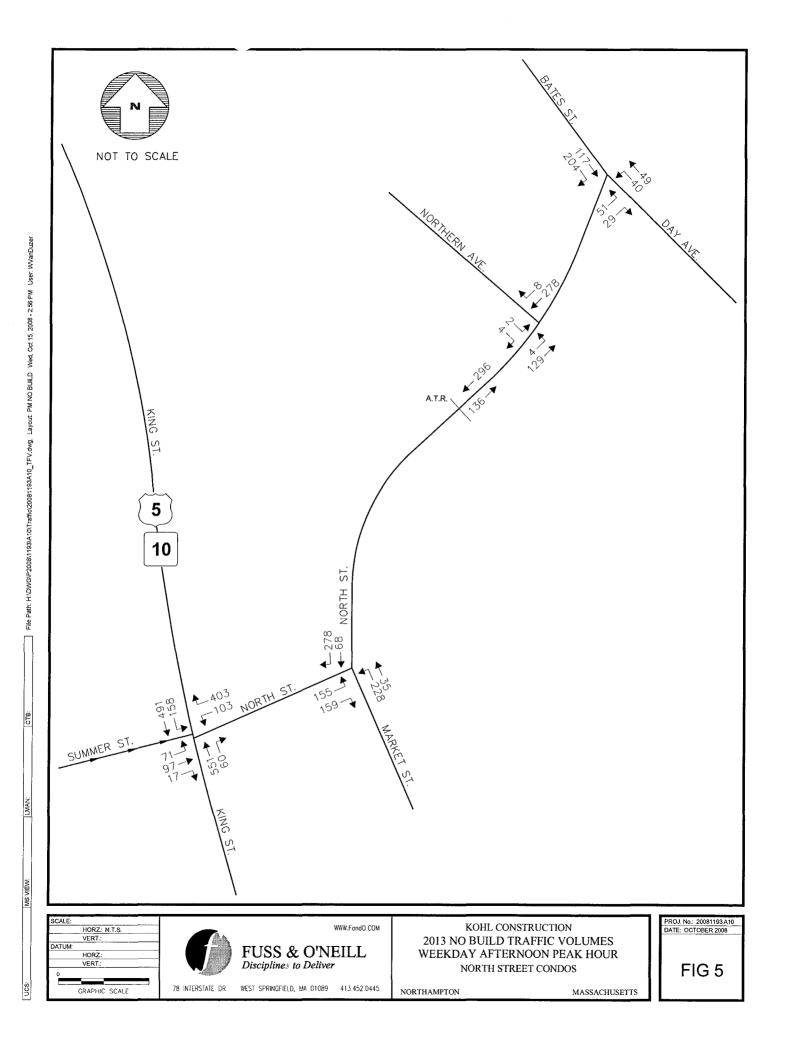


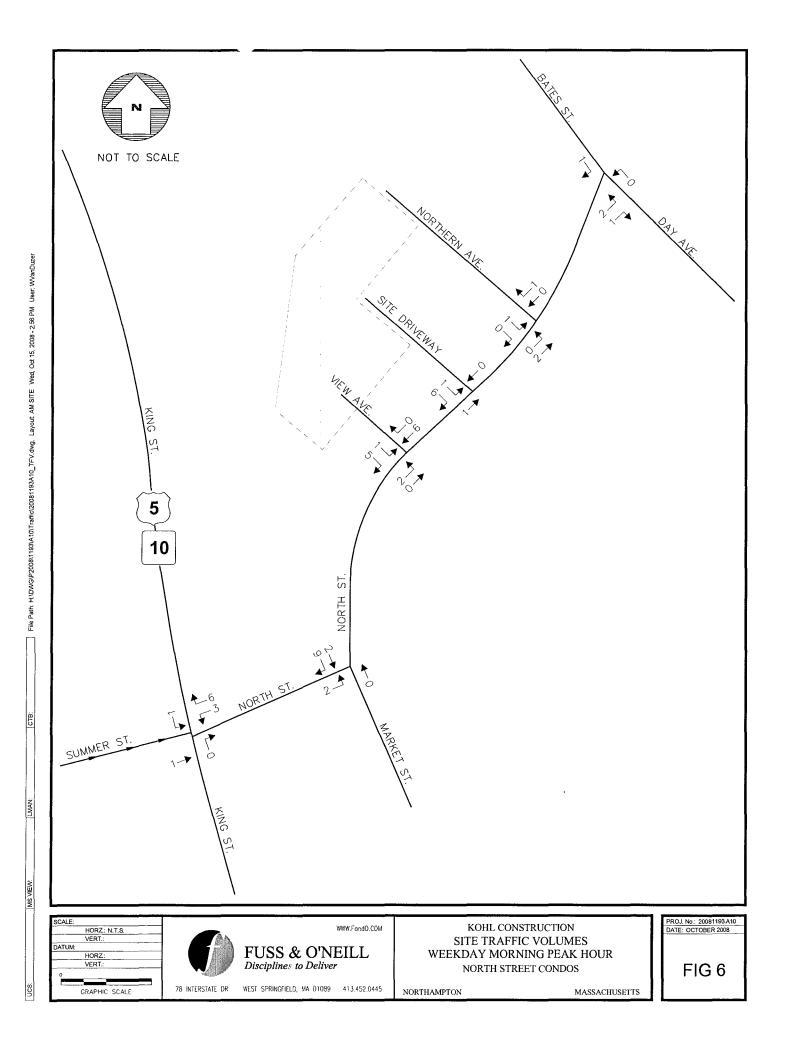


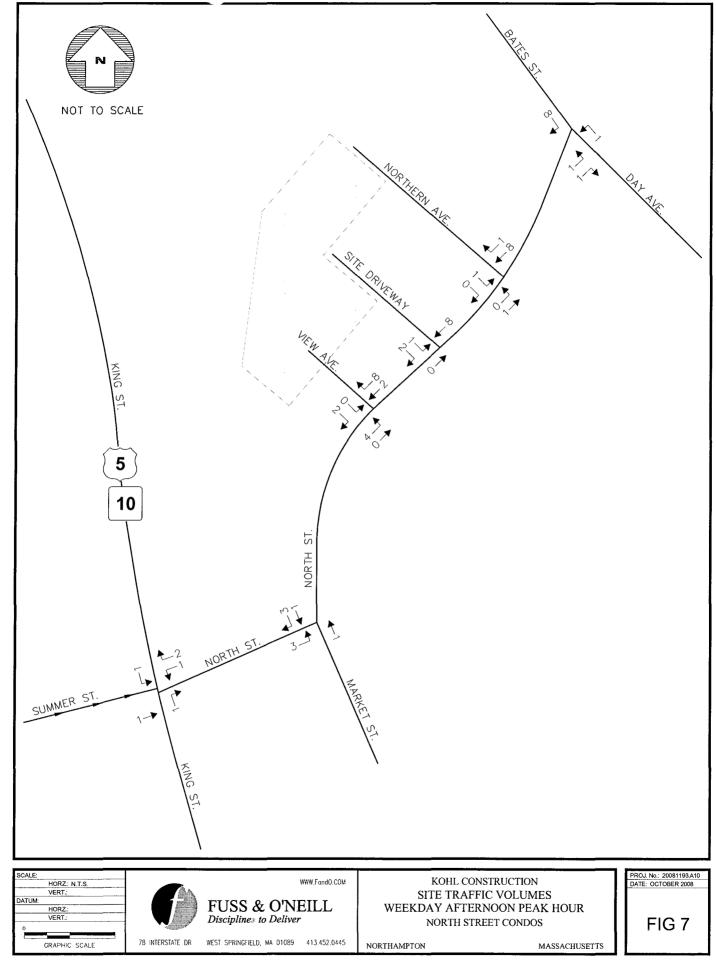
File Path: H1DWGP200811193A10TTraffic)20081193A10_TFV.dwg. Layout: AM NO BUILD Wed, Oct 15, 2008-256 PM User: WVanDizer

LMAN: MS VIEW:

NCS



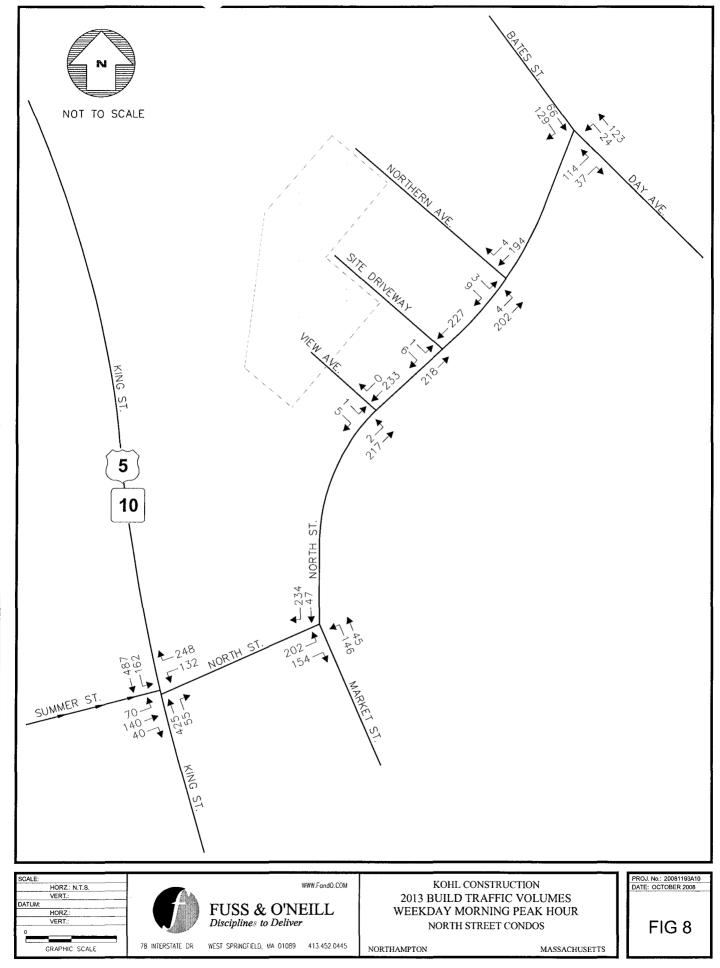




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CTB:

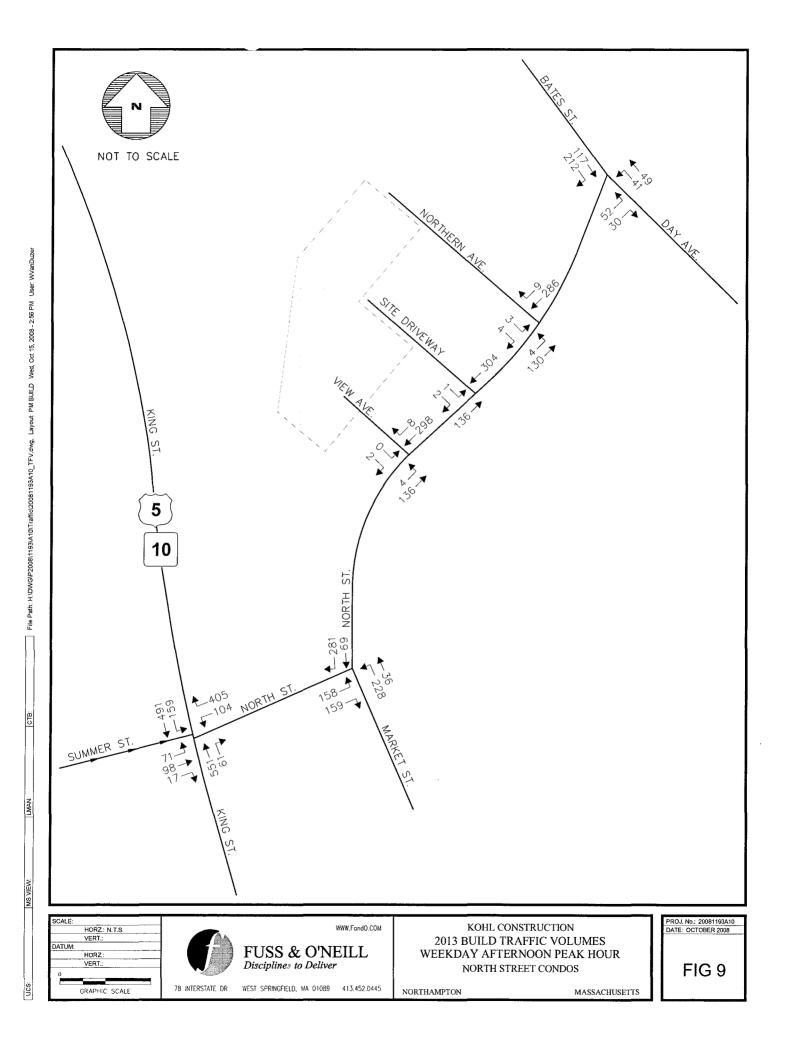
ucs



LMAN: CTB:

MS VIEW:

SOD



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Location 1: North Street Location 2: West of Northern Avenue

City, Sta	te: North	ampton	. MA										Site	Code: 1
Start	01-Oct-		bound	Northb	ound	Com	oined	02-Oct-	South	bound	Northb	ound	Comb	
Time	Wed	A.M.	P.M.	A.M.	P.M.	A.M.	P.M.	Thu	A.M.	P.M.	A.M.	P.M.	A.M.	P.M.
12:00		0	48	1	27	1	75		5	43	1	25	6	68
12:15		1	48	2	35	3	83		2	49	4	45	6	94
12:30		2	56	3	36	5	92		3	42	1	28	4	70
12:45		0	53	0	34	0	87		0	41	2	28	2	69
01:00		1	27	1	33	2	60		3	26	1	34	4	60
01:15		0	28	ò	29	ō	57		õ	36	O	23	Ó	59
01:30		ŏ	41	Ő	26	õ	67		1	29	1	26	2	55
01:45		0	31	1	36	1	67		2	35	· 1	27	-3	62
02:00		1	42	3	32	4	74		2	30	. 1	31	3	61
02:00		ò	31	ŏ	26	0	57		Ő	35	0	25	ŏ	60
02:13		0	44	2	33	2	77		1	38	0	23	1	66
02:30		0	37	0	38	Ő	75			40	1	36	2	76
02:45		0	56	0			97				. 1	46	1	95
		0			41	0	78	a se	0	49				95 81
03:15			49	0	29	0			1	46	2	35	3	
03:30		0	71	0	35	0	106	1.1.1.1.1.1	0	68	0	45	0	113
03:45		0	51	2	32	2	83	1	0	53	0	35	0	88
04:00		0	55	1	29	1	84		1	55	0	34	1	89
04:15		. 3	67	0	36	3	103		2	58	0	33	2	91
04:30		1	62	2	35	3	97		1	59	3	43	4	102
04:45		0	73	6	28	6	101	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	0	52	4	42	4	94
05:00		1	80	3	30	4	110		Q	77	7	41	7	118
05:15		2	51	7	36	9	87		1	64	8	47	9	111
05:30		1	62	6	25	7	87		3	54	7	38	10	92
05:45		3	54	3	31	6	85		2	53	1	35	3	88
06:00		1	32	6	28	7	60		3	38	4	29	7	67
06:15		8	30	8	28	16	58		9	44	13	33	22	77
06:30		7	25	9	18	16	43		9	35	13	34	. 22	69
06:45		9	26	14	11	23	37		8	23	17	26	25	49
07:00		12	19	20	15	32	34		10	24	17	18	27	42
07:15		16	14	26	18	42	32	1.1.4.	16	19	16	20	32	39
07:30		20	13	32	11	52	24		21	14	37	24	58	38
07:45		40	15	46	. 11	86	26		40	13	40	13	80	26
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08:30		. 46	8 i i i	62	11	108	25		44	14	55	18	99	32
08:45	· · · · ·	65		52	9	117	14		59	9	47	12	106	21
09:00	*	27	13	35	14	62	27		27	7	24	10	51	17
09:15		27	12	24	10	51	22		34	23	27		61	31
09:30		30	7	29	10	59	17		30	6	28	4	58	10
09:45		57	9	30	3	87	12	· .	24	9	25	3	49	12
10:00		45	3	31	3	76	6		32	3	23	1	55	4
10:00		29	8	33	6	62	14		25	. 3	23	4	49	7
10:15		29	4	24	4	53	8		29	6	24	4	43 51	10
10:30		32	4	34	43	66	· 7		32	4	28	9	60	13
									32 29			. 9		13
11:00		28	2	20	2	48	4			6	23		52	
11:15		22	3	27	6	49	9	1	18	6	32	1	50 76	7
11:30		36		30	2	66	3		48	2	28	4	76	6
11:45		45		26	1	71	4	L	51		22	5	73	
Total		749	1493	753	1016	1502	2509		728	1458	704	1148	1432	2606
Day		22	242	17	69	40	11		21	86	18	52	40)38
Total						10								
% Total		18.7%	37.2%	18.8%	25.3%				18.0%	36.1%	17.4%	28.4%		
Peak		08:00		08:00	02:45	08:00	04:15		08:00	04:30	08:00	04:30	08:00	04:30
Vol.		213		206	143	419	411		202	252	195	173	397	425
P.H.F.		0.819	0.881	0.831	0.872	0.895	0.934		0.856	0.818	0.886	0.920	0.936	0.900

ADT Not Calculated

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayoureguested.com

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

Site Code: 1 Southbound Start Time 5<u>5</u> Total 10/01/08 00:15 Ó 00:30 n 00:45 n 0 ŏ õ 01:00 õ ō 01:15 Ó 01:30 Ò ō Ó Ō Ō Ō 01:45 Ó 02:00 n 02:15 n. ñ 02:30 n n n n 02:45 n Õ 03:00 ō ō Ó ō ō 03:15 ō ō Ō 03:30 03:45 n 0 04.00 0 04:15 Ö ō õ ŏ ŏ n **n** 04:30 ŏ õ 04:45 Ó n n n 05:00 Ó 05:15 Ó 05:30 05:45 0 n ŏ 06:00 Ō 06:15 Ö Õ õ ō 06:30 Ò Ó 06:45 :0 Ô 07:00 Ò 07:15 07:30 Ó 88 07:45 13 10 21 15 Ô n £ £ n 08:00 20 08:15 ō Ō 08:30 Ō 08:45 13 Ó 27 30 09:00 09:15 n 09:30 ί0 o 35 62 14 15 09:45 n ō Ō Ō Ō 10:00 10:15 10:30 135 10:45 12 0 2 n 11:00 n n A n 11:15 õ 11:30 11:45 Total

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayoureguested.com

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

Southbound Site Code: 1 Start Time Total 17 12 PM 12:15 12:30 12:45 52 2 12 n 13:00 7 13:15 13:30 ŏ 13:45 14:00 14:15 Ò .31 14:30 n 61 14:45 -3 15:00 15:15 15:30 <u>15:45</u> 7 24 n 67 16:00 25 n ŏ 16:15 16:30 16:45 з 17:00 17:15 17:30 17:45 13 15 18:00 O 18:15 18:30 18:45 19:00 Ó 19:15 19:30 19:45 29 20.00 ō 20:15 20:30 Ó Ō 20:45 13 21:00 7 21:15 21:30 21:45 Ó 22:00 22:15 Ō Ó 22:30 22:45 n 23:00 23:15 23:30 Ó 0 / 23:45 Total

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Location 2: West of Northern Avenue City, State: Northampton, MA

Location 1: North Street

Data Acquisition, Transformation & Analysis, Inc. 50 Alden Avenue

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA 50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

tart	1	16	21	26	31	36	41	46	51	56	61	66	71	76	
me	15	20		30	35	40	45	50	55	60	65	70	75	999	Tota
2 PM	1	1	6	13	20	2	0	0	0	0	0	0		0	4
12:15	2	1	11	22	1.1	2	0	0	0	0	0	0	0	0	4
12:30	1	1	9	15	15	1	0	0	0	0	0	0	0	0	4
12:45	0		6	25	9	- 1	0	_0	0	0	0	0	0	0	
	4	3	32	75	55	6	0	0	0	0	0	0		0	11
13:00	0	- 1	1	18	3	3	0	0	0	0	-0	0	0	-0	
13:15	0	2	9	18	6	1	0	0	0	0	0	0	0	0	
13:30	0	1	4	14	8	0	1	1	0	0	0	0	0	0	
13:45	3	2		14	12	1	0	0	0	0	0	0		.0	
	3	6		64	29	5	1	1	0	0	0	0	0	0	1
14:00	0	1	7	16	6	0	0	0	0	0	0	0	0	0	
14:15	0	1	6	18	. 8	2	0	0	. 0	. 0	0	0	. 0	. 0	
14:30	2	0		13	14	4	0	0	0	0	0	0		0	
14:45	2	1	9	16	11	1	0	0	0	0	0		0	0	
45.00	4	3		63	39	7	0	0	0	0	0	0		0	1
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15:30	. 1	. 2		23	20	0	0	0	0	0	0	0		0	
13.43	5	10		<u>23</u> 96	57	8	0	0	0	0	0	0		0	
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16:15	5	1	23	20	. 7	1	0	-	i o	. 0	0	0	0	0	
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18:45	4	2		6	4	0	0	0	0	0	0	0		0	
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19:00	2	6		8	. 4	. 0	0	0	. 0	0	0	0	. 0	0	
19:15	1	4	8	4	2	0	0	0	0	0	0	0	0	0	
19:30	4	2	2	5	1	0	0	0	0	0	0	0	. 0	0	
19:45	0	2	5	5	1	0	0	0	0	0	0	0	0	0	
	7	14	19	22	8	0	0	0	0	0	0	0	0	0	
20:00	0	0	1	2	2	2	0	0	0	0	0	0	0	0	
20:15	0	0	2	4	0	0	0	0	0	0	0	- 0	0	Ó	
20:30	1	. 1	4	4	3	1	0	0	0	0	0	0	0	0	
20:45	0	1	3	4	11	0	0	0	0	0	0	0	0	0	
	1	2	10	14	6	3	0	0	0	0	0	0	0	0	
21:00	0	0	1	3	3	0	0	0	0	0	0	0		0	
21:15	0	1	4	6	11	1	0	0	0	0	0	0		0	
21:30	0	1	0	4	1	0	0	0	0	0	0	0		0	
21:45	0	0		4	5	0	0	0	0	0	0	0		0	
	0	2		17	20	1	0	0	0	0	0	0		0	
22:00	0	0		1	2	0	0	0	0	0	0	0		0	
22:15	0 -	0		2	0	-0	0	0	0	0	0	0	+	0	
22:30	0	0		1	1	0	0	0	0	0	0	0		0	
22:45	0	0		11	1	0	0	0	0	0	0	0		0	
	0	0		5	4	0	0	0	0	0	0	0		0	
23:00	0	1	1	2	2	0	0	0	0	-0	0	0		0	
23:15	0	1	0	2	3	0	0	0	0	0	0	0		0	
23:30	0	1		0	0	0	0	0	0	0	0	0		0	
23:45	0	1	1	2	0	1	0	0	0	0	0	0		0	
	0	4		6	5	1	0	0	0	0	0	0		0	
Total	70	98	345	588	314	41	1	1	0	0	0	0	0	0	1 1
Grand Total	177	222	1006	1833	1035	143	9	3	0	0	0	0	0	0	4

	85th Percentile :	33 MPH
	95th Percentile :	35 MPH
Stats	Mean Speed(Average) :	27 MPH
	10 MPH Pace Speed :	26-35 MPH
	Number in Pace :	2868
	Percent in Pace :	64.8%
	Number of Vehicles > 55 MPH :	0
	Percent of Vehicles > 55 MPH :	0.0%

Page 4

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

orthbou														OILC	Code
Start	1	16	21	26	31	36	41	46	51	56	61	66	71	76	
Time	15	20	25	30	35	40	45	50	55	60	65	5 70	75	999	Tot
0/01/08	0	1	0	0	0	0	0	0	C					0	
00:15	1	1	0	0	0	0	0		C					0	
00:30	0	0	1	1	1	0	0		C					0	
00:45	0	0	0	.0	0	0	0	0	<u>c</u>					0	
01:00	1 0	2	. 0	1	1 0	0	0 0	0	0					-0	
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Total	58	66	189	336	97	5	2		(0 0			

Page 5

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA 50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

orthboui	nd													Site	Code:
Start	1	16	21	26	31	36	41	46	51	56	61	66	71	76	
Time	15	20	25	30	35	40	45	50	55		65		75	999	Tota
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12:45	1.	3	8	19	2	1	0	0	0		0		0	0	3
	7	14	30	64	16	1	0	0	0		0		0	0	13
13:00	1	4	6	16	6	0	0	0	0		· 0		0	0	3
13:15	0	1	8	15	3	2	0	0	0		0		0	0	2
13:30	3	3	4	10	5	1	0	0	0		0		0	0	2
13:45	37	5	<u>10</u> 28	<u>13</u> 54	<u>5</u> 19	0	0	0	0		0		0	0	
14:00	1	13 3	28 17	54 9	19	3	0	0	0		0		0	0	12
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14:15	2	0	14	12	4	0	0	0	0		0		0	0	
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<u>, 17,70</u>	9	6	57	41	14	2	0	0	0		0		0	0	12
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	12	13	45	54	13	0	0	0	0	0	0	0	0	0	1
16:00	0	1	11	12	4	1	0	0	0	0	0	0	0	0	
16:15	2	4	15	9	3	3	0	0	0	0	0	0	0	0	
16:30	1	4	10	13	7	0	0	0	0		0		0	0	
16:45	3		9	10	5	0	0	0	0		0		0	0	
	6	10	45	44	19	4	0	0	0		0		0	0	1
17:00	4	4	8	11	3 .	0	0	0	0		0		0	0	
17:15	1	2	7	20	5	1	0	0	0		0		0	0	
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17:45	8	5	9	8	0	1	0	0	0		0		0	0	
40.00	15	12	34	45	14	2	0	0	0		0			0	1
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18:15	1	0	4	17	6	0	0	Ö	0		0		0	0	
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50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

Start	1	16	21	26	31	36	41	46	51	56	61	66	71	76	
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Data Acquisition, Transformation & Analysis, Inc. 50 Alden Avenue

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

Start	1	16	21	26	31	36	41	46	51	5	3	61	66	5 7'	1 76	
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Stats	Mean Speed(Average):	25 MPH
	10 MPH Pace Speed :	21-30 MPH
	Number in Pace :	2483
	Percent in Pace :	68.6%
	Number of Vehicles > 55 MPH :	0
	Percent of Vehicles > 55 MPH :	0.0%

Belchertown, Moren Avenue 888-389-9524 or www.dat

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA 50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Time Pikes Trailers Long Puses 6 Tire Single Double Double Double Multi Multi Multi Class 100:168 0 1 0 <t< th=""><th><u>outhbour</u> Start</th><th></th><th>Cars 8</th><th>2 Axle</th><th></th><th>2 Axle</th><th>3 Axle</th><th>4 Axle</th><th><5 Axl</th><th>5 Axle</th><th>>6 Axl</th><th><6 Axl</th><th>6 Axle</th><th>>6 Axl</th><th>Not</th><th>Code: 1</th></t<>	<u>outhbour</u> Start		Cars 8	2 Axle		2 Axle	3 Axle	4 Axle	<5 Axl	5 Axle	>6 Axl	<6 Axl	6 Axle	>6 Axl	Not	Code: 1
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Date Start: 01-Oct-08

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

4 Axle

Single

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA Southbound

Bikes Trailers

Cars &

2 Axle

Long

Buses

2 Axle

6 Tire

3 Axle

Single

Start

Time

Oct-08	Start: 01-	Date				•	·
Code: 1	Site C						
	Not	>6 Axl	6 Axle	<6 Axl	>6 Axl	5 Axle	<5 Axl
Total	Classe	Multi	Multi	Multi	Double	Double	Double
48	2	0	0	0	0	0	0
48	0	0	0	0	0	0	0
56	3	0	0	0	0	0	0
53	0	0	0	0	0	0	0
205	5	0	0	0	0	0	0
27	1	0	0	0	0	0	0
28	0	0	0	0	0	0	0
41	2	0	0	0	Ó	0	0
31	0	0	0	0	0	0	0
127	3	0	0	0	0	0	0
42	1	0	0	0	0	0	0

Time	Bikes	Trailers			6 Tire	Single				Double	Multi	Mult			Total
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16:30	0	48				0				0	0	0			62
16:45	0	57				0				0	0	C			73
	0	203				1	0			0	0	C) () 6	257
17:00	0	58	17	7.0	3	1	0	C	0	0	0	C) () 1.	80
17:15	0	42	6	30	2	0	0	C	0	0	0	C) () 1	51
17:30	0	50				0	0	Ó	0	0	0	Ċ) C) 2	62
17:45	3	36			3	0				ō	Ő	Č			54
	3	186				1				Ő	0				247
18:00	ŏ	24				0				0	ŏ	0	-		32
18:15	: 0	23				0				0	0	··· · · (
	-					-	-								30
18:30	0	22				0				0	0	C			25
18:45	1	20				0				0	. 0	: (26
	. 1	89				0				0	0	. 0) 2	113
19:00	1	15	2	2 0	···· 0	0	0	0	0	0	0) () 1	19
19:15	0	13	1	1 0	0	0	0	a	0	0	0	C) () 0	14
19:30	0	11	2	2 0	0	0	0	· C	0	0	0) i	0 0	13
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	1	50	ç) 0	0	0	0	C	0	0	0	() () 1	61
20:00	Ó	10				Ő				õ	õ	Ċ			10
20:15	õ	4				Ő				ŏ	. 0	(-	-	4
20:30	ŏ	12				0				ő	ŏ				14
20:30	. Ö	5				0				. 0	0				
20.45	0	31				0				0	0	· · · · · · · · · · · · · · · · · · ·			5
04.00	. 0.														33
21:00	-	11				0		-		0	0	(13
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21:30	0	7			-	0		-		0	0	-(7
21:45						0				0	0				
	0	36	3			0	0	C	0	0	0	() () 1	41
22:00	0	3	÷ 0) 0	0	0	0	C	0	0	0	() () 0	3
22:15	0	8	C) 0	·0	0	0	C	0	0	0	() () 0	8
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22:45	Ō	2				Ő				Ő	õ				4
	0	16				0	and an and a second sec			0	0				19
23:00	ŏ	2				0				0	0				2
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	-						-	-							3
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	0			· · · · · · · · · · · · · · · · · · ·		0				0	0				
Total	13	1105				5				0	0				1493
Percent	0.9%	74.0%	18.6%	6 0.2%	3.0%	0.3%	0.0%	0.2%	0.0%	0.0%	0.0%	0.0%	5 0.0%	s 2.8%	

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA Southbound 50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Date Start: 01-Oct-08 Site Code: 1 6 Axl 6 Axle >6 Axl Not

Soumpor	<u>unu</u>														Code. I
Start		Cars &	2 Axle		2 Axle	3 Axle	4 Axle	<5 Ax	5 Axle	>6 Ax	Axl < 6 Axl	6 Axle	>6 Axl	Not	
Time	Bikes	Trailers				Single							Multi	Classe	Total
													0		
10/02/08	0	4	0		1	0		0						0	5
00:15	0	2				0							0	0	2
00:30	0	3	0		0	0		0					0	0	3
00:45	0	0			0	0	0	0			,		0	0	0
	0	9	0	0	1	0	0	0	C) () 0	0	0	0	10
01:00	0	3	0	0	0	0	0	0	· () () 0	. 0	0	0	3
01:15	0	0	0	0	0	0	0	0	C) (0	0	0
01:30	Ő	1	Ő		ŏ	õ		Ő					ō	Ō	1
01:45	ŏ	0	0		1	0	ŏ	ő					Ő	1	2
01.40	0														
~~~~		4	0			0		0					0	1	6
02:00	0	0	0			0							0	2	2
02:15	0	0	0		0	0		· · · O					°. O'	0	. 0
02:30	0	1	0	0	0	0	0	0	C	) (	) 0	0	0	0	1
02:45	0	1	0	0	0		0	0		) (	) 0	0	0	0	1
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03:30	Ŭ,	ŏ				. : ŏ							· "õ	ŏ	· · · · · · · · · · · · · · · · · · ·
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04:15	0	' <b>2</b>	0			0							0	0	2
04:30	0	1	0	0	0	0	0	0	. (	) (	) (	0	0	0	1
04:45	0	0	0	0		0	0	_0		) (	) 0	0	0	0	0
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		1													
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	0	4	2			0		0					0	0	6
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06:15	. 0	8 8	. i i i	0	0	0	0	0		) (	) 0	0	. 0	0	9
06:30	0	7	1	0	1	0	0	0	(	) (	) (	0	0	0	9
06:45	0	5	3			0							0	0	8
0,0,110	0	23	5			0							0	0	29
07:00	, i i	- 5	. 4			ő				-			ŏ	ŏ	10
07:15	0	13	2			0							0	1	16
07:30	0	12	8		-	0							0		21
07:45	0	30	7	0		0							0	2	40
	0	60	21			0			(				0	3	87
08:00	0	30	12	0	2	0	0	1	(	) (	) (	0	0	3	48
08:15	. 1	29	: 19	. 0	2	0	. 0	0	i (	) (	) (	) 0	0	0	51
08:30	0	28	12		0	0	0	0	(	) (			0	3	44
08:45	o č	49				Ő							. õ	. õ	59
00.40	1	136	51		6	0							0	6	202
00.00	. 0	20	6			0							0		
09:00						-							-	-	27
09:15	0	19	10										0		34
09:30	0	20	9			0							0		30
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	0	81	27	0	4	0			) (	) (	) (	) 0	0	3	115
10:00	0	22	7	0	1	1	0	0		) (	) (	) 0	0	1	32
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10.43															
	0	76	32			1					) (		0		118
11:00	0	17	8			0							0		29
11:15	0	11	6			1	0						0		18
11:30	2	29	13			0							0		48
11:45	1	40	10	00		0	0	0	. (	)(	) (	) 0	0	0	51
	3	97	37			1	0			) (	) (		0	1	146
Total	4	496	176			2									728
Percent	0.5%	68.1%	24.2%			0.3%							0.0%		120
Percent	0.5%	00.1%	24.2%	0.1%	3.0%	0.3%	0.0%	0.3%	0.0%	.0%	0.0%	5 0.0%	0.0%	2.9%	

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

Date Start: 01-Oct-08

Northbou	Ind	•													Code: 1
Start	<b>D</b> .1	Cars &	2 Axle	_	2 Axle	3 Axle	4 Axle	<5 Axl	5 Axle	>6 Axl	<6 Axl	6 Axle	>6 Axl	Not	<b>-</b>
<u>Time</u> 10/01/08	Bikes 0	Trailers	Long 0	Buses 0	<u>6 Tire</u>	Single 0	Single 0	Double 0	Double 0	Double 0	<u>Multi</u> 0	<u>Multi</u> 0	<u>Multi</u> 0	<u>Classe</u>	Total
00:15	0	1 2	0	0	0	0	. 0	0	0	0	0 0	0	0	0	1 2
00:30	õ	3	õ	õ	õ	ŏ	õ	õ	õ	õ	Ő	õ	ŏ	ŏ	3
00:45	0		0	0	0	0	0	0	0	0	0	0	0	0	0
	0	6	0	0	0	0	0	0	0	0	0	0	0	0	6
01:00	0	. 1	0	0	0	0	0	0	. 0	0	0	0	0	0	1
01:15 01:30	0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
01:45	0	. 0	1	0	0	0	0	0	. 0	0	0	0	0	0	1
01.45	0	1	1	0	0	0	0	0	0	0	0	0	0	0	2
02:00	Ō	2	1	Ő	ō	õ	Ō	Ō	Ō	Ō	Ō	Ō	0	Ō	3
02:15	0	. 0	0	. 0	0	- 0	0	0	0	- 0	0	Ö	0	0	0
02:30	0	1	. 1	0	0	0	0	0	0	0	Q	0	0	0	2
02:45	0	0	0	0	0	<u></u>	0	0		0	0	0	0	<u> </u>	0
00.00	0	3	2	0	0	0	0	0	0	0	0	0	0	0	5
03:00 03:15	0	0	0.1	0	· 0 0	0 ¹	0	0	0	0	0,1 0	0	0	0	0
03:30	0	0	0	0	. 0.	0	0	o o o		0	0	0	0	0	Ŭ Ŭ
03:45	ŏ	2	ŏ	Ő	ŏ	Ő	Ŭ	Ő	ŏ	ŏ	Ŭ.	õ	ŏ	ŏ	2
	0	2	0	0	0	Ő	0	0	0	0	0	0	0	0	2
04:00	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
04:15	0	0	0	0		0	0	. 0	0	0	0	0	0	, i o o	: <b>0</b>
04:30	0	2	0	0	0	0	0	0	0	0	0	0	0	0	2
04:45	1	2	2	0	0	0		0	0	0	0	0	0	1	6
05:00	1	5	2	0	0	0	0	0	0	0	0	0	0	1	9
05:00	0	4	2	0	. 0.	0	0	0	0	0	0	0	0	0	7
05:30	ŏ	5	1	ŏ	, o	· · o	ŏ	- Ŭ	0	Ŭ		ŏ		ŏ	- 6
05:45	ō	2	1	Ō	0	õ	0	õ	0	0	0	Ō	0	0	3
	0	14	4	0	1	0	0	0	0	0	0	0	0	0	19
06:00	0	3	3	0	0	0	0	0	0	0	0	0	0		6
06:15	0	4	4	0	0	0	0	0	0	0		0	0	0	8
06:30	0	5	4	0	0	0	0	0	0	0	0	0	0		9
06:45	0	20	5	<u> </u>	1	0	0	0	0	0	0	0	0		<u>14</u> 37
07:00	0	20	16 4	0	0	0	0	0	. 0	-0	0	. 0	0		20
07:15	ő	19	4	0	1	0	0	0	0	0	ő	0	ő		26
07:30	õ	28	1	õ	1	õ	. Õ	ŏ	ŏ	ŏ	÷. Õ	Ő	0		32
07:45	1	34	10	0	0	0	0	1	0	0	0	0	0	0	46
	1	97	19	0	2	0	0	1	0	0	0	0	0		124
08:00	4	28	8	0	2	1	0	1	0	0	0	0	0		48
08:15	. 0	35	6	0	1	· . 1	0	- 0.	. 0	0	0	0	-0		44
08:30 08:45	1	52 .38	5 10	0	0	0	0	0	0	0.0	0	0	0		62 52
00.45	6	153	29	0	3	3	0	1	0	0	0	0	0		206
09:00	Ő	29	4	õ	2	. õ	õ	ò	- Ŭ	ŏ	ŏ	Ő			35
09:15	1	18	4	õ	ō	Ő	0	õ	õ	õ	õ	ō		1	24
09:30	1	21	5	0	0	0	0	0	0	0	0	0	0	2	29
09:45	0	26	4	0	0	0	0	0	0	0	0	0	0		30
	2	94	17	0	2	0	0	0	0	0	0	0	0		118
10:00	2	18	9	0	1	0	0	1 0	0	0	0	0	0		31
10:15 10:30	0 0	23 17	8 5	0	1	0	0	0	0	0	0	0			-33 24
10:30	0	22	5 6	0	1	1	0	1	0	0	0	0			
10.40	2	80	28	0	3	1	0	2	0		0	0			
11:00	ō	17	2	õ	õ	o	õ	õ	Ő	ŏ	õ	õ			20
11:15	0	16	5	1	0	0	0	0	0	0	0	0			27
11:30	0	23	6	0	0	1	0	0	0	0	0	0			30
11:45	1	19	3	0	0	1	0	0	0	0	0	0			26
	1	75	16	1	0	2	0		0	0	0	0			
Total	13	550	134 17.8%	1	12	6	0 0.0%	4	0 0.0%	0 0.0%	0 0.0%	0 0.0%	0 0.0%		
Percent	1.7%	73.0%	17.8%	0.1%	1.6%	0.8%	0.0%	0.5%	0.0%	0.0%	0.0%	0.0%	0.0%	4.4%	

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA

Start

Time

Percent

1.3%

77.6%

14.0%

0.1%

1.8%

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayoureguested.com

Date Start: 01-Oct-08 Northbound Site Code: 1 Cars & 2 Axle 2 Axle 3 Axle 4 Axle <5 Axl 5 Axle >6 Axl <6 Axl 6 Axle >6 Axl Not Bikes Buses Trailers Long 6 Tire Single Single Double Double Double Multi Multi Multi Classe Total 12 PM C 12:15 n 12:30 12:45 o n Ω n 13:00 ō 13:15 n 13:30 13:45 14:00 14:15 -O n n Ω n 14:30 n n n n 14;45 129 15:00 ō ō Ō ٠Õ õ ō 15:15 15:30 Ó Ó Ó 15:45 97 n n n n 16:00 n n n 16:15 16:30 Ō Ó 128 16:45 17:00 17:15 17:30 n 17:45 18.00 O n 18:15 18:30 ź 18:45 19:00 Ō Ó 19:15 ስ 19:30 n n 19:45 D n n Ó ò 20.00 O 20:15 .0 :0 20:30 Ō Ō 20:45 C 21:00 10 21:15 n n 'n Λ 21:30 21:45 <u>3</u> 33 n ŏ 22:00 Ó Ò 22:15 Ó ō 22:30 22:45 n n n n n 23.00 £ O 23:15 23:30 23:45 Tota 

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36

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37

0.0%

4.7%

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50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA Northbound

Date Start: 01-Oct-08 Site Code: 1

Northbou	nd													Site (	<u>Code: 1</u>
Start		Cars &	2 Axle		2 Axle	3 Axle	4 Axle	<5 Axl	5 Axle	>6 Axl	<6 Axl	6 Axle	>6 Axl	Not	
Time	Bikes	Trailers	Long	Buses	6 Tire	Single	Single	Double			Multi	Multi	Multi	Classe	Total
10/02/08	0	1	0	0	0	0	011/910	0	0	0	0	0	0	0	1
00:15	ō	4	õ	0	Ō	ō	Ō	õ	0	Ö	ō	0	ō	0	4
00:30	0	1	0	0	Ó	Ó	0	0	0		0	0	0	0	1
00:45	0	- 1	1	0	0	0	0	0	0	0	0	. 0	0	0	2
	0	7	1	0	0	0	0	0	0	0	0	0	0	0	8
01:00	0	- 1	0	0	0	0	0	0	0	0	0	0	-0	0	.1
01:15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
01:30	0	.1	0	0	0	0	0	0	0		0	0	0	0	1
01:45	0	0	0	0	00	0	0	0	0	0	0	0	0	11	1
	0	2	0	0	0	0	0	0	0		0	0	0	1	3
02:00	0	1	0	0	0	0	0	0	0		0	0	0	0	1
02:15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
02:30 02:45	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
02:45	0	1	0	0	0	0	0	0	0		0	0	0	0	2
03:00	0.5	· 1	: 0	0	. 0	0	Ö		0		Ö	. 0	0	0	1
03:15	0	2	0	0	0	0	0	0	0		ů 0	0	0	0	2
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04:30	0	3	0	0	0	0	0	0	0		0	0	0	0	3
04:45	0		0	0	0	0	0	0	0		0	0	0	0	4
	0	7	0	0	0	0	Q	0	0		0	0	0	0	7
05:00	0	3	2	0	0	: 0°	0	. Ó,	0		• 0	0	0	2	7
05:15	0	5	3	0	0	0	0	0	0		0	0	0	0	8
05:30	0	5	2	0	. 0	0	0	0	0		0	. 0	0	· · · · 0	7
05:45	0	0	1	0	0	0	0	0	0	0	0	0	0	0	1
00.00	0	13	8	0	0	0	0	0	0		0	0	0	2 0	23 4
06:00	0	4	0	0	0	0	0	0	0		0	· 0	0	-0.	13
06:15				0	1.		··· 0. 0		. 0		0	0	0	1	13
06:30 06:45	0	3 14	7	0	0	2	0	0	0		0	0	0	0	17
00.45	0	28	15	0	1	2	0	0	0		0	0	0	1	47
07:00	.0	13	. 4	. 0	. 0 .	ō	ŏ	Ö	. 0		0	ŏ	Ö	0	17
07:15	0	10	3	ŏ	1	ŏ	ŏ	ő	ŏ		Ö	Ö	ő	2	16
07:30	ŏ	31	5	Ō	1	Ŭ,	Ŏ	-0	Ő		Ŭ.	õ	. õ	ō	37
07:45	Ō	28	10	Ō	1	Ō	0	Ō	Ō		0	Ō	Ō	1	40
	0	82	22	0	3	0	0	0	0	0	0	0	0	3	110
08:00	0	32	7	0	0	0	0	0	1	0	0	0	0	4	44
08:15	0	34	11	0	2	0	0	0	0		-0	0	. 0	2	49
08:30	0	49	3	0	1	0	0	0			0	0	0	2	55
08:45		39	5	0	1	0	0	0	0			0	0	2	47
	0	154	26	0	4	0	0	0		0	0	0	0	10	195
09:00	0	20	2	0	0	0	0	0			0	0	-0	2	24
09:15	0	17	5	0	2	0	0	0			0	0	0	3 0	27
09:30	0	22	- 6	0	0 0	0	0 0	0			0	0	0	1	28 25
_09:45	0	<u>16</u> 75	<u>8</u> 21	0	2	0	0	0			0	0	0	6	104
10:00	1	75	12	0	2	0	0	0		-	0	0	0	2	23
10:00	o o	23	12	0	0	0	0	0		-	0	0	0	2	23
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10:45	ŏ	21	4	ő	2	Ő	ő	o o			ő	ő	0	1	28
	1	69	20	Ő	2	0	0	1	0		0	0	0	4	97
11:00	Ö	19	2	ŏ	1	õ	ŏ	, o	ő		Ő	ŏ	õ	1	23
11:15	Ō	24	6	0	1	Ō	Ō	Ő	-		Ō	Ō	Ō	1	32
11:30	1	17	8	Ó	1	Ō	0	Ō			Ō	0	Ó	1	28
11:45	1	16	4	0	0	0	0	0			0	0	0	11	22_
	2	76	20	0	3	0	0	0	0	0	0	0	0	4	105
Total	3	518	133	0	15	2	0	1	1	0	0	0	0	31	704
Percent	0.4%	73.6%	18.9%	0.0%	2.1%	0.3%	0.0%	0.1%	0.1%	0.0%	0.0%	0.0%	0.0%	4.4%	

Location 1: North Street Location 2: West of Northern Avenue City, State: Northampton, MA 50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

Start	Ind	Cars &	2 Axle		2 Axle	3 Axle	4 Axle	<5 Axl	5 Axle	>6 Axl	<6 Axl	6 Axle	>6 Axl	Not	Code:
Time	Bikes	Trailers	Long	Buses	6 Tire	Single	Single	Double	Double	Double	Multi	Multi	Multi	Classe	Tota
12 PM	0	21	3	0	0	0	0	0	0	0	0	0	0	1	25
12:15	. 0	34	7	0	0	1	0	0	0	Ó	0	0	0	3	45
12:30	1	21	4	0	1	0	0	0	0	0	0	0	0	1	2
12:45	0	22	4	0	2	0 -	0	0	0	0	0		0	0	2
	1	98	18	0	3	1	0	0	0	0	0	0	0	5	12
13:00	0	28	4	0	2	0	0	0	0	0	0	0	0	0	3
13:15	1	16	4	0	1	0	0	0	0	0	0	0	0	1	2
13:30	2 1	16 16	4 5	0	1 0	0	. 0 . 0	0	0	0. 0	0	0	0	3	2
13:45	4	76	17	0		1	0	0	0	00	0	0	0	4	2
14:00	4	21	6	0	4	0	0	0	0	0	0	0	0	2	11 3
14:15	. 0	21	· 3.	ŏ	ò	Ŭ,	ŏ	Ö	ŏ	ŏ	- Ö	. 0	ŏ	1	2
14:30	1	18	4	õ	1	0	õ	õ	Ő	ŏ	Õ	ŏ	õ	4	2
14:45	2	23	. 7	0	1		0.	0	0	ŏ		. 0	0	3	3
	4	83	20	0	3	0	0	0	0	0	0	0	0	10	12
15:00	0	35	6	0	1	0	0	0	0	0	.0	0	0	4	4
15:15	2	25	6	0	0	0	0	0	0	0	0	0	0	2	3
15:30	1	26	13	. 0	2	0	0	0	0	0	0	0	0	3	1
15:45	1	26	7	0	1_	0	0	0	0	0	0	0	0	0	
	4	112	32	0	4	0	0	0	0	0	0	0	0	9	16
16:00	0	20	4	0	1	0	0	0	0	0	0	0	0	9	3
16:15	1	21	5	0	0	. 0	. O	2	0	. 0	0	0	0	4	3
16:30 16:45	2 0	26 28	2	- U	1	0	0	0	0	0	0	0	0	12 9	4
10.45	3	95	14	0	4	0	0	2	0	0	0	0	0	34	15
17:00	3	29	4	.0	0	10	. <u>0</u> .	2	0	. 0		. 0	0	34 4	10
17:15	1	29	7	0	0	1	0	0	0	. 0	0		0	. 4	4
17:30	0	26	6	· ŏ	Ő,	ò	-Ö.	Ŭ	ŏ	ŏ	. 0	0.::	ŏ	6	
17:45	. 1	26	1	ŏ	ŏ	1	0	õ	ŏ	0	ő	0	0	6	
	5	110	18	0	0	3	0	0	0	0	0	0	0	25	16
18:00	1	19	3	Ō	1	õ	ō	ō	Ő	õ	õ	õ	Ő	5	2
18:15	· 1.	21	6	0	1	0	0	0	·	Ō	Ō	Ō	Ō	4	
18:30	2	26	1	0	1	0	0	0	0	Ó	0	0	0	4	3
18:45	0	21	2	0	0	0	0	0	0	0	0	0	0	3	
	4	87	12	0	3	0	0	0	0	0	0	0	0	16	12
19:00	0	16	. 1	. 0	0	0	0	0	0	0	0	0	0	<u>1</u>	1.1
19:15	0	14	1	0	0	0	0	0	0	0	0	0	0	5	2
19:30	0	21	2	0	1	0	0	0	0	0	. 0	0	0	• • 0	. 1
19:45	0	11	1	0	0	0	0	0	0	0	0	0	0	1	
	0	62	5	0	1	0	0	0	0	0	0	0	0	7	
20:00	0	18	. 0	0	0	0	0	0	0	0	0	0	0	0	
20:15	0	12	0	0.	1	0	0	0	0	0	0	0	0	0	
20:30 20:45	0	16 12		. 0	0	0	0	0	0	0 0	0	0	0	1	
20.45	0	58	1	0	1	0	0	0	0	0	0	0	0	1	(
21:00	0	10	0	ő	0	-0	0	0	0	0	0	0	0	0	
21:00	0 0	7	1	0	0	0	0 0	0	0	0	0	0	0	0	
21:30	Ő	3	1	ŏ	ŏ	Ö	ŏ	ŏ	ŏ	0 0	Ŭ,	0	-0	ŏ	
21:45	ō	3	Ó	Ő	Ŭ.	Ő	Ő	õ	Ő	Ő	õ	õ	Õ	õ	
	0	23	2	0	0	0	0	0	0	0	0	0	Ő	0	
22:00	0	1	0	0	0	0	0	0	0	Ō	0	0	Ó	0	
22:15	0	3	1	0	0	0	0	0	0	0	0	0	0	0	
22:30	0	4	0	0	0	0	0	0	0	0	0	0	0	0	
22:45	0	7	2	0	0	0	0	0	0	0	0	0	0	0	
	0	15	3	0	0	0	0	0	0	0	0	0	0	0	
23:00	1	4	1	0	0	0	0	0	0	0	0	0	0	1	
23:15	0	1	0	0	0	0	0	0	0	0	0	0	0	0	
23:30	0	4	0	0	0	0	0	0	0	0	0	0	0	0	
23:45	0	5	0	0	0	0	0	0	0	0	0	0	0	0	
T. 1-1	1	14	1	00	0	0	0	0	0	0	0	0	0	1	
Total	26 2.3%	833 72.6%	143 12.5%	0 0.0%	23	5 0.4%	0	2	0	0	0	0	0	116	11
Percent	2.3%	12.0%	12.0%	0.0%	2.0%	0.4%	0.0%	0.2%	0.0%	0.0%	0.0%	0.0%	0.0%	10.1%	
Grand															
Total	55	2689	552	2	68	16	0	9	2	0	0	0	0	228	36
	1.5%	74.3%	15.2%	0.1%	1.9%	0.4%	0.0%	0.2%	0.1%	0.0%	0.0%	0.0%	0.0%	6.3%	
Percent	1.0 /0	14.070	1.2.2./0	U.I /0	1.370	0.470	0.070	U.Z 70	U. 170	U.U.%	0.0%	0.070	0.0%	0.070	



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Northern Avenue City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ Northern Site Code : 3 Start Date : 10/1/2008 Page No : 1

~ <b>—</b>						G	roups	Print	ed- PC	s and P	eds - I	IVs an	d Bike	es							
		No	rth Str	reet				None				No	orth Sta	reet			North	ern A	venue		
		Fr	om No	rth			<u> </u>	rom E	ast			Fr	om So	uth			Fr	om W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	Арр. Тозаі	Left	Thru	Right	Peds	App. Total	Int. Total
07:30 AM	0	17	0	0	17	0	0	0	0	0	0	29	0	0	29	2	0	2	1	5	51
07:45 AM	0	37	0	0	37	0	0	0	0	0	2		0	0	49	1	0	1	0	2	88
Total	0	54	0	0	54	0	0	0	0	0	2	76	0	0	78	3	0	3	1	7	139
08:00 AM	0	46	1	0	47	0	0	0	0	0	1	49	0	0	50	1	0	2	2	5	102
08:15 AM	0	37	1	0	38	0	0	0	0	0	1	45	0	0	46	0	0	3	2	5	89
08:30 AM	0	47	1	0	48	0	0	0	0	0	1	56	0	0	57	1	0	1	3	5	110
08:45 AM	0	55	0	0		0	0	0	0	0	1	40	0		41	0	0	3	0	3	99_
Total	0	185	3	0	188	0	0	0	0	0	4	190	0	0	194	2	0	9	7	18	400
09:00 AM	0	24	0	0	24	0	0	0	0	0	3	27	0	0	30	1	0	1	2	4	58
09:15 AM	0	26	0	0	26	0	0	0	0	0	1	17	0	0	18	0	0	3	2	5	49
Grand Total	0	289	3	0	292	0	0	0	0	0	10	310	0	0	320	6	0	16	12	34	646
Apprch %	0	99	1	0		0	0	0	0		3.1	96.9	0	0		17.6	0	47.1	35.3		
Total %	0	44.7	0.5	0	45.2	0	0	0	0	0	1.5	48	0	0	49.5	0.9	0	2.5	1.9	5.3	
PCs and Peds																					
% PCs and Peds	0	99	100	0		0	0	0	0	0	100	100	0	0	100	100		100	100	100	99.5
HVs and Bikes	0	3	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
% HVs and Bikes	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5

		- • •	orth Sta om No				F	None rom E					rth St om So					iern A rom W	venue 'est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ar	nalysis	From (	07:30 A	M to 0	9:15 AM	I - Peal	cl of 1														
Peak Hour for	Entire	e Inters	ection ]	Begins	at 08:00	AM															
08:00 AM	0	46	1	0	47	0	0	0	0	0	1	49	0	0	50	1	0	2	2	5	102
08:15 AM	0	37	1	0	38	0	0	0	0	0	1	45	0	0	46	0	0	3	2	5	89
08:30 AM	0	47	1	0	48	0	0	0	0	0	1	56	0	0	57	1	0	1	3	5	110
08:45 AM	0	55	0	0	55	0	0	0	. 0	0	1	40	0	0	41	0	0	3	0	3	99_
Total Volume	0	185	3	0	188	0	0	0	0	0	4	190	0	0	194	2	0	9	7	18	400
% App. Total	0	98.4	1.6	0		0	0	0	0		2.1	97.9	0	0		11.1	0	50	38.9		
PHF	.000	.841	.750	.000	.855	.000	.000	.000	.000	.000	1.000	.848	.000	.000	.851	.500	.000	.750	,583	.900	.909



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Day Street / Bates Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ Day Site Code : 4 Start Date : 10/1/2008 Page No : 1

						Gro	ups Pri	inted- H	Vs and	Bikes							
		No	ne			Day S	Street				Street			Bates	Street		
		From	North			From	East			From	South			From	West		
Start Time	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Int. Total
07:30 AM	0	0	0	0	0	2	0	0	1	0	0	0	0	1	1	0	5
07:45 AM	0	0	0	0	0	0	0	0	2	0	0	0	1	1	6	0	10
Total	0	0	0	0	0	2	0	0	3	0	0	0	1	2	7	0	15
08:00 AM	0	0	0	0	0	3	0	0	2	0	0	0	0	1	2	0	8
08:15 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	1	0	0	2
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	2
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0	4
Total	0	0	0	0	0	4	0	0	2	0	0	0	0	2	8	0	16
09:00 AM	0	0	0	0	0	1	0	0	2	0	0	0	0	0	0	0	3
09:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	2	0	3
Grand Total	0	0	0	0	0	7	0	0	7	0	0	0	1	5	17	0	37
Apprch %	0	0	0	0	0	100	0	0	100	0	0	0	4.3	21.7	73.9	0	
Total %	0	0	0	0	0	18.9	0	0	18.9	0	0	0	2.7	13.5	45.9	0	

		Fr	None om Ne					ay Str rom E					orth St om Sc					ites St rom W			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysi	s Fron	n 07:30	O AM t	o 09:15	AM - F	Peak 1	of 1													
Peak Hour fo	or Enti	re Inte	rsectio	n Beg	ins at 0	7:30 A	М														
07:30 AM	0	0	0	0	0	0	2	0	0	2	1	0	0	0	1	0	1	1	0	2	5
07:45 AM	0	0	0	0	0	0	0	0	0	0	2	0	0	0	2	1	1	6	0	8	10
08:00 AM	0	0	0	0	0	0	3	0	0	3	2	0	0	0	2	0	1	2	0	3	8
08:15 AM	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	2
Total Volume	0	0	0	0	0	0	6	0	0	6	5	0	0	0	5	1	4	9	0	14	25
% App. Total	0	0	0	0		0	100	0	0		100	0	0	0		7.1	28.6	64.3	0		
PHF	.000	.000	.000	.000	.000	.000	.500	.000	.000	.500	.625	.000	.000	.000	.625	.250	1.000	.375	.000	.438	.625



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Day Street / Bates Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ Day Site Code : 4 Start Date : 10/1/2008 Page No : 1

					Grou	ps Prir	nted-PC	Cs and	Peds - I	IVs and	d Bikes						
		No	ne			Day S	Street			North	Street	1		Bates	Street		
		From	North			From	East			From	South			From	West		
Start Time	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Int. Total
07:30 AM	0	0	0	0	1	37	0	0	28	0	2	0	0	9	14	0	91
07:45 AM	0	0	0	0	6	27	0	0	34	0_	4	0	1	9	29	0	110
Total	0	0	0	0	7	64	0	0	62	0	6	0	1	18	43	0	201
08:00 AM	0	0	0	0	9	51	0	0	25	0	11	0	0	15	25	0	136
08:15 AM	0	0	0	0	5	25	0	0	28	0	7	1	0	13	20	0	99
08:30 AM	0	0	0	0	6	23	0	0	38	0	8	4	0	8	26	0	113
08:45 AM	0	0	0	0	3	18	0	1	16	0		0	0	27	51	0	124
Total	0	0	0	0	23	117	0	1	107	0	34	5	0	63	122	0	472
09:00 AM	0	0	0	0	1	12	0	0	16	0	5	0	0	12	19	0	65
09:15 AM	0	0	0	0	3	9	0	0	7	0	5	0	0	9	27	0	60
Grand Total	0	0	0	0	34	202	0	1	192	0	50	5	1	102	211	0	798
Apprch %	0	0	0	0	14.3	85.2	0	0.4	77.7	0	20.2	2	0.3	32.5	67.2	0	
Total %	0	0	0	0	4.3	25.3	0	0.1	24.1	0	6.3	0.6	0.1	12.8	26.4	0	<u> </u>
PCs and Peds	0	0	0	0	34	195	0	1	185	0	50	5	0	97	194	0	761
% PCs and Peds	0	0	0	0	100	96.5	0	100	96.4	0	100	100	0	95.1	91.9	0	95.4
HVs and Bikes	0	0	0	0	0	7	0	0	7	0	0	0	1	5	17	0	37
% HVs and Bikes	0	0	0	0	0	3.5	0	0	3.6	0	0	0	100	4.9	8.1	0	4.6

			None					ay Str					orth St					tes St			
		Fr	om No	orth			F	rom E	ast			Fr	om So	outh			<u> </u>	om W	lest		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysi	s From	n 07:30	D AM to	o 09:15	AM - F	Peak 1	of 1													
Peak Hour fo	or Entii	e Inte	rsectic	on Begi	ins at 0	8:00 A	м														
08:00 AM	0	0	0	0	0	9	51	0	0	60	25	0	11	0	36	0	15	25	0	40	136
08:15 AM	0	0	0	0	0	5	25	0	0	30	28	0	7	1	36	0	13	20	0	33	99
08:30 AM	0	0	0	0	0	6	23	0	0	29	38	0	8	4	50	0	8	26	0	34	113
08:45 AM	0	0	0	0	0	3	18	0	1	22	16	0	8	0	24	0	27	51	0	78	124
Total Volume	0	0	0	0	0	23	117	0	1	141	107	0	34	5	146	0	63	122	0	185	472
% App. Total	0	0	0	0		16.3	83	0	0.7		73.3	0	23.3	3.4		0	34.1	65.9	0		
PHF	.000	.000	.000	.000	.000	.639	.574	.000	.250	.588	.704	.000	.773	.313	.730	.000	.583	.598	.000	.593	.868



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: King Street E/W: North Street / Summer Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ King Site Code : 1 Start Date : 10/1/2008 Page No : 1

								Gro	ups Pi	rinted-	HVsa	nd Bi	kes								
		Ki	ng Str	reet			No	orth St	treet			K	ing St	reet			Sun	nmer \$	Street		
		Fre	om No	orth			Fi	rom E	ast			Fr	om So	outh			Fr	om W	lest		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:30 AM	0	3	0	0	3	0	0	0	0	0	0	7	1	0	8	0	0	1	0	1	12
07:45 AM	1	1	0	0	2	0	0	0	0	0	0	7	0	.2	9	0	0	0	1	1	12
Total	1	4	0	0	5	0	0	0	0	0	0	14	1	2	17	0	0	1	1	2	24
08:00 AM	1	3	0	0		0	0	0	1	1	0		0	0	4	0	0	0	0	0	0
	1	-	0	-	4		0	0			0	4	-		4	0		0	0	0	9
08:15 AM	0	3	0	0	3	0	0	1	1	2	0	3	0	0	3	0	1	1	0	2	10
08:30 AM	0	2	0	1	3	0	0	0	0	0	0	2	1	1	4	1	1	0	1	3	10
08:45 AM	0	3	0	1	4	0	0		1	2	0	2	0	1	3	0	0	0	1	1	10
Total	1	11	0	2	14	0	0	2	3	5	0	11	1	2	14	1	2	1	2	6	39
09:00 AM	1	1	0	0	2	0	0	0	0	0	0	1	1	0	2	0	1	0	1	2	6
09:15 AM	0	2	Ó	Ó	2	Ó	Ō	Ō	1	1	0	3	Ó	Ō	3	Ō	Ó	1	Ó	1	7
Grand Total	3	18	ō	2	23	Ō	ŏ	2	4	6	Ő	29	3	4	36	1	3	3	4	11	76
Apprch %	13	78.3	Ō	8.7		Ō	Ō	33.3	66.7	-	Ō	80.6	8.3	11.1		9.1	27.3	27.3	36.4		
Total %	3.9	23.7	Ō	2.6	30.3	0	Ō	2.6	5.3	7.9	0	38.2	3.9	5.3	47.4	1.3	3.9	3.9	5.3	14.5	

			ng St om N					rth St rom E					ing St om Sc					nmer s om W	Street /est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysi	s Fron	n 07:30	O AM te	0 09:15	AM - F	Peak 1	of 1													
Peak Hour fo	or Enti	re Inte	rsectio	on Beg	ins at 0	7:30 A	М														
07:30 AM	0	3	0	0	3	0	0	0	0	0	0	7	1	0	8	0	0	1	0	1	12
07:45 AM	1	1	0	0	2	0	0	0	0	0	0	7	0	2	9	0	0	0	1	1	12
08:00 AM	1	3	0	0	4	0	0	0	1	1	0	4	0	0	4	0	0	0	0	0	9
08:15 AM	0	3	0	0	3	0	0	1	1	2	0	3	0	0	3	0	1	1	0	2	10
Total Volume	2	10	0	0	12	0	0	1	2	3	0	21	1	2	24	0	1	2	1	4	43
% App. Total	16.7	83.3	0	0		0	0	33.3	66.7		0	87.5	4.2	8.3		0	25	50	25		
PHF	.500	.833	.000	.000	.750	.000	.000	.250	.500	.375	.000	.750	.250	.250	.667	.000	.250	.500	.250	.500	.896



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: King Street E/W: North Street / Summer Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ King Site Code : 1 Start Date : 10/1/2008 Page No : 1

						G	Group	s Prin	ted- P	Cs and	Peds	- HV	s and	Bikes							
		Ki	ng Str	eet			No	rth St	reet			Ki	ng St	reet			Sum	nmer S	Street	t	
		Fre	om No	orth			۴ı	om E	ast			Fr	om So	outh		ļ,	Fr	om W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:30 AM	14	85	0	1	100	13	0	36	0	49	0	86	10	1	97	9	7	6	0	22	268
07:45 AM	40	91	0	0	131	20	0	33_	0	<u>53</u>	0_	112	_14	2	128	16	32	6	1_	55	<u>367</u>
Total	54	176	0	1	231	33	0	69	0	102	0	198	24	3	225	25	39	12	1	77	635
08:00 AM	36	97	0	0	400	22	0	47	2	71	~	100	0	4	110	10	28	5	~	51	373
			0	0	133		0	47	2		0	109	8		118	16		-	2		
08:15 AM	44	124	0	0	168	29	0	58	2	89	0	102	11	0	113	16	33	12	2	63	433
08:30 AM	39	133	0	1	173	31	0	64	1	96	0	93	16	2	111	18	46	10	4	78	458
08:45 AM	34	_110_	0	2_	146	41	0	68	2	111	0	101	17	3	121_	17	25	11	5	58	436
Total	153	464	0	3	620	123	0	237	7	367	0	405	52	6	463	67	132	38	13	250	1700
09:00 AM	29	94	0	0	123	18	0	31	1	50	0	80	12	0	92	21	15	9	2	47	312
09:15 AM	25	103	ŏ	Ő	128	17	ŏ	41	3	61	ŏ	99	6	ŏ	105	10	14	ğ	1	34	328
Grand Total	261	837	ŏ	4	1102	191	ő	378	11	580	ň	782	94	ğ	885	123	200	68	17	408	2975
Apprch %	23.7	76	Ő	0.4	1102	32.9	0	65.2	1.9	500	0	88.4	10.6	1	000	30.1	49	16.7	4.2	400	2010
Total %	8.8	28.1	0	0.4	37	6.4	Ő	12.7	0.4	19.5	Ő	26.3	3.2	0.3	29.7	4.1	6.7	2.3	0.6	13.7	
	0.0	20.1		0.1	37	0.4	<u> </u>	12.7	0.4	19.5		20.5	5.2	0.5	23.1	4.1	0.7	2.5	0.0	10.7	
PCs and Peds	98.9	97.8	0	50	97.9	100	0	99.5	63.6	99	0	96.3	96.8	55.6	95.9	99.2	98.5	95.6	76.5	97.3	97.4
% PCs and Peds	30.9	31.0	0	50	57.9		0	33.0	0.0.0	99		30.3	90.0	00.0	50.9	99.Z	50.0	33.0	10.0	31.5	37.4
HVs and Bikes	1.1	2.2	0	50	2.1	0	0	0.5	36.4	1	0	3.7	3.2	44.4	4.1	0.8	1.5	4.4	23.5	2.7	2.6
% HVs and Bikes	1.1	Z.Z	0	50	2.1	U	0	0.5	30.4		0	3.7	3.2	44.4	4.1	0.0	1.0	4.4	23.0	2.1	2.0

			ng St om N					orth St rom E					ing St om Sc					nmer S om W	Street /est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysi	s Fron	n 07:30	0 AM t	o 09:15	AM - I	Peak 1	of 1													
Peak Hour fo	nalysis From 07:30 AM to 09:15 AM - Peak 1 of 1 or Entire Intersection Begins at 08:00 AM 36 97 0 0 133 22 0 47 2 71 0 109 8 1 118 16 28 5 2 51																				
08:00 AM	36	97	0	0	133	22	0	47	2	71	0	109	8	1	118	16	28	5	2	51	373
08:15 AM	44	124	0	0	168	29	0	58	2	89	0	102	11	0	113	16	33	12	2	63	433
08:30 AM	39	133	0	1	173	31	0	64	1	96	0	93	16	2	111	18	46	10	4	78	458
08:45 AM	34	110	0	2	146	41	0	68	2	111	0	101	17	3	121	17	25	11	5	58	436
Total Volume	153	464	0	3	620	123	0	237	7	367	0	405	52	6	463	67	132	38	13	250	1700
% App. Total	24.7	74.8	0	0.5		33.5	0	64.6	1.9		0	<u>87.5</u>	11.2	1.3		26.8	52.8	15.2	5.2		
PHF	.869	.872	.000	.375	.896	.750	.000	.871	.875	.827	.000	.929	.765	.500	.957	.931	,717	.792	.650	.801	.928



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street / Market Street E/W: North Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ Market Site Code : 2 Start Date : 10/1/2008 Page No : 1

								Gro	ups Pr	inted - H	Vs an	d Bike	s								-
		No	orth St	reet				None	9			Ma	rket S	treet			No	rth St	reet		
		Fı	om No	orth			F	rom E	ast			Fr	om So	uth			F1	rom W	'est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:30 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1	0	1	2
07:45 AM	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	2
Total	0	1	1	0	2	0	0	0	0	0	0	0	0	0	0	1	0	1	0	2	4
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	i	2	2
08:15 AM	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	2
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	0	2	2
08:45 AM	0	0	. 2	0	2	0	0	0	0	0	0		0	0	0	0	0	0	0	0	2
Total	0	0	3	0	3	0	0	0	0	0	0	0	0	0	0	4	0	0	1	5	8
09:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0	0	0	3	3
09:15 AM	0	1	1	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
Grand Total	0	2	5	0	7	0	0	0	0	0	0	0	0	0	0	8	0	1	1	10	17
Apprch %	0	28.6	71.4	0		0	0	0	0		0	0	0	0		80	0	10	10		
Total %	0	11.8	29.4	0	41.2	0	0	0	0	0	0	0	0	0	0	47.1	0	5.9	5.9	58.8	

			rth Str om No				F	None rom E					rket S om So					rth Sti om W			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ar	nalysis	From (	)7:30 A	M to 0	9:15 AM	1 - Peal	c I of I														
Peak Hour for	r Entire	Inters	ection ]	Begins	at 08:15	AM															
08:15 AM	0	0	1	0	1	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	2
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	0	2	2
08:45 AM	0	0	2	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
09:00 AM	0	. 0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0		0	3	3
Total Volume	0	0	3	0	3	0	0	0	0	0	0	0	0	0	0	6	0	0	0	6	9
% App. Total	0	0	100	0		0	0	0	0		0	0	0	0		100	0	0	0		
PHF	.000	.000	.375	.000	.375	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.500	.000	.000	.000	.500	.750



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street / Market Street E/W: North Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ Market Site Code : 2 Start Date : 10/1/2008 Page No : 1

							Froups	Print	ed- PC	s and P	eds - I	IVs ar	d Bike	es							
		No	orth Sti	reet				None				Ma	rket S	treet			No	rth St	reet		i
		Fı	om No	rth			F	rom E	ast			Fr	om So	uth			Fr	om W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:30 AM	0	8	26	0	34	0	0	0	0	0	25	9	0	0	34	19	0	20	1	40	108
07:45 AM	0	11	37	0	48	0	0	. 0	0_	0	15	11	0	1	27	51	0	36	0	87	162
Total	0	19	63	0	82	0	0	0	0	0	40	20	0	1	61	70	0	56	1	127	270
08:00 AM	0	13	50	0	63	0	0	0	0	0	24	11	0	1	36	42	0	31	2	75	174
08:15 AM	0	6	47	0	53	0	0	0	0	0	29	10	0	1	40	49	0	39	1	89	182
08:30 AM	0	9	56	0	65	0	0	0	0	0	41	13	0	2	56	57	0	45	0	102	223
08:45 AM	0	15	60	0	75	0	0	0	0	0	45	. 9	0	4	58	42	0	33	0	75	208
Total	0	43	213	0	256	0	0	0	0	0	139	43	0	8	190	190	0	148	3	341	787
09:00 AM	0	10	23	0	33	0	0	0	0	0	19	6	0	1	26	33	0	26	1	60	119
09:15 AM	0	9	31	0	40	0	0	0	0	0	24	3	0	1	28	23	0	24	0	47	115
Grand Total	0	81	330	0	411	0	0	0	0	0	222	72	0	11	305	316	0	254	5	575	1291
Apprch %	0	19.7	80.3	0		0	0	0	0		72.8	23.6	0	3.6		55	0	44.2	0.9		Í
Total %	0	6.3	25.6	0	31.8	0	0	0	0	0	17.2	5.6	0	0.9	23.6	24.5	0	19.7	0.4	44.5	
PCs and Peds																					
% PCs and Peds	0	97.5	98.5	0	98.3	0	0	0	0	0	100	100	0	100	100	97.5	0	99.6	80	98.3	98.7
HVs and Bikes																					
% HVs and Bikes	0	2.5	1.5	0	1.7	0	0	0	0	0	0	0	0	0	0	2.5	0	0.4	20	1.7	1.3

			orth St om No				F	None rom E					rket S om So					rth St rom W			
Stant Times	T . G	(******	1		1	Lan					T . A		1			Left		1			
Start Time	Left	Thru		Peds	App. Total		Thru		Peds	App. Total	Left	Thru	Right	Peds	App. Total	Len	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ai	nalysis	From (	07:30 A	M to C	)9:15 AM	1 - Peal	k 1 of 1														
Peak Hour for	Entire	e Inters	ection	Begins	at 08:00	AM															
08:00 AM	0	13	50	0	63	0	0	0	0	0	24	11	0	1	36	42	0	31	2	75	174
08:15 AM	0	6	47	0	53	0	0	0	0	0	29	10	0	1	40	49	0	39	1	89	182
08:30 AM	0	9	56	0	65	0	0	0	0	0	41	13	0	2	56	57	0	45	0	102	223
08:45 AM	0	15	60	0	75	0	0	0	0	0	45	9	0	4	58	42	0	33	0	75	208
Total Volume	0	43	213	0	256	0	0	0	0	0	139	43	0	8	190	190	0	148	3	341	787
% App. Total	0	16.8	83.2	0		0	0	0	0		73.2	22.6	0	4.2		55.7	0	43.4	0.9		
PHF	.000	.717	.888	.000	.853	.000	.000	.000	.000	.000	.772	.827	.000	.500	.819	.833	.000	.822	.375	.836	.882

#### Data Acquisition, Transformation & Analysis 50 Alden Avenue



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Northern Avenue City, State: Northampton, Ma Client: FandO / S. Savaria File Name : AM_North @ Northern Site Code : 3 Start Date : 10/1/2008 Page No : 1

								Gro	ups Pr	inted- H	Vs an	l Bike	s								_
		No	rth Stu	reet				None	•			No	rth St	reet			North	iern A	venue		•
		Fr	om No	orth			F	rom E	ast			Fr	om So	uth			F	rom W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App, Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:00 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
08:15 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:45 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Total	0	3	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
09:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
09:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	3	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
Apprch %	0	100	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
Total %	0	100	0	0	100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

			orth Str om No				F	None rom E					rth St om So					ern A om W	venue 'est		
Start Time	Left	Thru	Right	Peds	App. Tetal	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ar	nalysis	From (	07:30 A	M to 0	9:15 AM	1 - Peal	k 1 of 1														
Peak Hour for	r Entire	e Inters	ection ]	Begins	at 08:00	AM															
08:00 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
08:15 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:45 AM	0	1	0		1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Total Volume	0	3	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
% App. Total	0	100	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.750	.000	.000	.750	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.750



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Northern Avenue City, State: Northampton, Ma Client: FandO / S. Savaria

File Name : PM_North @ Northern Site Code : 3 Start Date : 10/1/2008 Page No : 1

								Gro	ups Pri	inted- H	Vs an	d Bike	s								_
		No	rth St	reet				None	•			No	rth St	reet			North	iern A	venue		
		Fr	om No	orth			F	rom E	ast			Fr	om So	uth			F1	rom W	'est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
03:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
03:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Apprch %	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
Total %																					

			orth Str om No				F	None rom E					rth St om So					ern A om W	venue 'est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour A	nalysis	From (	)3:30 P	M to 0	5:15 PM	- Peak	1 of 1														
Peak Hour fo	r Entire	Inters	ection	Begins	at 03:30	PM															
03:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
03:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total Volume	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% App. Total	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0		
PHF	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Northern Avenue City, State: Northampton, Ma Client: FandO / S. Savaria File Name : PM_North @ Northern Site Code : 3 Start Date : 10/1/2008 Page No : 1

							Groups	Print	ed- PC	s and P	eds - I	IVs ar	nd Bike	es							
		No	orth Stu	reet				None				No	orth St	reet			North	ern A	venue		
		Fr	om No	orth			F	rom E	ast			Fı	om So	uth			Fr	om W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
03:30 PM	0	63	1	0	64	0	0	0	0	0	0	27	0	0	27	1	0	2	4	7	98
03:45 PM	0	48	1	0	49	0	0	0	0	0	1	22	0	0	23	1	0	1	3	5	77
Total	0	111	2	0	113	0	0	0	0	0	1	49	0	0	50	2	0	3	7	12	175
04:00 PM	0	49	1	0	50	0	0	0	0	0	1	30	0	0	31	1	0	1	1	3	84
04:15 PM	0	65	2	0	67	0	0	0	0	0	1	34	0	0	35	1	0	0	6	7	109
04:30 PM	0	61	1	0	62	0	0	0	0	0	0	28	0	0	28	0	0	2	1	3	93
04:45 PM	0	61	3	0	64	0	0	0	0	0	2	24	0	0	26	0	0	2	2	4	94
Total	0	236	7	0	243	0	0	0	0	0	4	116	0	0	120	2	0	5	10	17	380
05:00 PM	0	78	2	0	80	0	0	0	0	0	1	37	1	0	39	1	0	0	1	2	121
05:15 PM	0	44	0	0	44	0	0	0	0	0	2	23	0	0	25	1	0	0	2	3	72
Grand Total	0	469	11	0	480	0	0	0	0	0	8	225	1	0	234	6	0	8	20	34	748
Apprch %	0	97.7	2.3	0		0	0	0	0		3.4	96.2	0.4	0		17.6	0	23.5	58.8		
Total %	0	62.7	1.5	0	64.2	0	0	0	0	0	1.1	30.1	0.1	0	31.3	0.8	0	1.1	2.7	4.5	
PCs and Peds																					
% PCs and Peds	0	100	100	0	100	0	0	0	0	0	100	100	100	0	100	100	0	100	100	100	100
HVs and Bikes	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% HVs and Bikes	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

			orth St					None					rth St						venue		
L		Fr	<u>om No</u>	orth			<b>F</b>	rom E	ast			Fr	<u>om So</u>	uth			<u>Fi</u>	rom W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour An	nalysis	From (	03:30 P	M to 0	5:15 PM	- Peak	1 of 1														
Peak Hour for	Entire	e Inters	ection ]	Begins	at 04:15	PM															
04:15 PM	0	65	2	0	67	0	0	0	0	0	1	34	0	0	35	1	0	0	6	7	109
04:30 PM	0	61	1	0	62	0	0	0	0	0	0	28	0	0	28	0	0	2	1	3	93
04:45 PM	0	61	3	0	64	0	0	0	0	0	2	24	0	0	26	0	0	2	2	4	94
05:00 PM	0	78	2	0	80	0	0	0	0	0	1	37	1	0	39	1	0	0	1	2	121
Total Volume	0	265	8	0	273	0	0	0	0	0	4	123	1	0	128	2	0	4	10	16	417
% App. Total	0	97.1	2.9	0		0	0	0	0		3.1	96.1	0.8	0		12.5	0	25	62.5		
PHF	.000	.849	.667	.000	.853	.000	.000	.000	.000	.000	.500	.831	.250	.000	.821	.500	.000	.500	.417	.571	.862



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Day Street / Bates Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : PM_North @ Day Site Code : 4 Start Date : 10/1/2008 Page No : 1

								Gro	ups Pri	inted- H	Vs an	d Bike	s								
			None				D	ay Str	eet			No	rth St	reet			Ba	tes Str	eet		Ì
		Fr	om No	orth			<b>F</b>	rom E	ast		İ	Fr	<u>om So</u>	uth			F	<u>rom W</u>	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
03:30 PM	0	0	0	0	0	0	0	0	0	0	2	0	0	0	2	0	0	2	0	2	4
03:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	3	0	3	3
Total	0	0	0	0	0	0	0	0	0	0	2	0	0	0	2	0	0	5	0	5	7
04:00 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	1	0	1	2
04:15 PM	0	0	0	0	0	0	1	0	0	1	3	0	0	0	3	0	0	1	0	1	5
04:30 PM	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0	2	1	0	3	4
04:45 PM	0	0	0	0	0_	0	1		0	1	2	0	0	0	2	0	0	1	0	1	4
Total	0	0	0	0	0	0	3	0	0	3	6	0	0	0	6	0	2	4	0	6	15
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
05:15 PM	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	2
Grand Total	0	0	0	0	0	0	4	0	0	4	8	0	0	0	8	0	3	9	0	12	24
Apprch %	0	0	0	0		0	100	0	0		100	0	0	0		0	25	75	0		
Total %	0	0	0	0	0	0	16.7	0	0	16.7	33.3	0	0	0	33.3	0	12.5	37.5	0	50	

		Fr	None om No					ay Str rom E					rth St om So					tes Str ·om W			
Start Time	Left	Thru	Right	Peds	App. Totai	Left	Thru	Right	Peds	App. Totzl	Left		Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ar	alysis	From (	)3:30 P	M to 0	5:15 PM	- Peak	1 of 1														
Peak Hour for	Entire	Inters	ection	Begins	at 04:00	PM															
04:00 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	0	1	0	1	2
04:15 PM	0	0	0	0	0	0	1	0	0	1	3	0	0	0	3	0	0	1	0	1	5
04:30 PM	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0	2	1	0	3	4
04:45 PM	0	0	0	0	0_	0	1	0	0	1	2	0	0	0	2	0	0	1	0	1	4
Total Volume	0	0	0	0	0	0	3	0	0	3	6	0	0	0	6	0	2	4	0	6	15
% App. Total	0	0	0	0		0	100	0	0		100	0	0	0		0	33.3	66.7	0		
PHF	.000	.000	.000	.000	.000	.000	.750	.000	.000	.750	.500	.000	.000	.000	.500	.000	.250	1.000	.000	.500	.750



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street E/W: Day Street / Bates Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : PM_North @ Day Site Code : 4 Start Date : 10/1/2008 Page No : 1

						0	Froups	S Print	ed- PC	s and P	eds - H	IVs an	d Bike	es							
			None				D	ay Stre	eet			No	rth St	reet			Ba	tes Str	eet		
		Fr	om No	rth			F	rom E	ast			Fr	om So	uth			F	rom W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
03:30 PM	0	0	0	0	0	7	9	0	0	16	17	0	3	0	20	0	31	56	0	87	123
03:45 PM	0	0	0	0	0	4	5	0	0		12	0	2	0	14	0	18	33	0	51	74
Total	0	0	0	0	0	11	14	0	0	25	29	0	5	0	34	0	49	89	0	138	197
04:00 PM	0	0	0	0	0	2	9	0	0	11	14	0	2	1	17	0	21	47	0	68	96
04:15 PM	0	0	0	0	0	10	10	0	0	20	16	0	9	0	25	0	34	45	0	79	124
04:30 PM	0	0	0	0	0	5	11	0	0	16	8	0	6	0	14	0	26	47	0	73	103
04:45 PM	0	0	0	0	0	10	18	0	0	28	13	0	3	0	16	0	22	44	0	66	110
Total	0	0	0	0	0	27	48	0	0	75	51	0	20	1	72	0	103	183	0	286	433
05:00 PM	0	0	0	0	0	13	8	0	0	21	12	0	10	0	22	0	29	58	0	87	130
05:15 PM	0	0	0	0	0	6	17	0	0	23	8	0	3	0	11	0	22	28	0	50	84
Grand Total	0	0	0	0	0	57	87	0	0	144	100	0	38	1	139	0	203	358	0	561	844
Apprch %	0	0	0	0		39.6	60.4	0	0		71.9	0	27.3	0.7		0	36.2	63.8	0		
Total %	0	0	0	0	0	6.8	10.3	0	0	17.1	11.8	0	4.5	0.1	16.5	0	24.1	42.4	0	66.5	
PCs and Peds					1																
% PCs and Peds	0	0	0	0	0	100	95.4	0	0	97.2	92	0	100	100	94.2	0	98.5	97.5	0	97.9	97.2
HVs and Bikes																					
% HVs and Bikes	0	0	0	0	0	0	4.6	0	0	2.8	8	0	0	0	5.8	0	1.5	2.5	0	2.1	2.8

		Fr	None om No					ay Str rom E					rth St om So					tes Str rom W			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ar	nalysis	From (	03:30 P	M to 0	5:15 PM	- Peak	1 of 1														
Peak Hour for	r Entire	e Inters	ection 1	Begins	at 04:15	PM															
04:15 PM	0	0	0	0	0	10	10	0	0	20	16	0	9	0	25	0	34	45	0	79	124
04:30 PM	0	0	0	0	0	5	11	0	0	16	8	0	6	0	14	0	26	47	0	73	103
04:45 PM	0	0	0	0	0	10	18	0	0	28	13	0	3	0	16	0	22	44	0	66	110
05:00 PM	0	0	0	0	0	13		0	0	21	12	0	10	0	_22	0	29	58	0	87	130
Total Volume	0	0	0	0	0	38	47	0	0	85	49	0	28	0	77	0	111	194	0	305	467
% App. Total	0		0	0		44.7	55.3	0	0		63.6	0	36.4	0		0	36.4	63.6	0		
PHF	.000	.000	.000	.000	.000	.731	.653	.000	.000	.759	.766	.000	.700	.000	.770	.000	.816	.836	.000	.876	.898



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: King Street E/W: North Street / Summer Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : Not Named 4 Site Code : 1 Start Date : 10/1/2008 Page No : 1

								Gro	ups Pr	inted <u>- H</u>	<u>Vs an</u>	d Bike	5								
		K	ing Str	eet			No	rth St	reet			K	ing Str	eet			Sum	mer S	treet		
		Fr	om No	orth			F	rom E	ast			Fr	om So	uth			F	rom W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
03:30 PM	0	1	0	0	1	0	0	0	2	2	0	5	0	4	9	0	0	0	3	3	15
03:45 PM	0	3	0	1	4	1	0	0	2	3	0	4	0	2	6	<u>,0</u>	0	0	1	1	14
Total	0	4	0	1	5	1	0	0	4	5	0	9	0	6	15	0	0	0	4	4	29
04:00 PM	0	2	0	0	2	0	0	0	1	1	0	2	0	4	6	0	0	0	1	1	10
04:15 PM	0	1	0	1	2	0	0	0	0	0	0	ł	0	1	2	1	0	0	5	6	10
04:30 PM	1	3	0	1	5	0	0	0	1	1	0	1	0	0	1	0	0	0	1	1	8
04:45 PM	0	1	0	0	1	0	0	1	2	3	0	0	1	2	3	0	0	0	2	2	9
Total	1	7	0	2	10	0	0	1	4	5	0	4	1	7	12	1	0	0	9	10	37
05:00 PM	1	0	0	0	1	1	0	0	1	2	0	3	0	1	4	0	0	0	2	2	9
05:15 PM	0	2	0	1	3	1	0	0	1	2	0	2	0	0	2	0	0	0	0	0	7
Grand Total	2	13	0	4	19	3	0	1	10	14	0	18	1	14	33	1	0	0	15	16	82
Apprch %	10.5	68.4	0	21.1		21.4	0	7.1	71.4		0	54.5	3	42.4		6.2	0	0	93.8		
Total %	2.4	15.9	0	4.9	23.2	3.7	0	1.2	12.2	17.1	0	22	1.2	17.1	40.2	1.2	0	0	18.3	19.5	

			ing Str om No					rth St rom E					ing Str om So					mer S om W			
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour An	nalysis	From (	03:30 P	M to 0	5:15 PM	- Peak	1 of 1														
Peak Hour for	Entire	Inters	ection	Begins	at 03:30	PM															
03:30 PM	0	1	0	0	1	0	0	0	2	2	0	5	0	4	9	0	0	0	3	3	15
03:45 PM	0	3	0	1	4	1	0	0	2	3	0	4	0	2	6	0	0	0	1	1	14
04:00 PM	0	2	0	0	2	0	0	0	1	1	0	2	0	4	6	0	0	0	1	1	10
04:15 PM	0	1	0	1	2	0	0	0	0	0	0	1	0	1	2	1	0	0	5	6	10
Total Volume	0	7	0	2	9	1	0	0	5	6	0	12	0	11	23	1	0	0	10	11	49
% App. Total	0	77.8	0	22.2		16.7	0_	0	83.3		0	52.2	0	47.8		9.1	0	0	90.9		
PHF	.000	.583	.000	.500	.563	.250	.000	.000	.625	.500	.000	.600	.000	.688	.639	.250	.000	.000	.500	.458	.817

# DATA, Inc.

## Data Acquisition, Transformation & Analysis

50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: King Street E/W: North Street / Summer Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : Not Named 4 Site Code : 1 Start Date : 10/1/2008 Page No : 1

						(	Froups	s Print	ed- PC	s and P	eds - F	IVs an	nd Bik	es							
		K	ing Str	eet			No	rth St	reet			K	ing Str	eet			Sum	mer S	treet		
		Fr	om No	rth			<b>F</b>	rom E	ast			Fr	om So	uth			Fr	om W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Tetal	Int. Total
03:30 PM	30	143	0	0	173	25	0	91	6	122	0	156	8	6	170	21	25	10	5	61	526
03:45 PM	_ 29	132	0	3	164	22	0	85		115	0	140	19	2	161	22	26	6	6	60	500
Total	59	275	0	3	337	47	0	176	14	237	0	296	27	8	331	43	51	16	11	121	1026
04:00 PM	32	122	0	0	154	23	0	56	2	81	0	149	5	6	160	18	25	6	1	50	445
04:15 PM	39	118	Ō	1	158	22	Ō	79	1	102	Ő	126	12	2	140	17	27	8	ŝ	57	457
04:30 PM	33	119	0	2	154	24	Ó	112	3	139	0	142	15	3	160	16	23	3	3	45	498
04:45 PM	37	101	Ō	0	138	19	Ō	103	5	127	0	116	16	3	135	17	17	1	6	41	441
Total	141	460	0	3	604	88	0	350	11	449	0	533	48	14	595	68	92	18	15	193	1841
05.00 DM		120	0		170	20	0	00	_	104				•	1.67	10	26			50	<b>611</b>
05:00 PM	41	130	0	1	172	29	0	90	5	124	0	141	14	2	157	18	25	4	11	58	511
05:15 PM	45	131	0	I	177	18	0	108	2	128	0	136	8	0	144	21	19	4	0	44	493
Grand Total	286	996	0	8	1290	182	0	724	32	938	0	1106	97	24	1227	150	187	42	37	416	3871
Apprch %	22.2	77.2	0	0.6		19.4	0	77.2	3.4		0	90.1	7.9	2		36.1	45	10.1	8.9		
Total %	7.4	25.7	0	0.2	33.3	4.7	0	18.7	0.8	24.2	0	28.6	2.5	0.6	31.7	3.9	4.8	1.1	1	10.7	
PCs and Peds												1088									}
% PCs and Peds	99.3	98.7	0	_50	98.5	98.4	0	99.9	68.8	98.5	0	98.4	99	41.7	97.3	99.3	100	100	59.5	96.2	97.9
HVs and Bikes																					
% HVs and Bikes	0.7	1.3	0	50	1.5	1.6	0	0.1	31.2	1.5	0	1.6	1	58.3	2.7	0.7	0	0	40.5	3.8	2.1

	King Street From North						rth St rom E					ing Str om So					mer S om W				
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ar	nalysis	From (		M to 0	5:15 PM	- Peak	1 of 1														
Peak Hour for	r Entire	Inters	ection l	Begins	at 04:30	PM															
04:30 PM	33	119	0	2	154	24	0	112	3	139	0	142	15	3	160	16	23	3	3	45	498
04:45 PM	37	101	0	0	138	19	0	103	5	127	0	1/16	16	3	135	17	17	1	6	41	441
05:00 PM	41	130	0	1	172	29	0	90	5	124	0	141	14	2	157	18	25	4	11	58	511
05:15 PM	45	131	0	1	177	18	0	108	2	128	0	136	8	0	144	21	19	4	0	44	493
Total Volume	156	481	0	4	641	90	0	413	15	518	0	535	53	8	596	72	84	12	20	188	1943
% App. Total	24.3	75	0	0.6		17.4	0	79.7	2.9		0	89.8	8.9	1.3		38.3	44.7	6.4	10.6		
PHF	.867	.918	.000	.500	.905	.776	.000	.922	.750	.932	.000	,942	.828	.667	.931	.857	.840	.750	.455	.810	.951



50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street / Market Street E/W: North Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : PM_North @ Market Site Code : 2 Start Date : 10/1/2008 Page No : 1

								Gro	ups Pr	inted- H	Vs and	l Bike	s								
		No	orth St	reet				None				Ma	rket S	treet			No	orth St	reet		
		Fı	om No	orth			F	rom E	ast			Fr	om So	uth			F	rom W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
03:30 PM	0	0	1	9	10	0	0	0	2	2	0	0	0	1	1	0	0	1	3	4	17
03:45 PM	0	0	2	14	16	0	0	0	4	4	0	0	0	0	0	1	0	1	0	2	22
Total	0	0	3	23	26	0	0	0	6	6	0	0	0	1	1	1	0	2	3	6	39
04:00 PM	0	1	0	7	8	0	0	0	1	1	0	0	0	0	0	1	0	1	5	7	16
04:15 PM	0	0	1	11	12	0	0	0	4	4	0	0	0	1	1	2	0	0	4	6	23
04:30 PM	0	0	0	6	6	0	0	0	3	3	0	0	0	0	0	0	0	3	2	5	14
04:45 PM	0	0	0	10	10	0	0		1	1	1	1	0	. 1	3	2	0	0	7	9	23
Total	0	1	1	34	36	0	0	0	9	9	1	1	0	2	4	5	0	4	18	27	76
05:00 PM	0	0	1	13	14	0	0	0	1	1	0	0	0	1	1	0	0	1	2	3	19
05:15 PM	0	0	1	10	11	0	0	0	4	4	2	0	0	2	4	0	0	2	5	7	26
Grand Total	0	1	6	80	87	0	0	0	20	20	3	1	0	6	10	6	0	9	28	43	160
Apprch %	0	1.1	6.9	92		0	0	0	100		30	10	0	60		14	0	20.9	65.1		
Total %	0	0.6	3.8	50	54.4	0	0	0	12.5	12.5	1.9	0.6	0	3.8	6.2	3.8	0	5.6	17.5	26.9	1

	North Street From North					F	None rom E					rket S om So					rth St om W				
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Tota
Peak Hour Ar	alysis	From (	03:30 P	M to 0	5:15 PM	- Peak	1 of 1														
Peak Hour for	Entire	Inters	ection	Begins	at 04:30	PM															
04:30 PM	0	0	0	6	6	0	0	0	3	3	0	0	0	0	0	0	0	3	2	5	14
04:45 PM	0	0	0	10	10	0	0	0	1	1	1	1	0	1	3	2	0	0	7	9	23
05:00 PM	0	0	1	13	14	0	0	0	1	1	0	0	0	1	1	0	0	1	2	3	19
05:15 PM	0	0	1	10	11	0	0	0	4	4	2	0	0	2	4	0	0	2	5		26
Total Volume	0	0	2	39	41	0	0	0	9	9	3	1	0	4	8	2	0	6	16	24	82
% App. Total	0	0	4.9	95.1		0	0	0	100		37.5	12.5	0	50		8.3	0	25	66.7		
PHF	.000	.000	.500	.750	.732	.000	.000	.000	,563	.563	.375	.250	.000	.500	.500	.250	.000	.500	.571	.667	.788

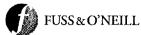


50 Alden Avenue Belchertown, MA 01007 888-389-9524 or www.datayourequested.com

N/S: North Street / Market Street E/W: North Street City, State: Northampton, Ma Client: FandO / S. Savaria File Name : PM_North @ Market Site Code : 2 Start Date : 10/1/2008 Page No : 1

							Groups	8 Print	<u>ed- PC</u>	s and P	eds - I	IVs an	d Bik	es							
		$\begin{array}{cccccccccccccccccccccccccccccccccccc$						None	•			Ma	rket S	treet			No	rth St	reet		
		Fı	om No	orth			F	rom E	ast			Fr	om So	uth			Fr	om W	est		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
03:30 PM	0	12	72	9	93	0	0	0	2	2	36	4	0	1	41	35	0	34	3	72	208
03:45 PM	0	13	52	14	79	0	0	0	4	4	52	7	0	0	59	36	0	40	0		218
Total	0	25	124	23	172	0	0	0	6	6	88	11	0	1	100	71	0	74	3	148	426
04:00 PM	0	8	45	7	60	0	0	0	1	1	30	6	1	0	37	35	0	30	5	70	168
04:15 PM	-	-		,	89	0	0	0	4	4	44	8	0	1	53	35	ŏ	41	4	80	226
04:30 PM	-				84	0	0	0	7	3	63	8	0	1	71	35	ő	35	2	72	220
	v				84 92	0	0	0	5	3	58	10	0		69	37	-		2	77	
04:45 PM						0	0		1				0	<u> </u>			0	33	/	-	239
Total	0	52	239	34	325	0	0	0	9	9	195	32	1	2	230	142	0	139	18	299	863
05:00 PM	0	21	71	13	105	1	0	0	1	2	52	7	0	1	60	39	0	40	2	81	248
05:15 PM	0	13	53	10	76	0	0	0	4	4	68	4	0	2	74	34	0	44	5	83	237
Grand Total	0	111	487	80	678	1	0	0	20	21	403	54	1	6	464	286	0	297	28	611	1774
Apprch %	0	16.4	71.8	11.8		4.8	0	0	95.2		86.9	11.6	0.2	1.3		46.8	0	48.6	4.6		
Total %	0	6.3	27.5	4.5	38.2	0.1	0	0	1.1	1.2	22.7	3	0.1	0.3	26.2	16.1	0	16.7	1.6	34.4	
PCs and Peds																					
% PCs and Peds	0	99.1	98.8	0	87.2	100	0	0	0	4.8	99.3	98.1	100	0	97.8	97.9	0		0	93	91
HVs and Bikes																					
% HVs and Bikes	0	0.9	1.2	100	12.8	0	0	0	100	95.2	0.7	1.9	0	100	2.2	2.1	0	3	100	7	9

			orth St. om No				F	None rom E			Market Street North Street From South From West										
Start Time	Left	Thru			App. Total	Left		Right		App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ar	nalysis	From (	)3:30 P	'M to 05	5:15 PM	- Peak	1 of 1														
Peak Hour for	r Entire	Inters	ection	Begins	at 04:30	PM															
04:30 PM	0	13	65	6	84	0	0	0	3	3	63	8	0	0	71	35	0	35	2	72	230
04:45 PM	0	20	62	10	92	0	0	0	1	1	58	10	0	1	69	37	0	33	7	77	239
05:00 PM	0	21	71	13	105	1	0	0	1	2	52	7	0	1	60	39	0	40	2	81	248
05:15 PM	0	13	53	10	76	0	0	0	4	4	68	4	0	2	74	34	0	44	5	83	237
Total Volume	0	67	251	39	357	1	0	0	9	10	241	29	0	4	274	145	0	152	16	313	954
% App. Total	0	18.8	70.3	10.9		10	0	0	90		88	10.6	0	1.5		46.3	0	48.6	5.1		
PHF	.000	.798	.884	.750	.850	.250	.000	.000	.563	.625	.886	.725	.000	.500	.926	.929	.000	.864	.571	.943	.962



#### TABLE A

#### LEVEL OF SERVICE CRITERIA FOR INTERSECTIONS

#### LEVEL OF SERVICE CRITERIA FOR SIGNALIZED INTERSECTIONS

LEVEL OF SERVICE	CONTROL DELAY PER VEHICLE (SEC)
А	_<10
В	>10 and <20
С	>20 and $\leq$ 35
D	>35 and <55
E	>55 and <u>&lt;</u> 80
F	>80

Source: Highway Capacity Manual 2000, Exhibit 16-2.

#### LEVEL OF SERVICE CRITERIA FOR UNSIGNALIZED INTERSECTIONS

LEVEL OF SERVICE	AVERAGE CONTROL DELAY (Sec. Per Vehicle)
Α	0 - 10
В	>10 and <15
С	>15 and <25
D	>25 and <35
E	>35 and <50
F	>50

Source: Highway Capacity Manual 2000, Exhibit 17-2.

#### Lanes, Volumes, Timings 1: North St. & King St.

	≯	-	$\mathbf{\hat{z}}$	¥	-	×.	1	t	1	1	Ļ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	ŧÎ,			4			<b>†</b>	7		-۠	
Volume (vph)	67	132	38	123	0	230	0	405	52	153	464	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0		0	0	d site	0	0		200	0		0
Storage Lanes	1		0	0		0	0		1	0		0
Taper Length (ft)	25		25	25		25	25		25	25		25
Right Turn on Red			Yes			Yes			Yes			Yes
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		143			471			282			275	
Travel Time (s)		3.3			10.7			6.4			6.3	
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Heavy Vehicles (%)	1%	3%	2%	0%	0%	1%	0%	3%	2%	1%	2%	0%
Shared Lane Traffic (%)			and of an art of the to									
Lane Group Flow (vph)	72	183	0	0	379	0	0	435	56	0	664	0
Turn Type	Perm		5.550.00 - 1880	Perm				52 C	Perm	Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4	9.7. INLAND		8	e Burran Artan			< 5.5 Black St	2	6		: "0205-2
Detector Phase	4	4		8	8			2	2	6	6	
Switch Phase			/ +x xx xx		8941 X 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			2 ( UN200 2 A			97 - 1 J. Breek	
Minimum Initial (s)	4.0	4.0		4.0	4.0	1 - <b>1</b> - <b>1</b> - <b>1</b>		4.0	4.0	4.0	4.0	
Minimum Split (s)	21.0	21.0	, print estimation	21.0	21.0	17. 2899 - X		22.0	22.0	22.0	22.0	·
Total Split (s)	27.0	27.0	0.0	27.0	27.0	0.0	0.0	53.0	53.0	53.0	53.0	0.0
Total Split (%)	33.8%	33.8%	0.0%	33.8%	33.8%	0.0%	0.0%	66.3%	66.3%	66.3%	66.3%	0.0%
Yellow Time (s)	4.0	4.0		4.0	4.0			4.0	4.0	4.0	4.0	0.000
All-Red Time (s)	1.0	1.0	v885018649	1.0	1.0	81 <b>-963</b> 4 - Roy 1	and an	2.0	2.0	2.0	2.0	2030992-2-2
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	5.0	5.0	4.0	5.0	5.0	4.0	4.0	6.0	6.0	6.0	6.0	4.0
Lead/Lag				909. 19								
Lead-Lag Optimize?	65 7 F 1 1 2628 - P	1999-1990-1990-1990-1990-1990-1990-1990	012 <b>0</b> 1 (* 1949)			1 (1999), s 5,28,	altri i s Atta			. \$9,2:05	222612111115214516	3948 CV-94
Recall Mode	None	None		None	None		5246-35 <b>2</b> 8	Max	Max	Max	Max	24.15k
Act Effct Green (s)	19.9	19.9		HONG	19.9	29:280) (J.C.	. 이는 한모양과	47.1	47.1	INICIA	47.1	1074 - E-1988 <del>9</del>
Actuated g/C Ratio	0.26	0.26			0.26	SSA SYR		0.60	0.60		0.60	
v/c Ratio	0.35	0.39	884) (3.17	en friddigele	0.92			0.39	0.06		0.00	NA CONSTRUCTION
Control Delay	28.9	24.1	1999 - 1991. 1999 - 1991.		48.5	44. 19		9.8	2.3		9.9	g y na
Queue Delay	0.0	0.0			0.0	an an the state of	1993년 11일년 11일년 - 11일년 11일년 - 11일년	0.0	0.0	a das rites.	0.0	5.893 - NEN
Total Delay	28.9	24.1			48.5			9.8	2.3		9.9	
LOS	20.0 C	24.1 C			-0.0 D			A	2.0 A		A	- 35 5
Approach Delay	, in the second s	25.4			48.5			8.9	<b>^</b>	alar	9.9	n dan s
Approach LOS		20.4 C			40.0 D			A			Â	
Queue Length 50th (ft)	29	66			128			107	0		88	
Queue Length 95th (ft)	66	121			#290			167	14		127	
Internal Link Dist (ft)		63			391			202			195	
Turn Bay Length (ft)		00			001			202	200		100	
Base Capacity (vph)	228	517			447			1114	978		1508	
Starvation Cap Reductn	0	0			· ++/ 0			0			1908	
		0						0	0			
Spillback Cap Reductn	0	0						0			0	
Storage Cap Reductn	0	-			0.85			-	0		0	
Reduced v/c Ratio	0.32	0.35			0.00			0.39	0.06		0.44	11 A) 
												- · · · · ·

North Street Condos : AM Base Condition Timing Plan: Existing Synchro 7 - Report Page 1

#### Lanes, Volumes, Timings 1: North St. & King St.

Intersection Summary
Area Type: Other
Cycle Length: 80
Actuated Cycle Length: 78
Natural Cycle: 45
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.92
Intersection Signal Delay: 20.0
Intersection Capacity Utilization 87.1% ICU Level of Service E
Analysis Period (min) 15
# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

▲ 2	→ ₀₄
53 s	27 s
<b>ν</b> [™] ø6	<b>4</b> <i>∞</i> 8
53 s	27 s

#### HCM Signalized Intersection Capacity Analysis 1: North St. & King St.

10/15/2008

	۶	-	$\mathbf{\hat{z}}$	∢		×	1	1	1	1	Ļ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	ĥ			4			<b>↑</b>	۲		41	
Volume (vph)	67	132	38	123	0	230	0	405	52	153	464	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	5.0	5.0			5.0			6.0	6.0		6.0	
Lane Util. Factor	1.00	1.00			1.00			1.00	1.00		0.95	
Frt	1.00	0.97			0.91			1.00	0.85		1.00	
Flt Protected	0.95	1.00			0.98			1.00	1.00		0.99	
Satd. Flow (prot)	1787	1787	r an the second s		1692			1845	1583		3504	
Flt Permitted	0.43	1.00	and the second		0.75			1.00	1.00		0.70	
Satd. Flow (perm)	807	1787			1286		40.2A	1845	1583		2498	
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	72	142	41	132	0	247	0	435	56	165	499	0
RTOR Reduction (vph)	0	13	0	0	86	0	0	0	22	0	0	0
Lane Group Flow (vph)	72	170	0	0	293	Ō	0	435	34	Ō	664	0
Heavy Vehicles (%)	1%	3%	2%	0%	0%	1%	0%	3%	2%	1%	2%	0%
Turn Type	Perm			Perm					Perm	Perm		
Protected Phases	set ouns	4	- 18882	. I WITH	8	-3882444 - 1798-147		2			6	13,78° -17231
Permitted Phases	4			8		1992 - 549	1. SM		2	6		40. RG.
Actuated Green, G (s)	19.9	19.9		8 - C. S. C. <b>T</b> . C.	19.9	SER 1249 - J. (1882) [	1.1823.50	47.1	47.1	460 MAR <b>4</b> 030	47.1	28281280.80
Effective Green, g (s)	19.9	19.9	SS: 252		19.9			47.1	47.1	28	47.1	91-5720
Actuated g/C Ratio	0.26	0.26	7.988 ( ) - 19 <b>7</b> 898		0.26	2020 - 1026 J.		0.60	0.60		0.60	
Clearance Time (s)	5.0	5.0	1997) 1997)	27 S.S.S.	5.0		8920-23	6.0	6.0		6.0	
Vehicle Extension (s)	3.0	3.0			3.0	n i station i sector T	2005-1283	3.0	3.0	C (199732) - Al	3.0	
Lane Grp Cap (vph)	206	456	<u> - 188</u>		328			1114	956	<u></u>	1508	
v/s Ratio Prot	200	0.09	897 986 V	987.8888 3479 1	520	889. 1. 22889.1. 1		0.24	200	87880 - 118699 - 1-	1000	(1) 날린 파랑 
v/s Ratio Perm	0.09				c0.23			0.24	0.02	- 25. CO	c0.27	
v/c Ratio	0.35	0.37			0.89	. 1.923 - 925-721	191272	0.39	0.02		0.44	~는 문제:3501 
Uniform Delay, d1	23.8	23.9			28.0		- 686	8.0	6.3	an sain	8.3	
Progression Factor	1.00	1.00			1.00	in 1. start a		1.00	1.00		1.00	
Incremental Delay, d2	1.00	0.5	an ann a'	ante d'Atte	24.8		228 N	1.0	0.1	ta da se	0.9	). Setterne :
Delay (s)	24.8	24.4	는 가장 전 시	shiftet 1997) -	52.8			9.0	6.3	94 - A. MODAN	9.3	**************************************
Level of Service	24.0 C	24.4 C		negara (194	52.0 D		38 - 13	J.O A	0.5 A	44. MARTE	э.э А	
Approach Delay (s)	1 1988 - <b>V</b> 24	24.5	St. Madd	1840/19993	52.8		1897 - S	8.7	8 (AN 19 <b>0</b> 4)	en i Martena.	9.3	
Approach LOS		24.0 C	87. K		52.0 D			A			3.5 A	
Intersection Summary				<u>.</u>			<u></u>					
HCM Average Control Delay HCM Volume to Capacity rati	0		20.5 0.57			l of Service			C			
Actuated Cycle Length (s)			78.0		um of los	· · · · · ·	2.		11.0			
Intersection Capacity Utilization	on		87.1%	IC	U Level	of Service			E			
Analysis Period (min)		lin e	15									

c Critical Lane Group

,

		Ŧ	3	I	•	•
Lane Group	EBL	EBR	NBL	NBT	SBT	T SBR
Lane Configurations	Ϋ́			 स	•	7 1
Volume (vph)	190	147	139	43	43	3 214
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	
Storage Length (ft)	0	0	75	이 가지? - 김 왕이 가		75
Storage Lanes	1	0	0			1
Taper Length (ft)	25	25	25			25
Link Speed (mph)	30			30	30	-
Link Distance (ft)	471			196	172	2
Travel Time (s)	10.7			4.5	3.9	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	8 0.88
Heavy Vehicles (%)	2%	0%	0%	0%	0%	6 1%
Shared Lane Traffic (%)						
Lane Group Flow (vph)	383	0	0	207	49	9 243
Sign Control	Stop			Free	Free	e
Intersection Summary					-	이 전에는 것이 같은 것은 것이 같은 물람

## オッチョメート キーマ

Area Type: Other Control Type: Unsignalized

Intersection Capacity Utilization 42.8% ICU Level of Service A Analysis Period (min) 15

#### HCM Unsignalized Intersection Capacity Analysis 2: North St. & Market St.

10/15/2008

	٭	$\mathbf{i}$	1	<b>†</b>	Ļ	1
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	¥			र्स	1	1
Volume (veh/h)	190	147	139	43	43	214
Sign Control	Stop			Free	Free	
Grade	0%		8 o 1937	0%	0%	한 약은 물건을 가슴을 가지 않는 것을 가슴을 가슴을 수 있다.
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	216	167	158	49	49	243
Pedestrians		ar 1965a ' ar 12	, to search			n an
Lane Width (ft)						
Walking Speed (ft/s)	. 26.2		rí - Luraviais		alan dalam	
Percent Blockage				27 <b>2</b> 23 ()		
Right turn flare (veh)			NU-ALM	Masa	MILLE	1988 - Maria Angelan, angelan kanala angelangkan kangelangkan kangelangkan kangelangkan kangelangkan kangelangk
Median type Median storage veh)				None	None	
Upstream signal (ft)					1997 - 2008 (m. 1997)	
pX, platoon unblocked	90 10 <b>8</b> 0 108		위 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19			
vC, conflicting volume	414	49	292	Stares e		
vC1, stage 1 conf vol	ાર વ્યવ્ય		LVL	10.1288.84646-4	CARAC CORRE	en die sekenden waard dat weer die die state dat die state die die state die state die state die state die stat Nationalise
vC2, stage 2 conf vol					4491 - 348	
vCu, unblocked vol	414	49	292		. (961) ASU - ASOS -	
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)		300 F V- 00 Y	u or 1, 2,000 1317 1	· · · · · · · · · · · · · · · · · · ·	1977 - C., Sooop	na – substati si na badama ke nyekara nasha yekaraban arrik a aanna a solameeti ke hababah in sa a wakari.
tF (s)	3.5	3.3	2.2			
p0 queue free %	59	84	88			
cM capacity (veh/h)	522	1025	1281			
Direction, Lane #	EB 1	NB 1	SB 1	SB 2		
Volume Total	383	207	49	243		
Volume Left	216	158	0	0		
Volume Right	167	0	0	243		에 많은 것이다. 이번 것이 같은 것이다. 것이다. 것이다. 것이다. 같은 것이 같은 것이 같은 것이 같은 것이다. 것이 같은 것이다. 것이 같은 것이다.
cSH	664	1281	1700	1700		
Volume to Capacity	0.58	0.12	0.03	0.14		
Queue Length 95th (ft)	92	11	0	0	alogan interest	
Control Delay (s)	17.5	6.5	0.0	0.0	19 - 19 - 19 - 19 - 19 - 19 - 19 - 19 -	
Lane LOS	C	A	han Netizsi	Sauce -	ter forte di servis	要:"你你你这一下,你还能说你了,你还能说你说了。"你你你能说,你你能说你?你你说你?你你说你是你是你的你。""你""你""你""你""你""
Approach Delay (s)	17.5	6.5	0.0		문란문화	동안방안된 해외는 밝혔다. 방법이 통신 방법이 방법이 통이
Approach LOS	С					
Intersection Summary		<u></u>				
Average Delay			9.1			a an
Intersection Capacity Utilization	'n		42.8%	IC	U Level o	of Service A
Analysis Period (min)			15			

## * ~ f x m Y

Lane Group	NBL	NBR SET	SER	NWL N	IWT			
Lane Configurations	Ŷ	\$	•		ŧ.			
Volume (vph)	107	34 63	122	23	117			
Ideal Flow (vphpl)	1900	1900 1900	) 1900		900			
Link Speed (mph)	30	3(	)		30			
Link Distance (ft)	403	673	}		909			
Travel Time (s)	9.2	15.3		2	20.7	20 영왕 날	8 . ISBN 188	
Peak Hour Factor	0.86	0.86 0.86	6 0.86	0.86 (	0.86			
Heavy Vehicles (%)	2%	0% 3%	5 7%	0%	3%		-261-662	
Shared Lane Traffic (%)	station and the second	and a second second	e trage a company				anna a staat	
Lane Group Flow (vph)	164	0 21	- 00000000			이 환환 관광		
Sign Control	Stop	Stop	)	S	Stop			
Intersection Summary								
Area Type:	Other							

Control Type: Unsignalized Intersection Capacity Utilization 36.2% ICU Level of Service A

Analysis Period (min) 15

## HCM Unsignalized Intersection Capacity Analysis 14: North St. & Bates St.

10/15/2008

	۲	<u>م</u>	X	$\mathbf{Y}$		×	
Movement	NBL	- NBR	SET	SER	NWL	NWT	
Lane Configurations	¥		₽			<del>با</del>	
Sign Control	Stop		Stop			Stop	·····································
Volume (vph)	107	34	63	122	23	117	
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86	
Hourly flow rate (vph)	124	40	73	142	27	136	
Direction, Lane #	NB 1	SE 1	NW 1				
Volume Total (vph)	164	215	163				
Volume Left (vph)	0	73	27				
Volume Right (vph)	40	0	136				
Hadj (s)	-0.12	0.16	-0.43				
Departure Headway (s)	4.4	4.6	4.3				
Degree Utilization, x	0.20	0.28	0.20				
Capacity (veh/h)	777	742	763				
Control Delay (s)	8.5	9.4	8.4				
Approach Delay (s)	8.5	9.4	8.4				
Approach LOS	Α	Α	Α				
Intersection Summary							
Delay			8.8		5.00		
HCM Level of Service			А				
Intersection Capacity Utili:	zation		36.2%	l (	CU Level	of Servic	e
Analysis Period (min)			15				

#### Lanes, Volumes, Timings 22: North St. & Northern Ave.

10/15/2008

	۲	Ť	Ļ	۶J	هـ.	$\rightarrow$
Lane Group	NBL	NBT	SBT	SBR	SEL	SER
Lane Configurations		र्भ	12		Ý	
Volume (vph)	4		185	3	2	9
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Link Speed (mph)		30	30	931 - 1985 - 1975 - 1	30	
Link Distance (ft)		92	212		622	
Fravel Time (s)		2.1	4.8		14.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	2%	0%	0%	0%
Shared Lane Traffic (%)						
ane Group Flow (vph)	0	211	204	0	12	0
Sign Control		Free	Free		Stop	
ntersection Summary						
Area Type:	Other					
Control Type: Unsignalize	d					
Intersection Capacity Utili	zation 23.2%			1	CU Level	of Service A

Intersection Capacity Utilization 23.2% ICU Level of Service A
Analysis Period (min) 15

10/15/2008

## Y + + + + + +

Movement	NBL NBT	SBT SBR	SEL SER		
Lane Configurations	- - स्	<u>ب</u>	¥		
Volume (veh/h)	4 190	185 3	2 9		상황가 관련 문제 (1
Sign Control	Free	Free	Stop		
Grade	0%	0%	0%		이 그렇는 그렇는 물건이다.
Peak Hour Factor	0.92 0.92 4 207	0.92 0.92 201 3	0.92 0.92 2 10		
Hourly flow rate (vph) Pedestrians	4 ZU/	201 3	2 10		
Lane Width (ft)	under Anders (1900)		er sek o defens		
Walking Speed (ft/s)			n derske er en skrive. Er	Balan di teoria di Konstead	n na mangan sa kana kana sa sa kana sa
Percent Blockage				8 SA - 28 - 28 - 28 - 28 - 28 - 28 - 28 - 2	이 않는 것을 가장한 것
Right turn flare (veh)					n an
Median type	None	None			
Median storage veh)	un in status statistica a statistica da se segur		19 8284. UMB/0244 1948	lander i sen en tradisioner en en	and the state of the state of the state
Upstream signal (ft)		Frank and a state of the second s			
pX, platoon unblocked vC, conflicting volume	204	2011 - SANS 12.2	418 203		
vC1, stage 1 conf vol	204		410 203	. 1982: 2011: 1938: 2017	ante de la contra de la composition de La composition de la c
vC2, stage 2 conf vol		259 - <b>2</b> 97 - 7			
vCu, unblocked vol	204	a an	418 203		e e l'e y fatalen i salaten a jaare si jagene
tC, single (s)	4.1		6.4 6.2		
tC, 2 stage (s)			بر را در منعد از دام المرودين رو	an ann an 11 an Ann ann an Annaich a	and the second
tF (s)	2.2		3.5 3.3		
p0 queue free %	100		100 99		
cM capacity (veh/h)	1379		594 843		
Direction, Lane #	NB1 SB1	SE 1			
Volume Total	211 204	12			
Volume Left	4 0	2		or "	national and the state of the s
Volume Right cSH	0 3 1379 1700	10 783			
Volume to Capacity	0.00 0.12	0.02			
Queue Length 95th (ft)	0.00 0.12	1	양양한홍선, 100 - 전원의 가격한 -	eren ol serie (orienes) or	
Control Delay (s)	0.2 0.0	9.7			
Lane LOS	Α	Α		para na pangana na ang pangana na ang pangana na pangana na pangana na pangana na pangana na pangana na pangan Pangana pangana	(1999) Son and Argentin (1999) Son (1999) Son (1999)
Approach Delay (s)	0.2 0.0	9.7	월 1998년 1998년 1999년 - 1999년 br>1999년 - 1999년		
Approach LOS		А			
Intersection Summary					
Average Delay	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	0.4	and the states of the		a terra ang terra ang
Intersection Capacity Utiliza	ation		CU Level of Service		As we have a statistic sector in the
Analysis Period (min)		15			

#### Lanes, Volumes, Timings 1: North St. & King St.

	الحر		$\mathbf{i}$	¥	-+	×.	1	1	1	1	Ļ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ኘ	f)			\$			1	1		<u>†</u> Ъ	
Volume (vph)	70	140	40	132	0	248	0	425	55	162	487	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0		0	0		0	0		200	0		0
Storage Lanes	1		0	0		0	0		1	0		0
Taper Length (ft)	25		25	25		25	25	di ku	25	25		25
Right Turn on Red			Yes			Yes			Yes			Yes
Link Speed (mph)	怒惑 문왕님	30			30			30			30	
Link Distance (ft)		143			471			282			275	ad 1 1 1 1 1 1 1 1.
Travel Time (s)		3.3			10.7		1991 - 19	6.4			6.3	
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Heavy Vehicles (%)	1%	3%	2%	0%	0%	1%	0%	3%	2%	1%	2%	0%
Shared Lane Traffic (%)	in vizioni i ficilitati a	2	29898-29897 - C. N		0 88 <b>8</b> 8667 - 71131	1975 - 1988 - 1988 - 1989 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	en de la sectadar		00999 LIGE 28697803		- 1000 1 (COTMOUT)	GK 1667 FI
Lane Group Flow (vph)	75	194	0	0	409	0	0	457	59	0	698	(
Turn Type	Perm			Perm	ana na data sa s	5 NK 8 SKO	an an an an tha	1997 1997 - 1993 1997 1997	Perm	Perm	1999 - C. C. B. Brinn	
Protected Phases		4			8			2			6	
Permitted Phases	4	. 1.860%94% - 1	9.0000 N.N.N.S.	8	39813 C 117293	866 N. WIMMON		- 98 88 90 - 1 <del>8 8</del> 8	2	6	998-32 (1997), [–] 199	
Detector Phase	4	4		8	8			2	$\overline{2}$	6	6	
Switch Phase	2.42° (2.70° 1.70% 9996) .		20021 - 190233	24 () - 60877. <b>7</b> ()	: <b>1</b> 000000000000000000000000000000000000	BSC 1, 173 M				s 1986-6691. ¥	2868330 - 51 👾 16	876 ( L. 200) 
Minimum Initial (s)	4.0	4.0		4.0	4.0			4.0	4.0	4.0	4.0	
Minimum Split (s)	21.0	21.0		21.0	21.0		1.17626011	22.0	22.0	22.0	22.0	
Total Split (s)	27.0	27.0	0.0	27.0	27.0	0.0	0.0	53.0	53.0	53.0	53.0	0.0
Total Split (%)	33.8%	33.8%	0.0%	33.8%	33.8%	0.0%	0.0%	66.3%	66.3%	66.3%	66.3%	0.0%
Yellow Time (s)	4.0	4.0	0.070	4.0	4.0	0.070	0.070	4.0	4.0	4.0	4.0	0.07
All-Red Time (s)	1.0	1.0		4.0 1.0	1.0	11.1.69895 - 51 1		2.0	2.0	2.0	2.0	617, 388
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	5.0	5.0	4.0	5.0	5.0	4.0	4.0	6.0	6.0 6.0	6.0	6.0	4.(
Lead/Lag	0.0	0.0	<b></b>	J.U	<b>0.0</b>	<b></b>	4.0	0.0	0.0	0.0	0.0	7.1 
Lead-Lag Optimize?		8899 N. 17				Sec.	i Mariana (19	an se		949). H98	21 - 가장한가 -	
Recall Mode	None	None	106473×1	None	None		9. S. S.	Max	Max	Max	Max	
Act Effct Green (s)	21.4	21.4		INDIA	21.4		1794년 14년 1797 1	47.0	47.0	IVIAX	47.0	
Actuated g/C Ratio	0.27	0.27	Salata kije	54.54.74G	0.27		syn i sw	0.59	0.59	830 - Kelli	0.59	385
v/c Ratio	0.27	0.27		1-DAV dars	0.27	1. T. T. S. A.	2월 14 - 174 	0.59	0.09		0.59	10년 11
Control Delay	29.0	24.1	5		58.2			10.42	2.3	1951 - 1953	10.8	113763
Queue Delay	29.0	0.0			0.0	18 - 11 R 11 1		0.0	0.0	California († 1741) Geografia	0.0	5 (1383) -
Total Delay	29.0	24.1		989 - C.A.	58.2			10.4	2.3	-73325	10.8	
LOS	29.0 C	24.1 C							·			
Approach Delay	n per production. The second second	25.5		1997 - 194	E 58.2			B 9.5	A		В 10.8	
Approach LOS					56.Z E					i jašiji		
Queue Length 50th (ft)	30	C 71		gi e stati	149			A 114	Å		В 96	
Queue Length 95th (ft)		128			#330			114	0 14		138	
Internal Link Dist (ft)	09	63			#330			202	14		138	
Turn Bay Length (ft)		00			291			202	200		190	
	010	508			400			1000			1110	
Base Capacity (vph)	219				433			1092	961		1446	
Starvation Cap Reductn	0	0			0			0	0		0	
Spillback Cap Reductn	0	0			0			0	0		0	
Storage Cap Reductn	0	0			0			0	0		0	
Reduced v/c Ratio	0.34	0.38			0.94			0.42	0.06		0.48	

North Street Condos : AM Build Condition Timing Plan: Existing Synchro 7 - Report Page 1

#### Lanes, Volumes, Timings 1: North St. & King St.

rsection Summary
a Type: Other
le Length: 80
lated Cycle Length: 79.4
ural Cycle: 50
trol Type: Actuated-Uncoordinated
imum v/c Ratio: 0.96
rsection Signal Delay: 22.8
rsection Capacity Utilization 91.2% ICU Level of Service F
lysis Period (min) 15
95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

#### Splits and Phases: 1: North St. & King St.

♠ @2	→ ₀ 4
53 s	• 27 s
<b>↓</b> [∞] ø6	<b>4</b> ∕∕ ø8
53 s	27 s

#### HCM Signalized Intersection Capacity Analysis 1: North St. & King St.

10/15/200	8
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	٦		$\mathbf{r}$	4	-	*	-	1	1	1	.↓	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	4			4			<b>≜</b>	7		₫ <b>†</b>	
Volume (vph)	70	140	40	132	0	248	0	425	55	162	487	Ó
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	5.0	5.0			5.0		84 - <i>3</i> 8	6.0	6.0		6.0	
Lane Util. Factor	1.00	1.00			1.00			1.00	1.00		0.95	
Frt	1.00	0.97			0.91			1.00	0.85		1.00	1
Flt Protected	0.95	1.00			0.98			1.00	1.00		0.99	
Satd. Flow (prot)	1787	1787			1692			1845	1583		3504	
Flt Permitted	0.42	1.00		100 C C	0.73			1.00	1.00		0.69	. a.dl.
Satd. Flow (perm)	791	1787			1259		988 - 13	1845	1583		2446	
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	75	151	43	142	0	267	0	457	59	174	524	0
RTOR Reduction (vph)	0	13	0	0	85	0	0	0	24	0	0	0
Lane Group Flow (vph)	75	181	0	0	324	Ó	0	457	35	0	698	0
Heavy Vehicles (%)	1%	3%	2%	0%	0%	1%	0%	3%	2%	1%	2%	0%
Tum Type	Perm			Perm					Perm	Perm		
Protected Phases	- 1990) - <b>2014</b> (201	4	1970 - Casser-	2016 C 1999 C	8	1997 - LAN 1998 P. 1	1.322.3280 1.1.1.0.1	2	201 (1997) 1997 (1997)	1866197	6	157567 - 2
Permitted Phases	4		G. MA	8	(1996) 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -			14	2	6		
Actuated Green, G (s)	21.4	21.4	1822	NUMBER OF STREET	21.4			47.0	47.0		47.0	9998° 1
Effective Green, g (s)	21.4	21.4			21.4			47.0	47.0		47.0	
Actuated g/C Ratio	0.27	0.27	1980 1999 - NB		0.27	1946) (241698) L.	. 2017-07 - 168899.	0.59	0.59		0.59	
Clearance Time (s)	5.0	5.0		8 . N (	5.0		21. <i>3</i> 22	6.0	6.0	5. <b>3</b> 84	6.0	8. (312) 8. (312)
Vehicle Extension (s)	3.0	3.0			3.0	- 1697,1 - 1998,888 - 1697,1 - 1998,888	A	3.0	3.0		3.0	
Lane Grp Cap (vph)	213	482			339			1092	937		1448	
v/s Ratio Prot		0.10	SEA 1111300-01130			s. 1998-60 - 1	8. 488 ° 1. 1589	0.25	9. HU <b>NT 7 1</b> H	1990 (J. 1971, 2499) 1	1918-94-97 <b>-</b> 1	
v/s Ratio Perm	0.09	0.10	197 - 199 1	3874 ()	c0.26		81 - <b>1</b> 888-1	0.20	0.02		c0.29	5.883. San 1997 - San 1997 - S
v/c Ratio	0.35	0.38		9885. C 11 7 7	0.95			0.42	0.04		0.48	
Uniform Delay, d1	23.4	23.6			28.5	Ka Alta	Stad Alt	8.8	6.8	19 - AN	9.2	
Progression Factor	1.00	1.00	11 - 1 - ANR		1.00		(11:13 - 11 (ASSE)	1.00	1.00	and solution.	1.00	
Incremental Delay, d2	1.0	0.5			36.7			1.2	0.1	n - Sala	1.2	
Delay (s)	24.4	24.1			65.2		1944 - 0.948600	10.0	6.8		10.4	90. (1997 <b>9</b> 27)
Level of Service	Ē	С. С			Ĕ	8. 48. 4	19. J. J. S.	A	Ă	ar an the second se	В	£ 982.
Approach Delay (s)	<b>-</b>	24.2			65.2	an Charles Arraig A		9.6	1999 (1999) - 1999 (1999)	an ing kanalang sa	10.4	
Approach LOS		C			Ē			Ă			В	
Intersection Summary	•											
HCM Average Control Delay			24.0	ŀ	ICM Leve	l of Servic	6		C		60.037	
HCM Volume to Capacity rat			0.63		Lander of the		and a second		9 1 - 50997		a an	
Actuated Cycle Length (s)			79.4	گر نے <b>د</b>	Sum of los	t time (s)			11.0			
Intersection Capacity Utilizat			91.2%		CU Level				F			
Analysis Period (min)			15				la de la composición de la com					
c Critical Lane Group			· . •									

		Ŧ	3	1	Ŧ	-	
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations	γ			र्स	•	7	
Volume (vph)	202	154	146	45	47	234	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Storage Length (ft)	0	0	75	14 19 28년 19 28년 - 14		75	
Storage Lanes	1	0	0			1	
Taper Length (ft)	25	25	25			25	
Link Speed (mph)	30			30	30		
Link Distance (ft)	471			196	172		
Travel Time (s)	10.7			4.5	3.9	and the base of man	a sugar and the second second second
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	
Heavy Vehicles (%)	2%	0%	0%	0%	0%	1%	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	405	0	0	217	53	266	
Sign Control	Stop			Free	Free		
Intersection Summary							
A CONTRACTOR OF A CONTRACTOR O	· *////////////////////////////////////		CONTRACTOR ( MALE)	2772		ARTENDATION AND THE ADDRESS	and the second

### メット・トレイ

Area Type:

Control Type: Unsignalized

Intersection Capacity Utilization 44.4% ICU Level of Service A Analysis Period (min) 15

Other

10/15/2008

		T	ſ	L	Ŧ								
Movement	EBL	EBR	NBL	NBT	SBT	SBR							
Lane Configurations	Y			र्भ	1	1							
Volume (veh/h)	202	154	146		47	234							
Sign Control	Stop			Free	Free								
Grade	0%			0%	10 100 1			t de la					
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88					20 A. A. A.		
Hourly flow rate (vph)	230	175	166	51	53	266							
Pedestrians	ster et etter to		de las de						3236 ²			tin a station of t	
Lane Width (ft)	양고 문화관을 읽을		의 관계 관심		f an star s	80 H ( ) 2							
Walking Speed (ft/s) Percent Blockage			1140			1848 - 1945	er Mai	Neissen i	- 1865 - 114		kira – 1938		S.
Right turn flare (veh)			- 1893 - K	Structure of the	340 - 1984 				MERSE - D		499 - 19 <b>6</b>	2019년 1919 1919년 - 1919년 - 1919년 1919년 - 1919년	
Median type		(111 <u>8)</u> (24)		None	None	1938 - 1	418. SZ	S - 192	HARLEY.				
Median storage veh)	17807 - 1883580 -	. 102838 - 4 <u>8</u>	1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998	Home			1245-128		n - Ny Silony	en is statictic. S	5384 . 2X	99.X SORA-A - 1	1992;
Upstream signal (ft)					y Meser			ti kana ja	6900-32				
pX, platoon unblocked	ah ikangka si Sada	ene l'èpidisere		na i Askas ki i den da	1997 - 1998 Barris			ti - stoten in			1	.a. 1997 - 11 B. Marso	
vC, conflicting volume	436	53	319									- 18 - 18 - 18	
vC1, stage 1 conf vol					and a converse				· · · · · · · · · · · · · · · · · · ·			/	
vC2, stage 2 conf vol													
vCu, unblocked vol	436	53	319					and the second					
tC, single (s)	6.4	6.2	4.1					e sk		Se da	k ski		
tC, 2 stage (s)		80 M 2025	- 200 - 100	e a contactor a co		28/1108.000029	e i seret	en de la companya	1.53.6 <b>6</b> .	yen aanee	en stille bet i	17 A.H. 1 M. 1 M.	
tF (s)	3.5	3.3	2.2						2011-1.CS	N SEC			de :
p0 queue free %	54	83	87	980 - 5469 i		87 - 2639 ⁻ 1-263	020-08		in the State of F		98 - CAS	81 J.M.C. P.C.	37.N c
cM capacity (veh/h)	501	1020	1252	F. 2854-8		1 : 영양한 132 		87 G.822			36.0198	9 & 1.10%	233
Direction, Lane #	EB 1	NB 1	SB 1	SB 2									
Volume Total	405	217	53	266		제 꽃하는		688-13					
Volume Left	230	166	0	0	8657 - 11139 ⁹								
Volume Right	175	0	0	266		38 N 198	\$ - 1 X						- 33
cSH	642 0.63	1252 0.13	1700 0.03	1700 0.16		1441 - C-9850			tana kao 196			laks ^a ana ar.	. 16.58
Volume to Capacity Queue Length 95th (ft)	0.63	0.13 11	0.03	U, 16 0					CAR - PR		N SEVA	137 - 28 M	-936
Control Delay (s)	19.7	6.6	0.0	0.0			1. 1.533		- Salar de			1948 - 1971	
Lane LOS	C	0.0 A	v.u	.0.0	900 - J.N	이야지 않는 신물형						1999년 - 1997년 - 1997년 - 1997년 - 1997년 - 1997년	
Approach Delay (s)	19.7	6.6	0.0	동 영관자				81 h. C			(+ 1988) 		
Approach LOS	С	Red Color Theory	ಾ ಬೇಡನ್ ಸಿಕ್ ಸಿ		an Call - Tala			Sangolari yu				. 1886 99	19 .
Intersection Summary													
Average Delay		<u>,</u>	10.0										
Intersection Capacity Utiliza	ation		44.4%	na di	CU Leve	of Servic	e			A			
Analysis Period (min)			15							· · ·			
,,													

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## メット・トレイ

North Street Condos : AM Build Condition Timing Plan: Existing Synchro 7 - Report Page 5

4	2	7	×	×	*~
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Lane Group	SEL	SER	NEL	NET	SWT	VT SWR
Lane Configurations	¥	<u></u>		¥	<u>↑</u>	<b></b>
Volume (vph)		6	0	218	227	27 0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	
Link Speed (mph)	30			30	30	30
Link Distance (ft)	291			226	155	
Travel Time (s)	6.6			5.1	3.5	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	
Heavy Vehicles (%)	0%	0%	0%	0%	2%	2% 0%
Shared Lane Traffic (%)						
Lane Group Flow (vph)	8	0	0	237	247	47 0
Sign Control	Stop			Free	Free	ee
Intersection Summary						
Area Type:	Other					
Control Type: Unsignalized						
Intersection Capacity Utiliza	tion 21.9%			10	CU Leve	evel of Service A

Analysis Period (min) 15

# HCM Unsignalized Intersection Capacity Analysis 4: Site Driveway & North St.

¥,

10/15/2008

4 2 7 X X W	
SEL SER NEL NET SWT SWR	
<u>۲</u>	
1 6 0 218 227 0	
Stop Free Free	
0% 0%	
0.92 0.92 0.92 0.92 0.92 0.92	
1 7 0 237 247 0	2 2
n Surano andre al maradare dana andra na angra dana angra dana angra angra sa	
None None	1 - Sila,
n sanan in ang ang ang ang ang ang ang ang ang an	0.66391-19
484 247 247	
aere aander vaar vaar verster e aan de aras 1 ander 1990 - bever dat e ander staar in verstelen konste verstel De eer	
484 247 247	
6.4 6.2 4.1	
u sustant comment company sense company contra the second second second second second second second second contr	-1 6/1
3.5 3.3 2.2	9178 1
546 797 1331	
SE 1 NE 1 SW 1	
8 237 247	
<u>7</u> 0 0	
748 1700 1700	oyî da
0.01 0.14 0.15	801234 8
1 0 0 9.9 0.0 0.0	
9.9 0.0 0.0 A	89 - A
A 9.9 0.0 0.0	
A A A A A A A A A A A A A A A A A A A	gen.
0.2	
21.9% ICU Level of Service A	
15	

Synchro 7 - Report Page 7

	ሻ	۴	X	$\mathbf{F}$	Ð	*
Lane Group	NBL	NBR	SET	SER	NWL	NWT
Lane Configurations	Ý		ŧ,	_		्र स
Volume (vph)	114	37	66	129	24	123
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Link Speed (mph)	30		30			30
Link Distance (ft)	403		673			909
Travel Time (s)	9.2		15.3			20.7
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86
Heavy Vehicles (%)	2%	0%	3%	7%	0%	3%
Shared Lane Traffic (%)						
Lane Group Flow (vph)	176	0	227	0	0	171 - 128 - 6 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2
Sign Control	Stop		Stop			Stop
Intersection Summary						的"新"和"新"的"新"的"新"的"新"。
Area Type:	Other	-3886 () ⁽			112232	

Control Type: Unsignalized Intersection Capacity Utilization 37.8% ICU Level of Service A Analysis Period (min) 15

# North Street Condos : AM Build Condition Timing Plan: Existing

Synchro 7 - Report Page 8

#### HCM Unsignalized Intersection Capacity Analysis 14: North St. & Bates St.

10/15/2008

	۲	۴	X	4	<b>F</b>	×	
Movement 2	NBL	NBR	SET	SER	NWL	NWT	
Lane Configurations	Y		4			ęţ,	
Sign Control	Stop		Stop			Stop	
Volume (vph)	114	37	66	129	24	123	
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86	1. 我们的问题,我们就是我们的问题。"
Hourly flow rate (vph)	133	43	77	150	28	143	
Direction, Lane #	NB 1	SE 1	NW 1				
Volume Total (vph)	176	227	171				
Volume Left (vph)	0	77	28				는 이 동생은 것 것 같은 것은 것을 통해야 한다. 같은 이 동생은 것 같은 것은 것은 것을 통해야 한다.
Volume Right (vph)	43	0	143				
Hadj (s)	-0.12	0.16	-0.43				
Departure Headway (s)	4.5	4.7	4.4				
Degree Utilization, x	0.22	0.29	0.21				
Capacity (veh/h)	769	736	752				
Control Delay (s)	8.7	9.6	8.6		것이라는		
Approach Delay (s)	8.7	9.6	8.6				
Approach LOS	A	A	A				
Intersection Summary			-				
Delay			9.0				
HCM Level of Service			Α				
Intersection Capacity Utiliz	ation		37.8%	l (	CU Level c	f Service	ə A
Analysis Period (min)			15				(c) construction of the state of the stat
		회생값.					

## ~ 2 7 × × ~

Lane Group	SEL	SER	NEL N	et swi	SWR
Lane Configurations	¥			4 Þ	,
Volume (vph)	1	5	2 2	17 233	
Ideal Flow (vphpl)	1900	1900	1900 19	00 1900	
Link Speed (mph)	30	지 않는 것이		30 30	
Link Distance (ft)	212			91 226	
Travel Time (s)	4.8			.2 5.1	
Peak Hour Factor	0.92	0.92	AND A RACE	92 0.92	
Heavy Vehicles (%)	0%	0%	0%	)% 2%	o <b>0%</b>
Shared Lane Traffic (%)	ling stagements of	<ul> <li>A static constant</li> </ul>	1	uur indukri	an a
Lane Group Flow (vph)	6	0		38 253	T MET POINT
Sign Control	Stop		Fi	ee Free	
Intersection Summary		5 S.			
Area Type:	Other				
Control Type: Unsignalize	ed				

Intersection Capacity Utilization 23.0%

Analysis Period (min) 15

ICU Level of Service A

		×	2	$\mathcal{I}$	*	
Movement	SEL	SER	NEL	NET	SWT	SWR
Lane Configurations	Ϋ́		_	र्भ	4	
Volume (veh/h)	1	5	2	217	233	
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	<u></u>	5	2	236	253	0
Pedestrians		and The Base			ente a succ	
Lane Width (ft)	공감가					[1992] · [1994] · [1995] · [1996] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [1997] · [197] · [197] · [1977] · [1977] · [1977] · [1977] · [1977] · [197
Walking Speed (ft/s)	ka siya ya		Aliteko est	Althour Maine		
Percent Blockage	80.32 A S		ARTS I PE			
Right turn flare (veh)				Mono	None	
Median type Median storage veh)		le tokasa		None	None	
Upstream signal (ft)	inin - 128	SARS-, CAR				
oX, platoon unblocked	1999 - A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A			88 J (* 12292626)		n an the second sec Second second
/C, conflicting volume	493	253	253			
vC1, stage 1 conf vol	-00000 F.M	Caller .				
/C2, stage 2 conf vol		6.33867	14 A A A		2. 329	
/Cu, unblocked vol	493	253	253	000000000000000000000000000000000000000		naroweksen i kononina – kononina senanan senanangan kutu senan kaka senan senan senan menu unan konon kaka kaka
C, single (s)	6.4	6.2	4.1			
C, 2 stage (s)						
F (s)	3.5	3.3	2.2			
o0 queue free %	100	99	100			
cM capacity (veh/h)	538	790	1324			
Direction, Lane #	SE 1	NE 1	SW 1			
Volume Total	7	238	253			
Volume Left	1	2	0			
Volume Right	5	0	0	이 가려면 가 이 가지만 가		영화 2011년 1985년 - 1992년 br>1992년 - 1992년 - 1992년 - 1992년 -
SH	733	1324	1700			na na na sa na sa na
Volume to Capacity	0.01	0.00	0.15			2019년 2019년 2019년 1월 2019년 2019년 2019년 1월 2019년 1월 2019년 1월 br>2019년 1월 2019년 1월 201
Queue Length 95th (ft)	1	0	0	Janes (Marco)		Regional de la companya de la compan
Control Delay (s)	10.0	0.1	0.0		SE STATION	
Lane LOS	A 10.0	A 0,1		sin hadasta	e na hair	
Approach Delay (s) Approach LOS	10.0 A	U. I	0.0	약의 수영한 ⁴ .	1999 (MAR) 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 19 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	stand and a standard state of the second state of the sta
Intersection Summary						
Average Delay			0.2			
Intersection Capacity Utilizatio	n		23.0%	IC.	CU Level	of Service A
Analysis Period (min)			15			

### w z y x x w

	•	•	•			•						
Lane Group	NBL	NBT	SBT	SBR	SEL	SER						
Lane Configurations		र्भ	<b>1</b> +		Υ							
Volume (vph)	4	202	194	4	3	9	698 - K					
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900						
Link Speed (mph)		30	30		30						ste sete	
Link Distance (ft)		92	212		622							
Travel Time (s)	전 영광 영	2.1	4.8		14.1							
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92						
Heavy Vehicles (%)	0%	0%	2%	0%	0%	0%						
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	224	215	0	13	0						
Sign Control		Free	Free		Stop							
Intersection Summary												
Area Type:	Other											
Control Type: Uncignolized	백자는 것 않습니다				1865 OF	1. MAR LA 1986	1865 S 18	RANGOX.	1966	3896 de 10		. 1588se

# Control Type: Unsignalized Intersection Capacity Utilization 23.8% ICU Level of Service A

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Analysis Period (min) 15

10/15/2008

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Movement	NBL	NBT	SBT	SBR	SEL	SER				
Lane Configurations		र्स	1>		Y					
Volume (veh/h)	4	202	194	4	3	9				
Sign Control		Free	Free		Stop					a
Grade		0%	0%		0%		영상은 사람이 많다.			
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92		assen i testa	- setter to setter	28 - 17-828. M.
Hourly flow rate (vph)	4	220	211	4	3	10				8 - SS-36 - S
Pedestrians Lane Width (ft)	e felinin i d					a state and the	- an Star and States and		1945)), suidei	
Walking Speed (ft/s)	988. H - N - K			24.1 1.4464					9 340	관광고가 관광 -
Percent Blockage			448-201 - 14				5446. HAR.			1.582 - 2025
Right turn flare (veh)	19489999 - 196995 -	882 - L. H.				- 1.8892 ( ) XS'	1.90.9821.092809		Sector California Sector	Parities (1985)
Median type		None	None							
Median storage veh)		e në qua në myuz		. 1. 99995339. 14	CTE MANU	. 9 1920-1933 194233	eren hen XV. verse	na ortoop reenandi po	an a	n zestanten er en
Upstream signal (ft)										
pX, platoon unblocked										
vC, conflicting volume	215				441	213				
vC1, stage 1 conf vol	1251 uppersite filmete	A.S 3176 (2000)				and the second	1.00008411.0007230953.		Mark 1997 (marks 199	an a
vC2, stage 2 conf vol									en sette	
vCu, unblocked vol	215	En 1982.			441	213	1988 - J. Partons			
tC, single (s)	4.1		* <b>1993</b> 200 P		6.4	6.2				
tC, 2 stage (s) tF (s)	2.2	1.0889.20	165 - CSRI		3.5	3.3		88139 C - 68	80	988-12 <i>822</i> 78-115
p0 queue free %	100		8797. ARK 1		99	99			1983 - 1983 	215 A 28803, DA 199
cM capacity (veh/h)	1367				575	832				
Direction, Lane #	NB 1	SB 1	SE 1							ero mo s Rivensio (1)
Volume Total	224	215	13		<u></u>					<u></u>
Volume Left	4	0	3				alifada si nasishin	- 11.5 Statistic - 181-	3939 - JUB/22369	99807 - 19898s.
Volume Right	0	4	10		88 - N					
cSH	1367	1700	749				ang a siya ang a siya			
Volume to Capacity	0.00	0.13	0.02			한 전화 가운				
Queue Length 95th (ft)	0	0	<b>1</b>				a konstruction and	a a sana a sanata a		
Control Delay (s)	0.2	0.0	9.9	8 7 7 S	경험 관계		영양수값공품	201 I B		황 관계 전
Lane LOS	A		A			Sec. S. Statuter		antes de la sera	C	ar e for to traver a fr
Approach Delay (s) Approach LOS	0.2	0.0	9.9 A						있다. 1911년 1911년 1911년 - 1911년 br>1911년 1911년 191	
Intersection Summary										
Average Delay			0.4							
Intersection Capacity Utilizat	ion		23.8%	ICL	Level	of Service		A		
Analysis Period (min)			15							

#### Lanes, Volumes, Timings 1: North St. & King St.

	٨	-+	$\mathbf{i}$	4	4	×	1	†	1	1	ţ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	¢Î			4			1	*		<b>∱</b> }	
Volume (vph)	70	139	40	129	0	242	0	425	55	161	487	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0		0	0			0		200	0		0
Storage Lanes	1		0	0		0	0		·	0		0
Taper Length (ft)	25		25	25		25	25		25	25	d de	25
Right Turn on Red		u tri i fini sente	Yes		8 (QA) (*)	Yes		5878 C 6 C 8	Yes			Yes
Link Speed (mph)	신경성이다.	30	1948 - 19 <b>8</b>	전 감정 -	30	8 . 399	1,38-1,7	30			30	
Link Distance (ft)		143			471			282		(88.45°) 1. 4.2	275	
Travel Time (s)		3.3	981. SK		10.7	1 - <b>1</b> - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		6.4			6.3	
Peak Hour Factor	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Heavy Vehicles (%)	1%	3%	2%	0%	0%	1%	0%	3%	2%	1%	2%	0%
Shared Lane Traffic (%)	66001 - 1 <b>3</b> 65 <b>8</b> 6		0.00000000000	1402200 <b>- 17</b> 020		082-0 <b>159</b> 6			899 (N <b>H (X</b> ) (	: 30° 3323-57	- eu	
Lane Group Flow (vph)	75	192	0	0	399	۰ ۱	0	457	59	0	697	0
Turn Type	Perm		red and a stranger of the second s	Perm		C	1. Mar 19 . Mar		Perm	Perm		- 1988 (1997) - Maria Maria
Protected Phases		4			8			2			6	
Permitted Phases	4		1999 - Alian	8	1.1983 C <b>U</b> -S	999997 813979 9	1.12262150	<b>4</b>	2	6	V	한국 이상한 인가
Detector Phase	4	1	- 1973 - 1974 1974 - 1974	8	<b>8</b>	214 B.B.B.		2	2	6	6	
Switch Phase	2400 (SBN <b>U</b> X		19545bar 1988	- <b>-</b>	- 6 88 <b>0</b> 8	XI - 10,6%237	17489033	۷.	4 ي	U.	0	198223
Minimum Initial (s)	4.0	4.0	800 A 328	4.0	4.0	8 . <b>E</b> ROAS		4.0	4.0	4.0	4.0	1980335
Minimum Split (s)	21.0	21.0	48.879 (J. 2020) 	21.0	21.0	9-923807	1997 1997 1998	22.0	4.0	22.0	22.0	R69873-74
- control we have have to be made	27.0	21.0	0.0	27.0	21.0	0.0	0.0	53.0	53.0	53.0	53.0	0.0
Total Split (s)	33.8%	33.8%	0.0%	33.8%	33.8%	0.0%	0.0%	66.3%		66.3%		en el la Madel Horana -
Total Split (%)		the second second second second second	0.0%			U.U%	0.0%		66.3%		66.3%	0.0%
Yellow Time (s)	4.0	4.0		4.0	4.0	8 1 <b>8</b> 8 9 8	9882 A.S.D.F	4.0	4.0	4.0	4.0	방법은 것을
All-Red Time (s)	1.0	1.0		1.0	1.0			2.0	2.0	2.0	2.0	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	5.0	5.0	4.0	5.0	5.0	4.0	4.0	6.0	6.0	6.0	6.0	4.0
Lead/Lag	38 7 6 A C C		980 - <b>8</b> 842 -		882 1998.				988 - 1983 1987 - 1983	한다. 관련하는		SECTOR
Lead-Lag Optimize?	1996 <b>- 1</b> 1998	236 <b>1</b> 2 - 726	1. (1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		8897 <u>9</u> 1 P 1910		still aparts safer	n transfer		1. 1. junio <b>1. s</b> 2006 - 11		990 N. H.S.&
Recall Mode	None	None		None	None		ke taki	Max	Max	Max	Max	
Act Effct Green (s)	21.0	21.0		t i dentina Ja	/ 21.0	1.6084 - 54777	17 1988 (A 21	47.1	47.1		47.1	661107 - VERIS
Actuated g/C Ratio	0.27	0.27			0.27	SET - A	96 C-162	0.60	0.60		0.60	
v/c Ratio	0.35	0.39			0.95			0.42	0.06		0.48	www.comerce.com
Control Delay	29.0	24.1			55.3		86 873	10.3	2.3	\$1. 488) \$1. 488	10.6	
Queue Delay	0.0	0.0		. ange i sman	0.0	131 2×15	fatz est	0.0	0.0		0.0	
Total Delay	29.0	24.1			55.3			10.3	2.3	Q7	10.6	
LOS	С	C			E		e a la Martine	В	Α		В	
Approach Delay		25.5			55.3			9.4			10.6	
Approach LOS		С			E			Α			В	
Queue Length 50th (ft)	30	70			143			114	0		96	
Queue Length 95th (ft)	69	127			#317			177	14		137	
Internal Link Dist (ft)		63			391			202			195	
Turn Bay Length (ft)									200			
Base Capacity (vph)	222	510			435			1098	965		1459	
Starvation Cap Reductn	0	0			0			0	0		0	
Spillback Cap Reductn	0	0			0			0	0		0	
Storage Cap Reductn	0	0			0			0	0		0	
Reduced v/c Ratio	0.34	0.38			0.92			0.42	0.06		0.48	
6												

North Street Condos : AM No-Build Condition Timing Plan: Existing

Synchro 7 - Report Page 1

### Lanes, Volumes, Timings 1: North St. & King St.

Intersection Summary	
Area Type: Other	
Cycle Length: 80	
Actuated Cycle Length: 79.1	
Natural Cycle: 50	
Control Type: Actuated-Uncoordinated	
Maximum v/c Ratio: 0.95	
Intersection Signal Delay: 21.9	Intersection LOS: C
Intersection Capacity Utilization 90.6%	ICU Level of Service E
Analysis Period (min) 15	
# 95th percentile volume exceeds capacity, queue may be long	jer.
Queue shown is maximum after two cycles.	

	→ o4
53 s	≠ 27 s
<b>φ</b> 6	<b>↓</b> _ ø8
53 s	27 s

#### HCM Signalized Intersection Capacity Analysis 1: North St. & King St.

	۶	-	$\mathbf{\hat{z}}$	1	←-	*	1	1	1	4	Ļ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	4			<del>4</del> )			1	7		412	
Volume (vph)	70	139	40	129	0	242	0	425	55	161	487	0
	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	5.0	5.0			5.0	St. St.		6.0	6.0		6.0	
Lane Util. Factor	1.00	1.00	1' SP-8-		1.00			1.00	1.00		0.95	
Frt	1.00	0.97			0.91			1.00	0.85		1.00	
Flt Protected	0.95	1.00			0.98			1.00	1.00		0.99	
Satd. Flow (prot)	1787	1787	fo an		1692			1845	1583		3504	
Flt Permitted	0.42	1.00			0.73			1.00	1.00		0.69	
Satd. Flow (perm)	798	1787			1263			1845	1583		2451	
Peak-hour factor, PHF	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93	0.93
Adj. Flow (vph)	75	149	43	139	0	260	0	457	59	173	524	0
RTOR Reduction (vph)	0	13	0	0	85	0	0	0	24	0	0	0
Lane Group Flow (vph)	75	179	0	0	314	0	0	457	35	0	697	0
Heavy Vehicles (%)	1%	3%	2%	0%	0%	1%	0%	3%	2%	1%	2%	0%
Turn Type	Perm			Perm					Perm	Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8					2	6		
Actuated Green, G (s)	21.0	21.0			21.0			47.0	47.0		47.0	
Effective Green, g (s)	21.0	21.0			21.0			47.0	47.0		47.0	
Actuated g/C Ratio	0.27	0.27			0.27			0.59	0.59		0.59	
Clearance Time (s)	5.0	5.0	0.24		5.0			6.0	6.0		6.0	
Vehicle Extension (s)	3.0	3.0			3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)	212	475			336			1098	942		1458	
v/s Ratio Prot		0.10						0.25				
v/s Ratio Perm	0.09				c0.25				0.02		c0.28	
v/c Ratio	0.35	0.38			0.93			0.42	0.04		0.48	
Uniform Delay, d1	23.5	23.7		SR 2	28.3			8.6	6.6		9.1	
Progression Factor	1.00	1.00			1.00			1.00	1.00		1.00	
Incremental Delay, d2	1.0	0.5			32.3			1.2	0.1		1,1	
Delay (s)	24.5	24.2			60.6			9.8	6.7		10.2	
Level of Service	C	C			E			Α	Α		В	
Approach Delay (s)		24.3			60.6			9.4			10.2	
Approach LOS		C			E	88 - N.C.		Α			В	
Intersection Summary						÷				·		
HCM Average Control Delay			22.7	Н	CM Level	of Service	1		C			
HCM Volume to Capacity ratio			0.62		- Adar - Sona	°. graxor ∠doda	n n Maraka				2000 - C.L. 2000	
Actuated Cycle Length (s)			79.0	S	um of losi	time (s)			11.0			
Intersection Capacity Utilization			90.6%			of Service	1.1983		E			
Analysis Period (min)			15									
c Critical Lane Group												

	-	Ŧ	1	1	Ŧ	•
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	- ¥			{	<b>↑</b>	
Volume (vph)	200	154	146	45	45	225
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0	0	75			75
Storage Lanes	1	0	0			1
Taper Length (ft)	25	25	25			25
Link Speed (mph)	30			30	30	
Link Distance (ft)	471			196	172	
Travel Time (s)	10.7			4.5	3.9	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88
Heavy Vehicles (%)	2%	0%	0%	0%	0%	1%
Shared Lane Traffic (%)						
Lane Group Flow (vph)	402	0	0	217	51	256
Sign Control	Stop			Free	Free	
Intersection Summary						

#### ŧ Ţ 1 ۶ •

Area Type: Other Control Type: Unsignalized

Intersection Capacity Utilization 44.3% ICU Level of Service A Analysis Period (min) 15

### HCM Unsignalized Intersection Capacity Analysis 2: North St. & Market St.

10/15/2008

	۶	$\mathbf{F}$	1	T	¥	*				
Movement	EBL	EBR	NBL	NBT	SBT	SBR		<u>.</u>		
Lane Configurations	¥			र्स	<b>†</b>	1	ala i santis sasta			
Volume (veh/h)	200	154	146	45	45	225	2 JAN 1997	- 1979 - A	영양이 관련하	
Sign Control	Stop		n	Free	Free				test to the second	
Grade	0%	80 <u>- 9</u> -90		0%	0%		성 다음 옷이 들었다.	영상 승규님이		
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88				at tajatu.
Hourly flow rate (vph)	227	175	166	51	51	256				
Pedestrians		elahan Balah.		art and and	. මැන්ත් - පත	and same that	8.24 J. J. S. S. S.		a an taon an tao an	
Lane Width (ft)		소민 물건?				2019년 2021년 202	20년 - 20년 - 21년			2018년 1971년 - 1971년 1971년 - 1971년 - 1971년 - 1971년 1971년 - 1971년 - 1971년 - 1971년 1971년 - 1971년 - 1971년 - 1971년 - 1971년 1971년 - 1971년 - 1971년 - 1971년 - 1971년 - 1971년 1971년 - 1971년 - 1971년 - 1971년 - 1971년 1971년 - 1971년 - 1971년 - 1971년 - 1971년 1971년 - 1971년 - 1971년 - 1971년 - 1971년 - 1971년 1971년 - 1971년 - 1
Walking Speed (ft/s)	u de la companya de l	landi baterti	n sakata Dabat	Northeleoko			alest esteration de	Kalas Miller	348.373	aite a tr
Percent Blockage					- 1841 - A	Stan a China a She	같은 시작했는 것	94.11.25% G.		
Right turn flare (veh)			8.00a. 440	None	Nana	1997 - 1997 (J. J. J.	C.S.S. S.C. S.S.	1997 - AN		978 C.
Median type Median storage veh)		1983: BA	-382828 - 982	None	None		i stat Danisi			1999
Upstream signal (ft)			1993-1995-1	Alika 10	1948) - 1974 1948) - 1974		A COME CAN		Sist for Galage	- 33383
pX, platoon unblocked		8884 (853) 	EN BRITERS		1987 - H C		289 - <i>Jano 1997</i> 28	994 - <i>1944</i> C.S.		
vC, conflicting volume	434	51	307	이 소송하는				202 AND		
vC1, stage 1 conf vol		Υ)	501					97840 - MARKA		96921194
vC2, stage 2 conf vol	2 3 <b>3</b> 3 3	1968 - E		20					01-369-362	
vCu, unblocked vol	434	51	307	asanan'i Sheren	19869332000113	letter 3 fritting (* 1	1998-1997 - 1998-1997 - 1998 1998 - 1999 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997	8490.000 - 139.200 -	o Mariaka di Jawa	
tC, single (s)	6.4	6.2	4.1							
tC, 2 stage (s)	- 10.198.06000 <b>.</b> 10.66	899 - CEATLAN	870-1-15 <b>07</b> 990		1989,612,111,12,18	<ul> <li>Anti-Watchell (1977) for</li> </ul>	2007-11-118828702 - 1769		an ha waxa ang ang ang ang ang ang ang ang ang an	11.1.181.12
tF (s)	3.5	3.3	2.2	18 N N	28 G.S					386
p0 queue free %	55	83	87	and a high of the second	inge of a contrast.	Titte and I defendent .				
cM capacity (veh/h)	503	1023	1265							
Direction, Lane #	EB 1	NB 1	SB 1	SB 2				-		
Volume Total	402	217	51	256						
Volume Left	227	166	0	0	0100,01, 00 C 1,0		Andres Manuelles in .			
Volume Right	175	0	0	256				황고 관광관		- 38
cSH	646	1265	1700	1700						
Volume to Capacity	0.62	0.13	0.03	0.15				지 않는 것		
Queue Length 95th (ft)	108	11	0	0						
Control Delay (s)	19.3	6.6	0.0	0.0				한 감축하는		
Lane LOS	С	Α					Maria Antonio Antonio			
Approach Delay (s)	19.3	6.6	0.0			2011일급 등의	경찰에서 내용			
Approach LOS	С									
Intersection Summary										
Average Delay			9.9	. Patri Patri	Align the start	a an an an that a t	a standard	a na gata da		
Intersection Capacity Utiliza	ition		44.3%	୍ୟୁର୍ମ୍ବା	CU Level	f Service	에 가장 것을 수	Α		
Analysis Period (min)			15							

	ሻ	۴	X	$\mathbf{i}$	f	*
Lane Group	NBL	NBR	SET	SER	NWL	NWT
Lane Configurations	¥		1.			4
Volume (vph)	112	36	66	128	24	123
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Link Speed (mph)	30		30			30
Link Distance (ft)	403		673		200 00 201	909
Travel Time (s)	9.2		15.3		ST S	20.7
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86
Heavy Vehicles (%)	2%	0%	3%	7%	0%	3%
Shared Lane Traffic (%)						n ananyoti oo aayaa ku kusta saaxayaha ka ahka na yaasayaha
Lane Group Flow (vph)	172	0	226	0	0	171
Sign Control	Stop	and we also in	Stop			Stop
Intersection Summary					÷.	
Area Type:	Other					
Control Type: Unsignalized						
Intersection Capacity Utiliza	tion 37.5%			IC	CU Level	I of Service A

Analysis Period (min) 15

	ኘ	۴	X	$\mathbf{i}$	₹ <b>`</b>	×	
Movement	NBL	NBR	SET	SER	NWL	NWT	
Lane Configurations	Ŷ	_	4			र्भ	
Sign Control	Stop		Stop			Stop	
Volume (vph)	112	36	66	128	24	123	
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86	
Hourly flow rate (vph)	130	42	77	149	28	143	
Direction, Lane #	NB 1	SE 1	NW 1				
Volume Total (vph)	172	226	171				
Volume Left (vph)	0	77	28				
Volume Right (vph)	42	0	143				
Hadj (s)	-0.12	0.16	-0.43				
Departure Headway (s)	4.5	4.7	4.4				
Degree Utilization, x	0.21	0.29	0.21				
Capacity (veh/h)	769	736	754				
Control Delay (s)	8.7	9.6	8.6				
Approach Delay (s)	8.7	9.6	8.6				
Approach LOS	Α	A	Α				
Intersection Summary							
Delay			9.0				
HCM Level of Service			Α				
Intersection Capacity Util	lization		37.5%	IC	U Level o	of Service	A
Analysis Period (min)			15				

#### ኘ 1 Ļ NJ -7

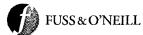
Lane Group	NBL	NBT	SBT	SBR	SEL	SER
Lane Configurations		र्भ	4		۲	
Volume (vph)	4	200	194	3	2	9
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Link Speed (mph)		30	30		30	
Link Distance (ft)		92	212		622	
Travel Time (s)		2.1	4.8		14.1	이 같은 것은
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	2%	0%	0%	0%
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	221	214	0	12	0
Sign Control		Free	Free		Stop	
Intersection Summary						
Area Type:	Other					
Control Type: Unsignalized						

Intersection Capacity Utilization 23.7%

ICU Level of Service A Analysis Period (min) 15

10/15/2008

	ኘ	Ť	¥	N	الله ا	$\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{\mathbf{$
Movement	NBL	NBT	SBT	SBR	SEL	SER SER STATISTICS
Lane Configurations		<del>ا</del> ب	4		۲	
Volume (veh/h)	4	200	194	3	2011 - 2016 ATT -	
Sign Control		Free	Free		Stop	
Grade		0%	0%		0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	4	217	211	3	2	10
Pedestrians			x t aborta			na sun antica de la companya de la c
Lane Width (ft)						
Walking Speed (ft/s)	1.00 (mail) no 44			daar in date s		2. 1913年1月11月1日(1919年1月) - 1月1日日 - 1月1日日(1919年1月1日) - 1月1日(1919年1月1日)(1919年1月1日) - 1月1日(1919年1日)
Percent Blockage		영양하는		1987 - 1945 Alexandre - 1945		
Right turn flare (veh)	ang ngangan sa sa	28 <b>1</b> - 285 - 5	en an traite	1268224 - 5 ta-	rinda. B	
Median type		None	None		5 K. J	
Median storage veh)	andra - Addar	-750.2888	i dina.	1997 - SARAN I.	7860 - 1954a)	
Upstream signal (ft)						
oX, platoon unblocked	214	N. JOSKI A			400	212
vC, conflicting volume vC1, stage 1 conf vol	214	86-89-023 		1968 - 1 <b>9</b> 83	439	<b>414</b>
vC2, stage 2 conf vol	#11:3:45-1:2	361.0368-3	389 - WAR	1882 - 2685	- 2000 a Cre	
vCz, stage z com vol	214	8. S. 2489. C.	2006. N 1860		439	212
C, single (s)	4.1				6.4	
C, 2 stage (s)	9 - XSSOT • 1289	1973년 <u>영</u> 종의 1973년 1979년 - 1973년 br>1973년 - 1973년 -			V.T.	2 192 <b>2 : 슈</b> 사는 방법은 1922년 1월 1922년 - 1922년 1월 1932년 1월 19 
F (s)	2.2	1993 - 1983 1983 - 1983			3.5	3.3
p0 queue free %	100	948 - 1994) 1			100	
cM capacity (veh/h)	1368				577	833
		~~ 4	~~ 4	- andra Graheva Milie		i sana in <del>a sa</del> na kabula kana ka muningi kabula kana kana kana kana kana kana kana ka
Direction, Lane #	NB 1	SB 1	SE 1			
Volume Total	222	214	12			
Volume Left	4	0	2	218.38×10.1		
Volume Right	0	3	10	Real Street of Street of Street		
cSH	1368	1700	771		68 <b>8</b> 62 ⁷ -	
Volume to Capacity	0.00	0.13	0.02	20. H <b>o</b> & P		
Queue Length 95th (ft)	0 0.2	0 0.0	1 9.7	sto steachtr		
Control Delay (s) Lane LOS	0.2 A	0.0	9.7 A			
Approach Delay (s)	0.2	0.0	9.7		1981 - Mar	
Approach LOS	0.2	0.0	9.7 A	- 2011 (26)。		2017년 1월 19일 - 1일 19일 19일 19일 19일 19일 19일 19일 19일 19일
Intersection Summary			~			
Average Delay			0.3			
Average Delay Intersection Capacity Utilizat	lion		23.7%	Sart da m		I of Service
Analysis Period (min)				st Prink	O Level	n on ô genere a state de la state de la service de la s
maiysis renoù (min)			15			



#### TABLE A

#### LEVEL OF SERVICE CRITERIA FOR INTERSECTIONS

#### LEVEL OF SERVICE CRITERIA FOR SIGNALIZED INTERSECTIONS

LEVEL OF SERVICE	CONTROL DELAY PER VEHICLE (SEC)
Α	0
В	>10 and <u>&lt;</u> 20
С	$>20$ and $\leq 35$
D	>35 and <55
E	>55 and <80
F	>80

Source: Highway Capacity Manual 2000, Exhibit 16-2.

#### LEVEL OF SERVICE CRITERIA FOR UNSIGNALIZED INTERSECTIONS

LEVEL OF SERVICE	AVERAGE CONTROL DELAY (Sec. Per Vehicle)
Α	0 - 10
В	>10 and <15
С	>15 and <25
^v D	>25 and <35
E	>35 and <50
F	>50

Source: Highway Capacity Manual 2000, Exhibit 17-2.

#### Lanes, Volumes, Timings 1: North St. & King St.

	٦	-+	$\mathbf{i}$	1	◄—	×.	1	Ť	1	1	Ļ	1
Lane Group	EBL	EBT	EBR	WBL.	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$				1		<b>∱</b> }	
Volume (vph)	68	92	16	98	0	384	0	525	57	150	468	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0		0	0		25	0	1991-1991-2	200	0		0
Storage Lanes	1		0	0		0	0		1	0		0
Taper Length (ft)	25		25	25		25	25		25	25		25
Right Turn on Red			Yes			Yes			Yes			Yes
Link Speed (mph)		30			30			30		944 - X	30	
Link Distance (ft)		143			471			282			275	
Travel Time (s)		3.3			10.7			6.4			6,3	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	1%	0%	0%	1%	0%	0%	0%	1%	2%	1%	1%	0%
Shared Lane Traffic (%)												
Lane Group Flow (vph)	72	115	0	0	513	0	0	559	61	0	658	0
Turn Type	Perm			Perm					Perm	Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8					2	6		
Detector Phase	4	4		8	8	18. SK		2	2	6	6	
Switch Phase												
Minimum Initial (s)	4.0	4.0		4.0	4.0			4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0		20.0	20.0			20.0	20.0	20.0	20.0	
Total Split (s)	27.0	27.0	0.0	27.0	27.0	0.0	0.0	53.0	53.0	53.0	53.0	0.0
Total Split (%)	33.8%	33.8%	0.0%	33.8%	33.8%	0.0%	0.0%	66.3%	66.3%	66.3%	66.3%	0.0%
Yellow Time (s)	3.5	3.5		3.5	3.5			3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5		0.5	0.5			0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
Lead/Lag											신사람값	
Lead-Lag Optimize?												
Recall Mode	None	None		None	None			Max	Max	Max	Max	
Act Effct Green (s)	19.0	19.0			19.0			49.2	49.2		49.2	
Actuated g/C Ratio	0.25	0.25		역 14 1 - 54 1 스럽지 - 14 2	0.25			0.65	0.65		0.65	화가 것
v/c Ratio	0.64	0.24			0.91			0.46	0.06		0.42	
Control Delay	53.2	21.4			35.7			9.2	2.0	18 . C	8.4	
Queue Delay	0.0	0.0			0.0			0.0	0.0		0.0	
Total Delay	53.2	21.4			35.7			9.2	2.0		8.4	
LOS	D	С			D			Α	Α		A	
Approach Delay		33.6			35.7			8.5			8.4	
Approach LOS	·	С			D			. A			Α	
Queue Length 50th (ft)	30	39			126			136	0		82	
Queue Length 95th (ft)	#89	79			#304			211	13		119	
Internal Link Dist (ft)		63			391			202			195	
Turn Bay Length (ft)									200			
Base Capacity (vph)	136	571			635			1214	1043		1555	
Starvation Cap Reductn	0	0			0			0	0		0	
Spillback Cap Reductn	0	0			0,			0	0		0	
Storage Cap Reductn	0	0			0			0	0		0	
Reduced v/c Ratio	0.53	0.20		t 1	0.81			0.46	0.06		0.42	
												, ,

North Street Condos : PM Base Condition Timing Plan: Existing Synchro 7 - Report Page 1

#### Lanes, Volumes, Timings 1: North St. & King St.

Intersection Summary
Area Type: Other
Cycle Length: 80
Actuated Cycle Length: 76.2
Natural Cycle: 50
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.91
Intersection Signal Delay: 17.9
Intersection Capacity Utilization 90.7% ICU Level of Service E
Analysis Period (min) 15
# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

#### Splits and Phases: 1: North St. & King St.

<b>↑</b> ø2	A 04
53 s	27 s
v [™] ø6	<b>a</b> 8
53 s	27 s

#### HCM Signalized Intersection Capacity Analysis 1: North St. & King St.

	٠	-	$\mathbf{r}$	<b>F</b>		×.	1	1	1	1	Ŧ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	ţ,						1	7		<u>ብ</u> ተ	
Volume (vph)	68	92	16	98	0	384	0	525	57	150	468	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0			4.0			4.0	4.0		4.0	
Lane Util. Factor	1.00	1.00			1.00			1.00	1.00		0.95	
Fri	1.00	0.98			0.89		F. 38	1.00	0.85		1.00	
Flt Protected	0.95	1.00			0.99			1.00	1.00		0.99	
Satd. Flow (prot)	1787	1858			1675		한 영상은	1881	1583		3531	18-5
Flt Permitted	0.24	1.00			0.90			1.00	1.00		0.67	
Satd. Flow (perm)	449	1858			1527		e XXI.	1881	1583		2408	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	72	98	17	104	0	409	0	559	61	160	498	0
RTOR Reduction (vph)	0	8	0	0	186	0	0	0	22	0	0	0
Lane Group Flow (vph)	72	107	0	0	327	0	0	559	39	0	658	0
Heavy Vehicles (%)	1%	0%	0%	1%	0%	0%	0%	1%	2%	1%	1%	0%
Tum Type	Perm			Perm					Perm	Perm		
Protected Phases	1.169002000084	4	1.125.136 0.67.6380	8617 - 19896 -	8			2	1 1. AV 6435 - 1. 1. 1. A	eo constituinte non	6	1996 (1983) 1996 (1983)
Permitted Phases	4			8		NG SP 18			2	6		
Actuated Green, G (s)	19.0	19.0	571/161 - Willia	an li tari.a	19.0		Webs and the first sec	49.2	49.2	20909194 - SAUD-1	49.2	
Effective Green, g (s)	19.0	19.0			19.0			49.2	49.2		49.2	
Actuated g/C Ratio	0.25	0.25			0.25		al a 23126.	0.65	0.65		0.65	10010
Clearance Time (s)	4.0	4.0	1999 (MA)	1818 - S.	4.0			4.0	4.0	1.484.4	4.0	ge state i
Vehicle Extension (s)	3.0	3.0	999 - Lie 9 39 - 9		3.0			3.0	3.0	9 9 . A	3.0	
Lane Grp Cap (vph)	112	463		8	381			1215	1022		1555	<u></u>
v/s Ratio Prot	2000 • 29 <del>77</del> 899	0.06	areana a 1990	1997 AN 1993	2009 - USBERS	11.1.999117 - 891871 		c0.30	1999 - <b>199</b> 96	1. 866 6 G	1.000000000	
v/s Ratio Perm	0.16				c0.21			89 99 <b>8</b>	0.02		0.27	
v/c Ratio	0.64	0.23	112 - SS891 - 1127		0.86	n - 51,6882 - 53 5		0.46	0.04	1.58511.000.085	0.42	
Uniform Delay, d1	25.6	22.8			27.3			6.8	4.9		6.6	\$1.5- <i>7.</i> 6
Progression Factor	1.00	1.00	na na nativ	n ( ), (),	1.00			1.00	1.00	an a	1.00	
Incremental Delay, d2	12.0	0.3		1. S. S.	17.1			1.3	0.1	1991 - 1994 1995 - 1995	0.8	e e sec
Delay (s)	37.5	23.0		5 - Marson - 1995 -	44.4			8.1	5.0		7.4	na sensitiv.
Level of Service	D	Ċ	91. JAG		D		le Blai	Α	A	in the	Á	
Approach Delay (s)		28.6	and dependent		44.4		17. A 1999.	7.8	19906411 11530	call ( l'haur	7.4	an sharar s
Approach LOS		C			D			Å			A	
Intersection Summary			<u>.</u>								•	
HCM Average Control Delay HCM Volume to Capacity ratio		말했다.	19.1 0.57	Ref. F	ICM Leve	l of Servic	θ	1000	В			
Actuated Cycle Length (s)			76.2	-	um of los	t time (c)			8.0			
Intersection Capacity Utilizatio	n n		90.7%			of Service			0.0 E			
Analysis Period (min)	1 <b>1</b>	an Alina	90.7% 15		CO Level							
c Critical Lane Group			19									

c Critical Lane Group

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	-	•	١	I	•	•
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	Y	_		र्भ	↑	مممممم
Volume (vph)	148	151	217	33	65	265
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0	0	75			75
Storage Lanes	1	0	0			1
Taper Length (ft)	25	25	25			25
Link Speed (mph)	30			30	30	1
Link Distance (ft)	471			196	172	
Travel Time (s)	10.7			4.5	3.9	
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95
Heavy Vehicles (%)	3%	3%	0%	3%	0%	
Shared Lane Traffic (%)						
Lane Group Flow (vph)	315	0	0	263	68	279
Sign Control	Stop			Free	Free	
Intersection Summary						
				A MARKEN IN THE REAL PROPERTY OF		

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Area Type: Other Control Type: Unsignalized

Intersection Capacity Utilization 44.5% ICU Level of Service A Analysis Period (min) 15

#### HCM Unsignalized Intersection Capacity Analysis 2: North St. & Market St.

10/15/2008

	۶	$\mathbf{i}$	•	1	ţ	~			-		
Movement	EBL	EBR	NBL	NBT	SBT	SBR					
Lane Configurations	Y			÷.	<b>†</b>	7					
Volume (veh/h)	148	151	217		65	265	신경제공품	경영 문	연구 관련을		
Sign Control	Stop			Free	Free						
Grade	0%	AL.A	a de	0%	0%		공간 영화		에서 공간을	연기관	영화 관람 중
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95			anta indexa		
Hourly flow rate (vph)	156	159	228	35	68	279		88 - 19 al			
Pedestrians	an kuna vir		N + 1 B + Josta	era suo see		, alter alter i	e and are d				
Lane Width (ft)					e sta						
Walking Speed (ft/s)				generation and ge					Querte l'doctora	an airtean a	
Percent Blockage	66741.581			2011년 1월 1911년 1월 1911년 1월		an in	813328-33			Res 1946 -	
Right turn flare (veh)			890-2988-988		201 <b>6 (</b> 1986) -		an a				-01880-01880-0
Median type			C	None	None			Contraction of the second s		- 326 387	
Median storage veh)		19403-19404	- 1998 - 2019) - 1998 - 2019)			601 31 319		. 345.0 m 7.528	911 <b>9</b> 82, 818	94 - 1289 N.S.K	i kereki a
Upstream signal (ft)		-1880-1894 C	- 1988 - 1983 - 1988 - 1983	11 SAG. (U.S.)	4. NY 19	248-1-1985 				:::::::::::::::::::::::::::::::::::::	1997 - 1987 - 1988 Amerika
pX, platoon unblocked vC, conflicting volume	560	68	347	89 - 69 - 69 - 69 - 69 - 69 - 69 - 69 -	8-1922-04				89. ( <i>6</i> 88%)	SMC - SMC2 -	
vC1, stage 1 conf vol	300	00	- 041		140 - S <b>B</b> (2				212-2224F		18 A 438 44
vC1, stage 1 confivor			G addinad	1. S <b>M</b> E	9	3 <b>8</b> 49359			erenii (* 1		9 12 S L 322 -
vCu, unblocked vol	560	68	347	82.73869 - 147.	TREAR AND A	1619-161 - 581 - 581	BA (PRESCO)	29. 19882 - 1 -		1989 - 1968 - 19	2020-0-10000-0-10 1
tC, single (s)	6.4	6.2	4.1				18.278 <i>.3</i> 2		6 223		86 . N. S. S
tC, 2 stage (s)	ne i <b>Mi</b> ziro?	·····	C 1. 1992 - 1999	6 ( <i>1999 - 199</i> 7)	alling to the	3802 S - C - MC	S	an 1983 na 1	unu 2000 (Brail	BARRONOLOU - UD	89 11 - 88 33 -
tF (s)	3.5	3.3	2.2						1. 1. j.		
p0 queue free %	61	84	81	(58884 - 15 9 47° (6° ).	0709/10 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		983. / Y / 1898/9	us a strategy (1997) a s			
cM capacity (veh/h)	397	992	1223								
Direction, Lane #	EB 1	NB 1	SB 1	SB 2							
Volume Total	315	263	68	279							
Volume Left	156	228	0	0	- 1,4 ga 191	anten festi inde	un or taxaa			an it weren nuo	ante en la consecta o
Volume Right	159	0	0	279						888	
cSH	569	1223	1700	1700						. in the states	
Volume to Capacity	0.55	0.19	0.04	0.16		81. S.					
Queue Length 95th (ft)	84	17	0	0							
Control Delay (s)	18.9	7.7	0.0	0.0			일정전했다				
Lane LOS	С	А									
Approach Delay (s)	18.9	7.7	0.0				한 가장 생활	1 방법 - 위			영양이는
Approach LOS	С										
Intersection Summary				÷							
Average Delay			8.6								
Intersection Capacity Utilization	on		44.5%	S IC	U Level	of Servic	ce .		Α		
Analysis Period (min)			15								

#### North Street Condos : PM Base Condition Timing Plan: Existing

	۲	۴	X	$\mathbf{F}$	£	×
Lane Group	NBL	NBR	SET	SER	NWL	NWT
Lane Configurations	·····································		ef -			र्स
Volume (vph)	49	28	111	194	38	47
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Link Speed (mph)	30		30			30
Link Distance (ft)	403		673			909
Travel Time (s)	9.2		15.3			20.7
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86
Heavy Vehicles (%)	10%	0%	2%	2%	0%	6%
Shared Lane Traffic (%)						
Lane Group Flow (vph)	90	0	355	0	0	99
Sign Control	Stop		Stop			Stop
Intersection Summary						
Area Type: Control Type: Unsignalized	Other					

Intersection Capacity Utilization 36.7%

ICU Level of Service A Analysis Period (min) 15

# HCM Unsignalized Intersection Capacity Analysis 14: North St. & Bates St.

10/15/2008

	7	۴	X	$\rightarrow$	₹ <b>`</b>	×		
Movement	NBL	NBR	SET	SER	NWL	NWT		
Lane Configurations	Y		4			4		
Sign Control	Stop		Stop	an a		Stop	영상 영향 영향 영향	
Volume (vph)	49	28	111	194	38	47		
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86		
Hourly flow rate (vph)	57	33	129	226	44	55		
Direction, Lane #	NB 1	SE 1	NW 1					
Volume Total (vph)	90	355	99					
Volume Left (vph)	0	129	44				장아가 물고 있는 것	
Volume Right (vph)	33	0	55					
Hadj (s)	-0.11	0.11	-0.19					이 가장을 가지 않는다. 이 가장을 가지 않는다. 이 가장을 가지 않는다.
Departure Headway (s)	4.4	4.4	4.7					
Degree Utilization, x	0.11	0.43	0.13					
Capacity (veh/h)	777	803	697					
Control Delay (s)	8.0	10.6	8.4					
Approach Delay (s)	8.0	10.6	8.4					
Approach LOS	Α	В	Α					
Intersection Summary								
Delay			9.8					
HCM Level of Service			Α			and the same of the second states of the second sta	- EMPROVATION - ALL COMPANY - ALL CO	
Intersection Capacity Utiliz	ation		36.7%	) IC	U Level	Service	A	
Analysis Period (min)	and a start and a start of the	مىرىغى مەمەر	15			and a subscript of the state of the	و و و و و و و و و و و و و و و و و و و	warde fan taal aan a

	ſ		¥	Ð	-	<b>→</b>
Lane Group	NBL	NBT	SBT	SBR	SEL	SER
Lane Configurations		र्स	4		Y	
Volume (vph)	4	123	265	8	2	4
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Link Speed (mph)		30	30		30	
Link Distance (ft)		92	212		622	
Travel Time (s)		2.1	4.8		14.1	
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	150	321	0	7	0
Sign Control		Free	Free		Stop	
Intersection Summary						
Area Type: C	Other					

### Y + + + + + + +

Control Type: Unsignalized

Intersection Capacity Utilization 24.4% ICU Level of Service A Analysis Period (min) 15

10/15/2008

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Movement	NBL NBT	SBT SBR	SEL SER	
Lane Configurations	<del>ا</del>	4	Y	
Volume (veh/h)	4 123	265 8	2 4	
Sign Control	Free	Free	Stop	
Grade	0%		0%	
Peak Hour Factor	0.85 0.85 5 145	0.85 0.85 312 9	0.85 0.85 2 5	
Hourly flow rate (vph) Pedestrians	3 3 143	91Z 9	2 3	
Lane Width (ft)	in an			
Walking Speed (ft/s)	1	ee Ark Look Arteliae 1931.	an a	n 201 - Na general 2010 in 1988 - Marche Indones, 1987 - 1986 - 1987 - 1987 - 1987 - 1987 - 1987 - 1987 - 1987
Percent Blockage	전화 화가는 것	2482 X.S. S.		
Right turn flare (veh)				
Median type	None	None		
Median storage veh)	and a state of the		genalis intervi constato dan	an a cherrente consideration construction and the second construction of the second second second second second
Upstream signal (ft)				
pX, platoon unblocked	2004		471 316	
vC, conflicting volume vC1, stage 1 conf vol	321		471 316	
vC2, stage 2 conf vol	ter an terretaria de la composición de			
vCu, unblocked vol	321	e da esta de la composición de la compo	471 316	에는 것같은 것은 것은 것은 것은 것은 것은 것은 것은 것은 것을 가장했다. 것은 것 같은 것은 것을 가장하는 것을 받았다. 같은 것 같은 것은 것 같은 것은 것 같은 것은 것 같은 것 같은 것
tC, single (s)	4.1	9 - <b>2</b> 0 - 12 - 12 - 13	6.4 6.2	
tC, 2 stage (s)			· · · · · · · · · · · · · · · · · · ·	nangereen oordewak en een toolowen oordenaarde oordenaarde oorden. Deeld oorden oorden oorden oorden oorden oor Gebeure
tF (s)	2.2		3.5 3.3	
p0 queue free %	100	1817 ⁻ Mardos I., 11 an. 21 S. Junio	100 99	
cM capacity (veh/h)	1250		553 729	
Direction, Lane #	NB1 SB1	SE 1		
Volume Total	149 321	7		
Volume Left	50 09	2 U 1944 - BATHLEA		
Volume Right cSH	0 9 1250 1700	5 659		
Volume to Capacity	0.00 0.19	0.01		
Queue Length 95th (ft)	0.00 0.10	v.vi 1		수는 사람은 3월 187일은 수 2일을 가장했습니다. 수별이다. 가장 이 가지 않는 
Control Delay (s)	0.3 0.0	10.5		
Lane LOS	Α	В		n na sente l'antico este superior de la sente de la sente de la se
Approach Delay (s)	0.3 0.0	10.5	문 김 왕이야 한 것을 했다.	
Approach LOS		В		
Intersection Summary				
Average Delay		0.2		
Intersection Capacity Utilizat	ion		CU Level of Service	
Analysis Period (min)		15		
and the second secon				

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SB
Lane Configurations	٦.	 }			\$			•	1		<b>€</b> ↑	
Volume (vph)	71	98	17	104	0	405	0	551	61	159	491	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	190
Storage Length (ft)	0		0	0		25	0		200	0		
Storage Lanes	1		0	0	19 AL 19 AL	0	0		1	0		
Taper Length (ft)	25		25	25	17 - C.S.S.	25	25		25	25	영상 승규는 것	
Right Turn on Red			Yes			Yes		9.00 ( AN AN AN AN	Yes			Y
Link Speed (mph)		30	한 한것		30		84 - 198 1	30			30	61-11
Link Distance (ft)		143	·		471	takat, di si si si di si		282			275	8° 4 - 124
Travel Time (s)		3.3			10.7			6.4			6.3	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.
Heavy Vehicles (%)	1%	0%	0%	1%	0%	0%	0%	1%	2%	1%	1%	0
Shared Lane Traffic (%)	299-25 1202223 119	ana ( 1947-1969 - 1			shuku ke Seeta k	na Centrus Stillas ch	128000000000000000000000000000000000000	19929 - 199588		Ferri	an an ann an	100994 ( ) - E
Lane Group Flow (vph)	76	122	0	0	542	0	0	586	65	0	691	
Turn Type	Perm	17. 2010. <u>– 41</u> 76. 9	90000 - 198 <b>9</b> 077 - 1	Perm		a (Massee 1993	se de la Câlilia de	V 1 JORAN I	Perm	Perm	NAN, 10 T. CARDO	
Protected Phases		4			8	88 - 86 d		2		5.736%	6	1993) 1993)
Permitted Phases	4		9922000 - Jone 7 - 1	8	997 - A. A. T. A.	Serie - College	1993 St. 1771 1983	8977 - C. 19 <del>73</del> 87	2	6	. 18 M 929 11 783	
Detector Phase	4	4		8	8	ite de la com		2	$\overline{2}$	Ğ	6	69
Switch Phase	19, 1, 17, 17, 19, 19, 19, 19, 19, 19, 19, 19, 19, 19	18 FRISLE <b>N</b> (* 11)	99500AC _3000	X8.48(34, 340) ¥	1980) - 28 <b>2</b> 014	8888. UN 1. 88943	1.300039 () 1.233	20055 - 111 <del>00</del> 7			o 460 408 m u.h. <u>∓</u> 660	877359 - CS
Minimum Initial (s)	4.0	4.0	1988 - S.S.	4.0	4.0			4.0	4.0	4.0	4.0	\$8
Minimum Split (s)	20.0	20.0	Sigilar - 5889.	20.0	20.0	1980 - 1997 - 1980. 1980 - 1997 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980 - 1980	1973 (S. S. S. S. S.	20.0	20.0	20.0	20.0	
Total Split (s)	27.0	27.0	0.0	27.0	27.0	0.0	0.0	53.0	53.0	53.0	53.0	
Total Split (%)	33.8%	33.8%	0.0%	33.8%	33.8%	0.0%	0.0%	66.3%	66.3%	66.3%	66.3%	0.0
Yellow Time (s)	3.5	3.5	0.070	3.5	3.5	0.070	0.070	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	2017 - AL 2017 2017 - AL 2017	0.5	0.5	97 (J. 1979) - J.	1849 - 19979	0.5	0.5	0.5	0.5	K. 4-283
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	C
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	د 4
Lead/Lag	4.0		7.0		4.V	4.0	4.V	4.0	4.0	4.V	4.0	• 51 - 136
Lead-Lag Optimize?	e star till		1980 A. 1978 P.		영화 영양의 문화	ange også de b	80 de 1993. Statistica	97	1321-1327	119338594	19892 - NASO	9.889
Recall Mode	None	None	20. ⁻ 1. 22	Mono	Mono		uto - MA	Max	0.30M238	Max	Hou	
contract wavelength and show where the start of the start of the	20.6	20.6	396 39.897 -	None	None 20.6		38. HAM	49.1	Max 49.1	IVIAX	Max 49.1	
Act Effct Green (s) Actuated g/C Ratio	0.27	0.27		n an tha	0.27	88 . 86 . I	u The local	0.63	49.1 0.63	5 - HIST 1.7	49.1 0.63	
v/c Ratio	0.62	0.21	ge star			See An S	68 - 1748 -		and the second second	는 않았는?	Charles - Coracona	27 98.
- Martin - Constant - Consta			18.20 - 143		0.93			0.49	0.06	gan italiya	0.47	
Control Delay Queue Delay	49.2 0.0	21.4 0.0			40.0 0.0			10.0	2.0	과 문화관	9.3	et fogg
							s. Sector	0.0	0.0		0.0	
Total Delay	49.2	21.4			40.0	5 1258 n. A		10.0	2.0		9.3	
	D NGC STREE	C			D			A	A A		A	
Approach Delay		32.0			40.0			9.2		n di Ja	9.3	
Approach LOS		C			D			A			A	
Queue Length 50th (ft)	32	42			148			148	0		90	
Queue Length 95th (ft)	#93	83			#342			225	14		131	
Internal Link Dist (ft)		63			391			202	000		195	
Turn Bay Length (ft)	407							4400	200			
Base Capacity (vph)	137	559			624			1189	1025		1464	
Starvation Cap Reductn	0	0			0			0	0		0	
Spillback Cap Reductn	0	0			0			0	0		0	
Storage Cap Reductn	0	0			0			0	0		0	
Reduced v/c Ratio	0.55	0.22			0.87			0.49	0.06		0.47	

North Street Condos : PM Build Condition Timing Plan: Existing Synchro 7 - Report Page 1

Intersection Summary
Area Type: Other
Cycle Length: 80
Actuated Cycle Length: 77.7
Natural Cycle: 55
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.93
Intersection Signal Delay: 19.4
Intersection Capacity Utilization 94.6% ICU Level of Service F
Analysis Period (min) 15
# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases:	1: North St. & King St.
--------------------	-------------------------

↑ _{ø2}	ø4
53 s	27 s
ø6	<b>4</b> Ø8
53 s	27 s

#### HCM Signalized Intersection Capacity Analysis 1: North St. & King St.

	۶	-+	$\mathbf{F}$	4	◄	×.	1	1	1	1	ţ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	4			4			↑	7		t}}	
Volume (vph)	71	98	17	104	0	405	0	551	61	159	491	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0			4.0			4.0	4.0		4.0	
Lane Util. Factor	1.00	1.00			1.00			1.00	1.00		0.95	
Frt	1.00	0.98			0.89			1.00	0.85		1.00	
Fit Protected	0.95	1.00			0.99			1.00	1.00		0.99	
Satd, Flow (prot)	1787	1858			1675			1881	1583		3531	
Flt Permitted	0.25	1.00			0.90			1.00	1.00		0.65	
Satd. Flow (perm)	462	1858			1522			1881	1583		2318	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	76	104	18	111	0	431	0	586	65	169	522	0
RTOR Reduction (vph)	0	8	0	0	180	0	0	0	24	0	0	0
Lane Group Flow (vph)	76	114	0	0	362	0	0	586	41	0	691	0
Heavy Vehicles (%)	1%	0%	0%	1%	0%	0%	0%	1%	2%	1%	1%	0%
Turn Type	Perm			Perm					Perm	Perm		
Protected Phases		4		·	8	· ( )() /// · · · · · · /// ///		2			6	
Permitted Phases	4			8					2	6		
Actuated Green, G (s)	20.6	20.6	o an co pana	1.4880.89 1. 42	20.6		C 1. 4 25000	49.1	49.1		49.1	
Effective Green, g (s)	20.6	20.6	* 38		20,6			49.1	49.1		49.1	
Actuated g/C Ratio	0.27	0.27			0.27			0.63	0.63		0.63	
Clearance Time (s)	4.0	4.0			4.0	e setter		4.0	4.0		4.0	
Vehicle Extension (s)	3.0	3.0			3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)	122	493			404			1189	1000		1465	
v/s Ratio Prot		0.06		1997 - SA - C 1979	<ul> <li>X 3 247 1,3383</li> </ul>		10.000000	c0.31	1979 - 1977, 1977 - 1977, 1979 - 1977, 1977 - 1977, 1977		- an and a first strategy	
v/s Ratio Perm	0.16				c0.24				0.03		0.30	
v/c Ratio	0.62	0.23			0.90		· · · · · · · · · · · · · · · · · · ·	0.49	0.04		0.47	
Uniform Delay, d1	25.1	22.3			27.5			7.6	5.4		7.5	
Progression Factor	1.00	1.00			1.00			1.00	1.00		1.00	
Incremental Delay, d2	9.5	0.2			21.6			1.5	0.1	관광 문	1.1	
Delay (s)	34.6	22.6			49.1			9.1	5.5		8.6	
Level of Service	C	C			D			Α	A		A	
Approach Delay (s)		27.2		·····	49.1			8.7			8.6	
Approach LOS		C			D			A			Α	
Intersection Summary	2.2.N							•				
HCM Average Control Delay			21.0	Н	CM Leve	l of Service			С			
HCM Volume to Capacity ratio		NGC 127 - 928.47	0.61		. erektiőt		e ga nijeri.	n an an Arabi	99 - 19 (MRF) 			
Actuated Cycle Length (s)			77.7	S	um of los	t time (s)			8.0			
Intersection Capacity Utilization	1		94.6%			of Service			F			
Analysis Period (min)	٠ ب		15						лаў.			
c Critical Lane Group												

		Ŧ	1	•	Ŧ	
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	¥		:	र्स	Ť	7
Volume (vph)	158	159	228	36	69	281
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0	0	75			75
Storage Lanes	1	0	0			1
Taper Length (ft)	25	25	25	걸렸으며	한 같 않	<b>25</b>
Link Speed (mph)	30			30	30	
Link Distance (ft)	471			196	172	전화 이 없는 것을 알려왔는 것을 이 없는 것이 있다. 않는
Travel Time (s)	10.7			4.5	3.9	
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95
Heavy Vehicles (%)	3%	3%	0%	3%	0%	1%
Shared Lane Traffic (%)						
Lane Group Flow (vph)	333	0	0	278	73	296
Sign Control	Stop			Free	Free	
Intersection Summary					1945	그는 물을 손을 손을 가 들었다.

# メ ネ ネ - † ↓ イ

Area Type: Other Control Type: Unsignalized

Intersection Capacity Utilization 46.4% ICU Level of Service A Analysis Period (min) 15

### HCM Unsignalized Intersection Capacity Analysis 2: North St. & Market St.

10/15/2008

	۶	$\mathbf{F}$	1	· †	Ļ	4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR				·	1
Lane Configurations	Y				1	7					
Volume (veh/h)	158	159	228	36	69	281		19 A B			
Sign Control	Stop			Free	Free						
Grade	0%			0%	0%						
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95					
Hourly flow rate (vph)	166	167	240	38	73	296				전 관 것이	
Pedestrians											
Lane Width (ft)											
Walking Speed (ft/s)											
Percent Blockage											
Right turn flare (veh)											
Median type				None	None						
Median storage veh)											
Upstream signal (ft)						\$s - 20				94.6 M	
pX, platoon unblocked											
vC, conflicting volume	591	73	368								
vC1, stage 1 conf vol											
vC2, stage 2 conf vol											
vCu, unblocked vol	591	73	368								
tC, single (s)	6.4	6.2	4.1								
tC, 2 stage (s)											
tF (s)	3.5	3.3	2.2								
p0 queue free %	56	83	80								
cM capacity (veh/h)	375	987	1201								
Direction, Lane #	EB 1	NB 1	SB 1	SB 2							
Volume Total	334	278	73	296							
Volume Left	166	240	0	0							
Volume Right	167	0	0	296							
cSH	544	1201	1700	1700							
Volume to Capacity	0.61	0.20	0.04	0.17						철도 공항	
Queue Length 95th (ft)	103	19	0	0							
Control Delay (s)	21.6	7.8	0.0	0.0							
Lane LOS	С	А									
Approach Delay (s) Approach LOS	21.6 C	7.8	0.0								
Intersection Summary				1							
Average Delay			9.6								
Intersection Capacity Utiliza	tion		46.4%			of Service	San Ang A	wale in	Δ		
Analysis Period (min)	UUN		40.4 %	R.	10 LEVEL		and the		A		
Analysis Feriou (min)			GI								

		¥.	1			
Lane Group	SEL	SER	NEL	NET	SWT	SWR
Lane Configurations	- ¥		_	1	1	
Volume (vph)	1	2	0	136	304	Ó
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Link Speed (mph)	30			30	30	
Link Distance (ft)	206			239	155	
Travel Time (s)	4.7			5.4	3.5	
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85
Shared Lane Traffic (%)			8 K - K - K			
Lane Group Flow (vph)	3	0	0	160	358	0
Sign Control	Stop			Free	Free	
Intersection Summary	i.		1		5	
Area Type: O	ther					

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Control Type: Unsignalized
Intersection Capacity Utilization 26.0%
ICU Level of Service A

Analysis Period (min) 15

10/15/2008

10/15/2008

	¥	2	Ŋ	*	¥	*	
Movement	SEL	SER	NEL	NET	SWT	SWR	
Lane Configurations	Y			↑	1		
Volume (veh/h)	8 <b>1</b>	2	0	136	304	0	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85	en un elevante de la compositionen en autoritaria de la composition a contra sufficiencia de terror de trategic
Hourly flow rate (vph)	1	2	0	160	358	0	
Pedestrians Lane Width (ft)	1.984		anti uzza			ti e Stor - Sola	
Walking Speed (ft/s)	9889-67 1		- 19 (A) 	9 - 1993 - 11 1		이 아파라 가락했는	
Percent Blockage	1999 - S						
Right turn flare (veh)	1998) <del>-</del> 616			(1) = 1.5% = 1.		new kresse Garagen	n un de la companya br>La companya de la comp
Median type				None	None		
Median storage veh)			Sec. 24. Constants				алы аларын ал
Upstream signal (ft)							
pX, platoon unblocked	- 40	0-0		9 - 1 - MARCANO -			
vC, conflicting volume	518	358	358		1999		
vC1, stage 1 conf vol vC2, stage 2 conf vol	\$ <del>.</del>	1. 19. j Parista		et bariet		2683 (2003) 1983	
vCu, unblocked vol	518	358	358	9 <b></b>	11 <u>(</u> 201 3)		
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)	17 - 37 ⁶ 2537-		1885 - 1 TADA	19 - 19 - 19 - 19 19 19 19 19 19 19 19 19 19 19 19 19		anne solite, galler	ne o possie o so nazione despensione de service en constructione de service de la service de la service de la s
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	100	100				
cM capacity (veh/h)	522	691	1212				
Direction, Lane #	SE 1	NE 1	SW 1				
Volume Total	4	160	358				
Volume Left	1	0	0	N 1 1.883 N 1		andar an	an an anna ann anna ann ann ann ann ann
Volume Right	2	0	0				
cSH Volume to Capacity	624 0.01	1700 0.09	1700 0.21		alata ta <b>ta</b>		
Queue Length 95th (ft)	0.01	0.09	0.21		1992) († 1992) 1		
Control Delay (s)	10.8	0.0	0.0				
Lane LOS	B		1.433 - <b>∀•∀</b> 38	a fortager i			n - An ann - Airte Chine, an
Approach Delay (s)	10.8	0.0	0.0			Ngan Kasil	
Approach LOS	В	and a second				(III · · ·	under den in skuluten en den sjon en en en stille strukter in Nuder om en politiker en en en en en en en en en En en
Intersection Summary							
Average Delay			0.1				and the second
Intersection Capacity Utilization			26.0%	(* 1. je	CU Level	of Service	
Analysis Period (min)			15				

### North Street Condos : PM Build Condition Timing Plan: Existing

### Lanes, Volumes, Timings 14: North St. & Bates St.

ኘ	r*	X	$\mathbf{Y}$	<b>₽</b> `	×

Lane Group	NBL	NBR	SET	SER	NWL	NWT	
Lane Configurations	Y		4			र्भ	
Volume (vph)	52	30	117	212	41	49	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Link Speed (mph)	30		30			30	
Link Distance (ft)	403		673			909	
Travel Time (s)	9.2		15.3	1 옷 옷 좀 한	경험적의	20.7	
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86	
Heavy Vehicles (%)	10%	0%	2%	2%	0%	6%	
Shared Lane Traffic (%)	and ready it was a ser-	- investories			no tap su - p		
Lane Group Flow (vph)	95	0	383	0	0	105	
Sign Control	Stop		Stop			Stop	
Intersection Summary							
Area Type:	Other		en l'ante anna la la	1762 - 673 - J		2051 (8 <b>6</b> 396), (4),	

Control Type: Unsignalized Intersection Capacity Utilization 38.7% ICU Level of Service A

Analysis Period (min) 15

	۲	۴	X	$\rightarrow$	<b>₽</b> ``	×	
Movement	NBL	NBR	SET	SER	NWL	NWT	
Lane Configurations	- Y		4	_		र्भ	
Sign Control	Stop		Stop			Stop	
Volume (vph)	52	30	117	212	41	49	and the second
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86	
Hourly flow rate (vph)	60	35	136	247	48	57	
Direction, Lane #	NB 1	SE 1	NW 1				
Volume Total (vph)	95	383	105				
Volume Left (vph)	0	136	48				
Volume Right (vph)	35	0	57				
Hadj (s)	-0.11	0.11	-0.18				
Departure Headway (s)	4.5	4.4	4.8	ann a' mhaire caille		THE REAL REPORTS	n sa manana sa isana manana manana ka asana ka ang kana kana ka sa manana ka matana masakana manana ka sa sa s
Degree Utilization, x	0.12	0.47	0.14				
Capacity (veh/h)	767	799	683	sonounes, un cristin	- 0.000214- 1-00451	20.1000000	
Control Delay (s)	8.1	11.1	8.6				
Approach Delay (s)	8.1	11.1	8.6	• scatter 11 100*.			- o recención de la constante de sector de sector de la constante de la constante de sector de la constante de
Approach LOS	А	В	A				
Intersection Summary							
Delay			10.2				
HCM Level of Service			В				
Intersection Capacity Utilization	n		38.7%	IC	U Level c	of Service	e
Analysis Period (min)			15	an en an			w to zama na na wakata na na na na na na na wakata na wakata na wakata na kata kata na na kata na na mana na na
	이 공격하						

# 4 2 7 × × ×

Lane Group	SEL	SER	NEL	NET	SWT	SWR	, in the second s	1	
Lane Configurations	Ъ.			र्स	4				
Volume (vph)	0	2	4	136	298	8			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
Link Speed (mph)	30			30	30				
Link Distance (ft)	158			479	239				
Travel Time (s)	3.6			10.9	5.4				
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85			
Shared Lane Traffic (%)								1988 I I	
Lane Group Flow (vph)	2	0	0	165	360	0			
Sign Control	Stop			Free	Free				
Intersection Summary		-							
Area Type:	Other								

Control Type: Unsignalized

Intersection Capacity Utilization 26.2% ICU Level of Service A Analysis Period (min) 15

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10/15/2008

# * 2 Y X X W

Movement		SER	NEL	NET	SWT	-22	SWR	. 499	A74 (4)				5. 1		
ane Configurations	Y			र्भ	ţ,	•									
/olume (veh/h)	0	2	4	136	298		8								
Sign Control	Stop	- 1881 -		Free	Free		5.5. J. 1.5.								
Grade	0%		in starter i se	0%	0%		환장님과								
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85		0.85	· National II.				5.490 · S			
Hourly flow rate (vph)	0	2	5	160	351		9		신 이상	8 K K				1980 - I	
[⊃] edestrians ₋ane Width (ft)	la stèrre			1.4532	6.83. J.					Set i	Ang a		å		
Valking Speed (ft/s)	일을 가지 않는									-28-2					
Percent Blockage	i si		2478 A.S.					- 4690	E Noão		1. 2.36A	. 993	ga et	8410 X	
Right turn flare (veh)	relation - Fest (M	0.0000.04000	anga tangga	1999 (1999) 1999 (1999)	i d'Anis			) (Q244)	8 - 1999) S	1 - 189 AP	6 - 1738 AU (		985 - 538 -		
Viedian type				None	None	•									
vledian storage veh)		1171-0-9-14 - MALAU			10 - 10 - 10 - 10 - 10 - 10 - 10 -			senara la			494 - 194				
Jpstream signal (ft)															
oX, platoon unblocked	171 . I PROVIDE 17		NUMBER OF STREET	ant crosses a m	258,32 5,007	. Status					e tit an erar	·· · · · · ·	no tranca	un de la seco	
/C, conflicting volume	525	355	360												
/C1, stage 1 conf vol	98277	en in stationer		987. <i>39</i> 7.9	xia ( - long cos						en - Percedes	an an an an	72	Jerebiet, Dis	09331
/C2, stage 2 conf vol	FOF	055	000		80 3985 1		1-1023		8 - 789 199			신간 것	84 B B	SSR 3	
/Cu, unblocked vol	525 6.4	355 6.2	360 4.1	ar gang	kal setsiki.				S 4539	Statense	14. 19453	52149			
C, single (s) C, 2 stage (s)	0.4	0.2	4.1	- 1.189.38 	e ses				19 - 19383				11.1783		\$\$^`~:-
C, 2 stage (s) F (s)	3.5	3.3	2.2	1935 - 1944 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 - 1945 -	320 V.A		44930.2	92341			390°				1948) 1948)
00 queue free %	100	100	100	(1993) (S.S.S.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C	1983 198 -		9494333		C), 1998 C	981-851-1-3 	2007 - 1-63 1	990.7469. 	( 1898) - Ci	2.886-0	01897
M capacity (veh/h)	515	693	1210				- <u>1</u>						6 33		7 8 4
Direction, Lane #	SE 1	NE 1	SW 1												
/olume Total	2	165	360												<u>9000000</u>
/olume Left	0	5	0		ala i Siñiya	u numer,	*	e - 1 1 10	2001 - 10001				64 X 643	юнна, на 	
/olume Right	2	0	9		1933)										
:SH	693	1210	1700												
/olume to Capacity	0.00	0.00	0.21												
Queue Length 95th (ft)	0	0	0		1.000		0.030-113	14.5×					< 1 50.001.		
Control Delay (s)	10.2	0.3	0.0												
₋ane LOS	В	A		9 E - 2068						SS 1.0			ja teks	la thirtiga	
Approach Delay (s) Approach LOS	10.2 B	0.3	0.0		4. 1822) 	5. 98									97. 197
							<b>.</b>				1.1				(A) Pé
ntersection Summary			0.4			÷ •									
Average Delay	Hon		0.1 26.2%		CUI	1 al c	ondos			「新たい」	A				10
ntersection Capacity Utiliza Analysis Period (min)	uun		20.2% 15		CU Leve	1015	el vice				A				
maiyos renou (mm)			10												

	.]	l	+	Ð	_	¥
Lane Group	NBL	NBT	SBT	SBR	SEL	SER
Lane Configurations		÷.	4Î		¥۲	-
Volume (vph)	4	130	286	9	3	3 4
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	
Link Speed (mph)		30	30	n an	30	
Link Distance (ft)		92	212		622	
Travel Time (s)		2.1	4.8		14.1	
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	158	347	0	9	
Sign Control		Free	Free		Stop	)
Intersection Summary						
	ther			<u>.</u>		

#### **1** I ∔ 1 ×

Control Type: Unsignalized Intersection Capacity Utilization 25.6% ICU Level of Service A Analysis Period (min) 15

10/15/2008

Movement         NBL         NBT         SBT         SBR         SEL         SER           Lane Configurations         4         12         286         9         3         4           Sign Control         Free         Free         Stop         3         4           Sign Control         Free         Free         Stop         0%         0%           Grade         0%         0%         0%         0%         0%           Peak Hour Factor         0.85         0.85         0.85         0.85         0.85           Hourly flow rate (vph)         5         153         336         11         4         5           Pedestrians         Lane Width (ft)         Walking Speed (ft/s)         Percent Blockage         8         8         8           Right turn flare (veh)         Median storage veh)         Upstream signal (ft)         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9         9			$\mathbf{F}$		N	Ļ	†	ኘ	
Volume (veh/h)       4       130       286       9       3       4         Sign Control       Free       Free       Stop       0%       0%         Grade       0%       0%       0%       0%       0%         Peak Hour Factor       0.85       0.85       0.85       0.85       0.85       0.85         Hourly flow rate (vph)       5       153       336       11       4       5         Pedestrians       Lane Width (ft)       Walking Speed (ft/s)       Percent Blockage       8       8         Right turn flare (veh)       Median type       None       None       None       8         Median storage veh)       Upstream signal (ft)       PX platoon unblocked       347       504       342         vC1, stage 1 conf vol       vC2, stage (s)       524       342       342         tC, single (s)       4.1       6.4       6.2       6.2       6.2         C2, stage (s)       1223       529       705       504       529       705         Direction, Lane #       NB1       SB1       SE1       529       705       524       529       705       524       529       705       524       529 <td< th=""><th></th><th></th><th>SER</th><th>SEL</th><th>SBR</th><th>SBT</th><th>NBT -</th><th>NBL</th><th>Movement</th></td<>			SER	SEL	SBR	SBT	NBT -	NBL	Movement
Sign Control       Free       Free       Stop         Grade       0%       0%       0%         Peak Hour Factor       0.85       0.85       0.85       0.85         Pedestrians       153       336       11       4       5         Pedestrians       Eane Width (ft)       Walking Speed (ft/s)       Percent Blockage       Free       Sign Control         Right turn flare (veh)       Median storage veh)       Upstream signal (ft)       Free       504       342         VC1, stage 1 conf vol       347       504       342       54       54         VC2, stage 2 conf vol       VC2, stage 2 conf vol       VC2, stage 2 conf vol       529       705         VC2, unblocked vol       347       504       342       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Usume Total       158       347       8       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       70									
Grade         0%         0%         0%           Peak Hour Factor         0.85         0.85         0.85         0.85         0.85           Hourly flow rate (vph)         5         153         336         11         4         5           Pedestrians         Lane Width (ft)         Walking Speed (ft/s)         Percent Blockage         Right turn flare (veh)           Median type         None         None         None         None           Median storage veh)         Upstream signal (ft)         7         504         342           VC1, stage 1 conf vol         VC2, stage 2 conf vol         -         -         -           VC2, stage 2 conf vol         -         -         -         -         -           VC2, stage 1 conf vol         VC2, stage 2 conf vol         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -			4		9	and the second second	10112	4	
Peak Hour Factor       0.85       0.85       0.85       0.85       0.85         Hourly flow rate (vph)       5       153       336       11       4       5         Pedestrians       Lane Width (ft)       Walking Speed (ft/s)       Percent Blockage       None       None         Walking Speed (ft/s)       Percent Blockage       None       None       None       None         Median storage veh)       Upstream signal (ft)       pX, platoon unblocked       VG, conflicting volume       347       504       342         VC1, stage 1 conf vol       VC2, stage 2 conf vol       VC4, unblocked vol       347       504       342         VC2, stage 2 conf vol       VC4, unblocked vol       347       6.4       6.2       6.2         VC3, stage (s)       Ef (s)       2.2       3.5       3.3       00       99       99         VC4 unblocked vol       347       8       529       705       529       705         Direction, Lane #       NB1       SE1       SE1       529       705       529       705         Direction, Lane #       NB1       SE1       SE1       529       705       524       529       705         Outume Total       158									
Hourly flow rate (vph)       5       153       336       11       4       5         Pedestrians       Lane Width (ft)       Walking Speed (ft/s)       Percent Blockage       Right turn flare (veh)         Median storage veh)       Upstream signal (ft)       None       None       None         Median storage veh)       Upstream signal (ft)       None       347       504       342         VC1, stage 1 conf vol       VC2, stage 1 conf vol         VC2, stage 1 conf vol       VC2, stage 1 conf vol       VC2, stage 1 conf vol       VC2, stage 1 conf vol       VC2, stage 1 conf vol         VC1, utblocked vol       347       504       342       S42         VC2, stage (s)       1       6.4       6.2       S42         VC3, stage 1 conf vol       VC2       3.5       3.3         00 queue free %       100       99       99         cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB1       SB1       SE 1         Volume Left       5       0       4         Volume Right       0       1       5         C34       0.3       0.0 <td< td=""><td></td><td></td><td>한 영혼 등 2</td><td></td><td></td><td></td><td></td><td></td><td></td></td<>			한 영혼 등 2						
Pedestrians         Lane Width (ft)         Walking Speed (ft/s)         Percent Blockage         Right turn flare (veh)         Median storage veh)         Upstream signal (ft)         Dx, platoon unblocked         vC1, stage 1 conf vol         vC2, stage 2 conf vol         vC2, stage 1 conf vol         vC2, stage 1 conf vol         vC2, stage 1 conf vol         vC2, stage 2 conf vol         vC4, unblocked vol         VG2, stage 2 conf vol         vC4, unblocked vol         VG2, stage 1 conf vol         vG2, stage 2 conf vol         vG1, unblocked vol         VG1, unblocked vol         VG1, unblocked vol         VG2, stage (s)         IF (s)       2.2         Stage 1       52.9         VG2       3.5         VG1me free %       100         Volume Total       158         Volume Total       158         Volume Right       0         Volume Right       0         Volume Right       0         U23       1700         Queue Length 95th (ft)       0         U23       0.0         Queue Length 95	an tao ing kara Kina tao kweli	- An I - 1944 - Marke Walter - 1955 - Suid-A - 1945 - Mark							
Lane Width (ft) Walking Speed (ft/s) Percent Blockage Right turn flare (veh) Median storage veh) Upstream signal (ft) pX, platoon unblocked vG, conflicting volume 347 VC1, stage 1 conf vol vC2, stage 2 conf vol VC2, unblocked vol 347 C, single (s) 14.1 C, single (s) 4.1 C, single (s) 4.1 C, single (s) 14.1 C, single (s) 14.1 C, single (s) 14.1 C, single (s) 14.1 C, single (s) 14.1 C, single (s) 14.1 C, single (s) 15 Sigle (s) 100 100 1223 100 100 1223 100 100 11 158 147 8 Volume Total 158 347 8 Volume Total 158 347 8 Volume Total 158 347 8 Volume Total 158 347 8 Volume Right 0 11 5 15 16 17 10 10 15 15 17 10 10 10 10 10 10 10 10 10 10		e de la compañía de l	ં 5	4	11	336	153	5	
Walking Speed (ft/s)         Percent Blockage         Right turn flare (veh)         Median storage veh)         Upstream signal (ft)         pX, platoon unblocked         vC, conflicting volume       347         vC1, stage 1 conf vol         vC2, stage 2 conf vol         vC2, stage 1 conf vol         vC2, stage 1 conf vol         vC2, stage 2 conf vol         vC2, stage 1 conf vol         vC2, stage 1 conf vol         vC2, stage 2 conf vol         vC2, stage 3         Ff (s)       2.2         100       99         of queue free %       100         102       529         p0 queue free %       100         1223       529         Direction, Lane #       NB 1       SE 1         Volume Total       158       347         Volume Right       0       11       5         cSH       1223       700       617         Volume Right       0       1       5         cSH       1223       1700       617         Volume to Capacity       0.0       0.0       1         CSH       123       10.9       1 <td>a</td> <td>n an Near Wierder an 1984 an the track with a statistical statistical statistical statistical statistical statis</td> <td>0 514 J</td> <td>Berlan oc</td> <td>ia - Ma</td> <td></td> <td>uddelera - azel</td> <td>eller issen fo</td> <td></td>	a	n an Near Wierder an 1984 an the track with a statistical statistical statistical statistical statistical statis	0 514 J	Berlan oc	ia - Ma		uddelera - azel	eller issen fo	
Percent Blockage       None       None         Right turn flare (veh)       Mone       None         Median storage veh)       Upstream signal (ft)       Dystream signal (ft)         pX, platoon unblocked       347       504       342         vC1, stage 1 conf vol	같은 강경철이 집중했어요.								
Right turn flare (veh)       None       None       None         Median storage veh)       Upstream signal (ft)       px, platoon unblocked       px, platoon unblocked         VC, conflicting volume       347       504       342         VC1, stage 1 conf vol       VC2, stage 2 conf vol       VC2, unblocked vol       347         VC2, unblocked vol       347       504       342         VC3, stage 2 conf vol       VC2, unblocked vol       347       504       342         VC3, stage 2 conf vol       VC2, unblocked vol       347       504       342         VC3, stage 2 conf vol       VC2, stage (s)       F       6.4       6.2       6.4       6.2         F (s)       2.2       3.5       3.3       00       queu free %       100       99       99       99         cM capacity (veh/h)       1223       529       705       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505       505	98	a na katalan ka	S. Jan	ana ang ang ang ang ang ang ang ang ang	201 - S.S.	1989) - 198			
Median type         None         None           Median storage veh)         Upstream signal (ft)            pX, platoon unblocked         VG, conflicting volume         347         504         342           vC1, stage 1 conf vol         VC2, stage 2 conf vol          State         State <t< td=""><td>Card Mark Charles</td><td></td><td>9 - 1938 - C</td><td></td><td>22) - 1480 -</td><td></td><td>1993 - Core</td><td></td><td></td></t<>	Card Mark Charles		9 - 1938 - C		22) - 1480 -		1993 - Core		
Median storage veh)       Upstream signal (ft)         pX, platoon unblocked       347       504       342         vC1, stage 1 conf vol       vC2, stage 2 conf vol       vC2, stage 2 conf vol       vC2, stage 2 conf vol         vC2, stage 2 conf vol       vC4, unblocked vol       347       504       342         tC, single (s)       4.1       6.4       6.2       6.2         tC, stage (s)       1       6.4       6.2         tF (s)       2.2       3.5       3.3         p0 queue free %       100       99       99         cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SB 1       SE 1				<u>C SARC</u>	1980 - 1989	Nono	None		
Upstream signal (ft)       pX, platoon unblocked         vC, conflicting volume       347       504       342         vC1, stage 1 conf vol       vC2, stage 2 conf vol       vC2, stage 2 conf vol         vC2, unblocked vol       347       504       342         VC2, stage 2 conf vol       vC1, unblocked vol       347       6.4       6.2         VC, single (s)       4.1       6.4       6.2       6.2         tC, 2 stage (s)       100       99       99         tF (s)       2.2       3.5       3.3         p0 queue free %       100       99       99         cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SB 1       SE 1         Volume Total       158       347       8         Volume Left       5       0       4         Volume to Capacity       0.00       0.20       0.01         Queue Length 95th (ft)       0       1       5         cSH       1223       1700       617         Volume to Capacity       0.00       0.20       0.01         Queue Length 95th (ft)       0       1       5         control Delay (s)			neer Selfer	9 . S. 28 Y.	1998 - 1999. 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999	NONE	NOUC	80.000 (1986) 1997	
pX, platoon unblocked     347     504     342       vC1, stage 1 conf vol     vC2, stage 2 conf vol     vC2, stage 2 conf vol       vCu, unblocked vol     347     504     342       vCu, unblocked vol     347     504     342       vCu, unblocked vol     347     504     342       vCu, unblocked vol     347     6.4     6.2       tC, stage (s)     4.1     6.4     6.2       tF (s)     2.2     3.5     3.3       p0 queue free %     100     99     99       cM capacity (veh/h)     1223     529     705       Direction, Lane #     NB 1     SB 1     SE 1       Volume Total     158     347     8       Volume Right     0     11     5       cSH     1223     1700     617       Volume to Capacity     0.00     0.20     0.01       Queue Length 95th (ft)     0     0     1       Control Delay (s)     0.3     0.0     10.9       Lane LOS     A     B       Approach LOS     B       Intersection Summary     0.3	11 - R. S.			Kirista		1994 - A.A.		rees - e	
vC, conflicting volume     347     504     342       vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage (s)     347     504     342       tC, single (s)     4.1     6.4     6.2       tC, single (s)     4.1     6.4     6.2       tC, stage (s)     2.2     3.5     3.3       p0 queue free %     100     99     99       cM capacity (veh/h)     1223     529     705       Direction, Lane #     NB1     SB1     SE 1       Volume Total     158     347     8       Volume Left     5     0     4       Volume Right     0     11     5       CSH     1223     1700     617       Volume to Capacity     0.00     0.20     0.01       Queue Length 95th (ft)     0     0     1       Control Delay (s)     0.3     0.0     10.9       Lane LOS     A     B       Approach Delay (s)     0.3     0.0       Approach LOS     B       Intersection Summary     0.3			10.86949-11	10.4890 - 1499 -	84 10 <b>288</b> 9	45096863 (J-148		1.0699001.2 - 903	
vC1, stage 1 conf vol       vC2, stage 2 conf vol         vCu, unblocked vol       347       504       342         tC, single (s)       4.1       6.4       6.2         tC, 2 stage (s)       100       99       99         tF (s)       2.2       3.5       3.3         p0 queue free %       100       99       99         cK capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SE 1       SE 1         Volume Total       158       347       8         Volume Left       5       0       4         Volume Right       0       11       5         cSH       1223       1700       617         Volume to Capacity       0.00       0.20       0.01         Queue Length 95th (ft)       0       0       1         Control Delay (s)       0.3       0.0       10.9         Lane LOS       A       B       Approach LOS       B         Intersection Summary       0.3       0.3       0.3	1999년 1998년 1999년 1997년 19 1997년 1997년 199 1997년 1997년 199		342	504				347	
vC2, stage 2 conf vol       347       504       342         vCu, unblocked vol       347       6.4       6.2         tC, single (s)       4.1       6.4       6.2         tC, 2 stage (s)       3.5       3.3         p0 queue free %       100       99       99         p0 queue free %       100       99       99         cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SB 1       SE 1	1997 by 1 - Kinger - Den Debende	n na theachadh a sear a' an an an ann an an ann an ann an ann an a	a i statet.	0 - 123867 - Th	2010 - 115 OB6710		n ang kalamin ang m	- 2 51 G1 8. 58575-	
vCu, unblocked vol     347     504     342       tC, single (s)     4.1     6.4     6.2       tC, 2 stage (s)     100     99     99       tF (s)     2.2     3.5     3.3       p0 queue free %     100     99     99       cK capacity (veh/h)     1223     529     705       Direction, Lane #     NB 1     SB 1     SE 1       Volume Total     158     347     8       Volume Left     5     0     4       Volume Right     0     11     5       cSH     1223     1700     617       Volume to Capacity     0.00     0.20     0.01       Queue Length 95th (ft)     0     0     1       Control Delay (s)     0.3     0.0     10.9       Lane LOS     A     B       Approach LOS     B     B       Intersection Summary     0.3     0.3									
tC, 2 stage (s)       2.2       3.5       3.3         p0 queue free %       100       99       99         cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SB 1       SE 1       100         Volume Total       158       347       8       100       100         Volume Total       158       347       8       100       100       100         Volume Eoft       5       0       4       100       11       5       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100	Constant and a constant of the	ander in der der er sterner im der eine gehenen der Gehandens im Ann der	342	504	TRAVIC I CONTRA			347	
IF (s)       2.2       3.5       3.3         p0 queue free %       100       99       99         cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Direction, Lane #       NB 1       SB 1       SE 1       529       705         Volume Total       158       347       8       50       4       50       4         Volume Right       0       11       5       55       50       0.01       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100 <t< td=""><td></td><td></td><td>6.2</td><td>6.4</td><td></td><td></td><td></td><td>4.1</td><td>tC, single (s)</td></t<>			6.2	6.4				4.1	tC, single (s)
p0 queue free %       100       99       99       99         cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SB 1       SE 1         Volume Total       158       347       8         Volume Left       5       0       4         Volume Right       0       11       5         cSH       1223       1700       617         Volume to Capacity       0.00       0.20       0.01         Queue Length 95th (ft)       0       0       1         Control Delay (s)       0.3       0.0       10.9         Lane LOS       A       B         Approach Delay (s)       0.3       0.0       10.9         Approach LOS       B       B         Intersection Summary       0.3       0.3									tC, 2 stage (s)
cM capacity (veh/h)       1223       529       705         Direction, Lane #       NB 1       SB 1       SE 1         Volume Total       158       347       8         Volume Left       5       0       4         Volume Right       0       11       5         cSH       1223       1700       617         Volume to Capacity       0.00       0.20       0.01         Queue Length 95th (ft)       0       0       1         Control Delay (s)       0.3       0.0       10.9         Lane LOS       A       B         Approach Delay (s)       0.3       0.0       10.9         Approach LOS       B       B         Intersection Summary       0.3       0.3									
Direction, Lane #         NB 1         SB 1         SE 1           Volume Total         158         347         8           Volume Left         5         0         4           Volume Right         0         11         5           cSH         1223         1700         617           Volume to Capacity         0.00         0.20         0.01           Queue Length 95th (ft)         0         0         1           Control Delay (s)         0.3         0.0         10.9           Lane LOS         A         B           Approach Delay (s)         0.3         0.0           Intersection Summary         0.3	name								
Volume Total         158         347         8           Volume Left         5         0         4           Volume Right         0         11         5           cSH         1223         1700         617           Volume to Capacity         0.00         0.20         0.01           Queue Length 95th (ft)         0         0         1           Control Delay (s)         0.3         0.0         10.9           Lane LOS         A         B           Approach Delay (s)         0.3         0.0         10.9           Approach LOS         B         B           Intersection Summary         0.3         0.3			705	529				1223	cM capacity (veh/h)
Volume Left         5         0         4           Volume Right         0         11         5           cSH         1223         1700         617           Volume to Capacity         0.00         0.20         0.01           Queue Length 95th (ft)         0         0         1           Control Delay (s)         0.3         0.0         10.9           Lane LOS         A         B           Approach Delay (s)         0.3         0.0         10.9           Approach LOS         B         B           Intersection Summary         0.3         0.3						SE 1			
Volume Right         0         11         5           cSH         1223         1700         617           Volume to Capacity         0.00         0.20         0.01           Queue Length 95th (ft)         0         0         1           Control Delay (s)         0.3         0.0         10.9           Lane LOS         A         B           Approach Delay (s)         0.3         0.0         10.9           Approach LOS         B         B           Intersection Summary         0.3         0.3						8	347	158	Reacond where involution states is a market of the
cSH         1223         1700         617           Volume to Capacity         0.00         0.20         0.01           Queue Length 95th (ft)         0         1         1           Control Delay (s)         0.3         0.0         10.9           Lane LOS         A         B           Approach Delay (s)         0.3         0.0         10.9           Intersection Summary         B         1           Average Delay         0.3         0.3						4			In the second
Volume to Capacity         0.00         0.20         0.01           Queue Length 95th (ft)         0         0         1           Control Delay (s)         0.3         0.0         10.9           Lane LOS         A         B           Approach Delay (s)         0.3         0.0         10.9           Intersection Summary         B         10.9           Average Delay         0.3         0.3				영화망		<ul> <li>ARE 187 - 2013</li> </ul>		200, 0000000 - C	
Queue Length 95th (ft)         0         0         1           Control Delay (s)         0.3         0.0         10.9           Lane LOS         A         B           Approach Delay (s)         0.3         0.0         10.9           Approach LOS         B         B           Intersection Summary         0.3         0.3	a state state and a	na stan stan	et satta		7 t. ma22-a4				
Control Delay (s)     0.3     0.0     10.9       Lane LOS     A     B       Approach Delay (s)     0.3     0.0     10.9       Approach LOS     B       Intersection Summary     0.3       Average Delay     0.3	2 - <b>2</b> 5 - 136 - 3 <b>8</b>	아 없는데 이것은 같은 것은 것은 것이다.	이 생활할			0.01	and the state of the second		
Lane LOS A B Approach Delay (s) 0.3 0.0 10.9 Approach LOS B Intersection Summary Average Delay 0.3	alah seri seri seri seri seri seri seri seri	a tanàna amin'ny faritr'i Andre North	ov 18498-	within and	an statist	1			
Approach Delay (s)     0.3     0.0     10.9       Approach LOS     B       Intersection Summary     0.3					8 88 s	a that is a second a second	0.0		
Approach LOS B Intersection Summary Average Delay 0.3	atta l'Atta Mila de A	an ing an			- 1990 - 1990 M		0.0		
Average Delay 0.3	· 철학의 · 철도 · 철도의 · 역				1999 - 1993		0.0	0.3	
Interception Canacity Utilization 25.6% ICLU avail of Service									
	중 : 21 : 3일 - 22	である類には行為で認う意思。	of Servic	U Leve	10	25.6%		ation	Intersection Capacity Utilization
Analysis Period (min) 15						15			Analysis Period (min)

### Lanes, Volumes, Timings 1: North St. & King St.

	٭		$\mathbf{F}$	4	-	×.	*	1	1	1	Ļ	~
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR -	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4						1	7			
Volume (vph)	71	.97	17	103	0	403	0	551	60	158	491	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0		0	0		25	0		200	0		0
Storage Lanes	1		0	0		0	0		1	0		0
Taper Length (ft)	25		25	25		25	25		25	25		25
Right Turn on Red			Yes			Yes			Yes		and the second second	Yes
Link Speed (mph)		30			30			30		생활님	30	
Link Distance (ft)		143			471		. 5." 5	282			275	
Travel Time (s)		3.3			10.7			6.4			6.3	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Heavy Vehicles (%)	1%	0%	0%	1%	0%	0%	0%	1%	2%	1%	1%	0%
Shared Lane Traffic (%)	1975 SURVA - 1977 A		2000 - 11.0794 -		100000000000000000000000000000000000000		a anna a se taca a		na na natari a siti tina		100 P.S. 1988	
Lane Group Flow (vph)	76	121	0	0	539	0	0	586	64	0	690	0
Turn Type	Perm	"tuv-n, 90"	1191 H HQ 1, 1799 Y	Perm	Dari Cibili Mari	112111234515.000	er - en 200300 e	- WILLING - 1943000	Perm	Perm	219 A 4 9 20 30	
Protected Phases		4			8			2			6	51232
Permitted Phases	4	. '- 1996 - 1998)'	e in New Yorks Ca	8	1.12 March 1 7.49		977. (* 1683 <u>8</u> 777)	61969 - 1716 <del>17</del> 69	2	6	ante de serre	
Detector Phase	4	4		8	8	17 C. M. J.	i de la compositación de la com	2	2	6	6	
Switch Phase		- 1 - CH - 1 - 3 H -	가지 않는 것은 것 같은 것		ng kalaban 📑 P		967 DV - 20 89.88	- 19 V - <b>1</b> 66	97 - 197 A <del>R</del> A	. NEW 7.2	8480° (Mr. 19 <b>7</b> 7)	, Shiri i Kasa
Minimum Initial (s)	4.0	4.0	1622 S.S.	4,0	4.0			4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0	ACTO BOXERA (C. A	20.0	20.0	- 0.0880 - 78	S. 1991981 (.	20.0	20.0	20.0	20.0	1.19930-109
Total Split (s)	27.0	27.0	0.0	27.0	27.0	0.0	0.0	53.0	53.0	53.0	53.0	0.0
Total Split (%)	33.8%	33.8%	0.0%	33.8%	33.8%	0.0%	0.0%	66.3%	66.3%	66.3%	66.3%	0.0%
Yellow Time (s)	3.5	3.5		3.5	3.5		0.070	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	- SAN 17 (1798)	0.5	0.5	1.988288 - 9893	- 1997 NGC - 1	0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
Lead/Lag	ier dat fil											
Lead-Lag Optimize?	an an Station ( ) a	4884 J. 1968	4980 N. 1997	h tinen tir	86°. : 428°. 1		- 1998 (1999) 1999 - State State (1997)	8001 - ARM ADU		30/2011 - 1477-147 1	12.11(2), 12(1.12	12.2814.015
Recall Mode	None	None	847 - SA	None	None	(187) (SA)		Max	Max	Max	Max	
Act Effct Green (s)	20.4	20.4	(\$4.57 NOA)	110110	20.4		1995 - 1988 Ali	49.1	49.1	. HIVEN	49.1	
Actuated g/C Ratio	0.26	0.26			0.26	Vala (2261)		0.63	0.63		0.63	
v/c Ratio	0.63	0.24	2010 81,919		0.93	en de est	nga siya naga	0.49	0.06	ness - Norra J	0.00	
Control Delay	50.5	21.4	een oo saad Namataan waxaa		39.4		Maria	9.9	2.0	ser del	9.2	
Queue Delay	0.0	0.0	49.28-S. 2 3	88 ret re 39 8	0.0			0.0	0.0	396080 - 19942 - 19	0.0	yeta dik
Total Delay	50.5	21.4			39.4			9.9	2.0		9.2	
LOS	D	C		a de la composition d	00.4 D	n seld gið		A	A		9.2 A	
Approach Delay		32.6			39.4			9.1			9.2	
Approach LOS	e neeste englige	C			D			A			A	
Queue Length 50th (ft)	32	41			145			148	0		89	
Queue Length 95th (ft)	#94	82			#338			225	13		130	
Internal Link Dist (ft)	<i>π</i> υ <del>1</del>	63			391			202			195	
Turn Bay Length (ft)		00			001			202	200		100	
Base Capacity (vph)	137	560			626			1192	1026		1472	
Starvation Cap Reductn	0	0			020			0	1020		0	
Spillback Cap Reductin	0	0			0			- 0	0		0	
Storage Cap Reductn	0	0			0			0	0		0.	
	0.55	0.22			0.86						-	
Reduced v/c Ratio	0.00	0.22			0.00			0.49	0.06		0.47	

North Street Condos : PM No-Build Condition Timing Plan: Existing Synchro 7 - Report Page 1

## Lanes, Volumes, Timings 1: North St. & King St.

section Summary
i Type:
e Length: 80
ated Cycle Length: 77.5
iral Cycle: 55
trol Type: Actuated-Uncoordinated
imum v/c Ratio: 0.93
section Signal Delay: 19.2
section Capacity Utilization 94.4% ICU Level of Service F
ysis Period (min) 15
95th percentile volume exceeds capacity, queue may be longer.
Dueue shown is maximum after two cycles.

Splits and Phases:	1: North St. & King St.

₽	→ _{ø4}
53 s	27 s
↓ ▼ ∞6	<b>8</b> a
53 s	27 s

### HCM Signalized Intersection Capacity Analysis 1: North St. & King St.

10/15/2008
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	٨		$\mathbf{F}$	4	-	×.	1	†	1	1	Ļ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	4			4			<b>↑</b>	1		- 4 <b>†</b>	
Volume (vph)	71	97	17	103	0	403	0	551	60	158	491	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0			4.0			4.0	4.0		4.0	
Lane Util. Factor	1.00	1.00			1.00			1.00	1.00		0.95	
Frt	1.00	0.98			0,89			1.00	0.85	Sti kaj	1.00	영상 영상
Fit Protected	0.95	1.00			0.99			1.00	1.00		0.99	
Satd. Flow (prot)	1787	1858			1675			1881	1583		3531	
Flt Permitted	0.24	1.00		orana (1. 2004 cm.	0.90			1.00	1.00		0.65	
Satd. Flow (perm)	460	1858			1523			1881	1583		2325	
Peak-hour factor, PHF	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Adj. Flow (vph)	76	103	18	110	0	429	0	586	64	168	522	0
RTOR Reduction (vph)	0	8	0	0	181	0	0	0	23	0	0	0
Lane Group Flow (vph)	76	113	0	0	358	0	Ó	586	41	Ó	690	0
Heavy Vehicles (%)	1%	0%	0%	1%	0%	0%	0%	1%	2%	1%	1%	0%
Turn Type	Perm			Perm					Perm	Perm		
Protected Phases		4			8	1998211-011251388	989 - 22796 ⁻ -	2		Cont. Autors	6	1 .0896.9162-
Permitted Phases	4			8				1982.	2	6		
Actuated Green, G (s)	20.4	20.4	72785970%	. 0478 - 165862	20.4	uces i princi		49.1	49.1		49.1	- 3687695 -
Effective Green, g (s)	20.4	20.4			20.4	8		49.1	49.1		49,1	
Actuated g/C Ratio	0.26	0.26		1987 - 1988 (N. 19	0.26		y y goor awa.	0.63	0.63	n in Spitter en	0.63	
Clearance Time (s)	4.0	4.0			4.0		568 (	4.0	4.0		4.0	1430
Vehicle Extension (s)	3.0	3.0		- 289 S	3.0		1.30 mi - 18-885	3.0	3.0	8099 - Des	3.0	
Lane Grp Cap (vph)	121	489	No. 19 (19)		401			1192	1003		1473	
v/s Ratio Prot	999999 <b>9</b> 49 - 20	0.06	29.20 463.883 	01777 (2026061°-68		a na sina ana ana ana ana ana ana ana ana ana		c0.31	1000			8088- JUP
v/s Ratio Perm	0.17	0.00			c0.23	279 ⁽ 199		00.01	0.03	5.41 ( <b>3</b> 49)	0.30	
v/c Ratio	0.63	0.23	See a see	n dix 1, maille	0.89	9879 - 1989 1	2019-08-08-00-0 1	0.49	0.03		0.47	
Uniform Delay, d1	25.2	22.4			27.5	24 - 43 F L		7.6	5.3	1 <b>2</b> 83	7.4	6384.45
Progression Factor	1.00	1.00	Rish i Usari		1,00			1.00	1.00	3.00 100	1.00	89 826 - C 83
Incremental Delay, d2	9.8	0.2	8. j j j j j j j.	. see .	21.3		174 - AR	1.5	0.1		1.1	85 I B.S
Delay (s)	35.0	22.6	1911 - H. M. S.		48.8		1.5 11 5.388.	9.0	5.4	an san an a	8.5	
Level of Service	C C	<u> </u>	51. KORO		D			Ă	Ă		A.	898 - S. Í.
Approach Delay (s)		27.4	an cointe	254.00053-048	48.8			8.7	e ni 1995 <b>Q</b>	(28023-1523) - (28023-1523)	8.5	
Approach LOS		21.4 C			ч0.0 D			A A	bo fili		A A	
Intersection Summary	<u> </u>								-			
HCM Average Control Delay		83 - 763	20.8	H	CM Level	of Servic	e		C			
HCM Volume to Capacity rat	io		0.61									
Actuated Cycle Length (s)			77.5			time (s)			8.0			
Intersection Capacity Utilizat	ion		94.4%	IC	U Level of	of Service			F			
Analysis Period (min)			15									
c Critical Lane Group												

### Lanes, Volumes, Timings 2: North St. & Market St.

Ideal Flow (vphpl)       1900       1900       1900       1900       1900       1900         Storage Length (ft)       0       0       75       75         Storage Lanes       1       0       0       1         Taper Length (ft)       25       25       25         Link Speed (mph)       30       30       30         Link Distance (ft)       471       196       172         Travel Time (s)       10.7       4.5       3.9         Peak Hour Factor       0.95       0.95       0.95       0.95         Heavy Vehicles (%)       3%       3%       0%       1%         Shared Lane Traffic (%)       2       277       72       293			Ŧ	ł	1	•	•
Volume (vph)       155       159       228       35       68       278         Ideal Flow (vphpl)       1900       1900       1900       1900       1900       1900       1900         Storage Length (ft)       0       0       75       75         Storage Lanes       1       0       0       1         Taper Length (ft)       25       25       25         Link Speed (mph)       30       30       30       30         Link Distance (ft)       471       196       172         Travel Time (s)       10.7       4.5       3.9         Peak Hour Factor       0.95       0.95       0.95       0.95         Heavy Vehicles (%)       3%       0%       3%       0%       1%         Shared Lane Traffic (%)       330       0       0       277       72       293	Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Ideal Flow (vphpl)       1900       1900       1900       1900       1900       1900         Storage Length (ft)       0       0       75       75         Storage Lanes       1       0       0       1         Taper Length (ft)       25       25       25         Link Speed (mph)       30       30       30         Link Distance (ft)       471       196       172         Travel Time (s)       10.7       4.5       3.9         Peak Hour Factor       0.95       0.95       0.95       0.95         Heavy Vehicles (%)       3%       3%       0%       1%         Shared Lane Traffic (%)       1       30       0       277       72       293	Lane Configurations	Y			र्भ	<b>†</b>	7
Storage Length (ft)         0         0         75         75           Storage Lanes         1         0         0         1           Taper Length (ft)         25         25         25           Link Speed (mph)         30         30         30           Link Distance (ft)         471         196         172           Travel Time (s)         10.7         4.5         3.9           Peak Hour Factor         0.95         0.95         0.95           Heavy Vehicles (%)         3%         3%         0%         1%           Shared Lane Traffic (%)         4         4         4           Lane Group Flow (vph)         330         0         0         277         72         293	Volume (vph)	155	159	228	35	68	278
Storage Lanes         1         0         0         1           Taper Length (ft)         25         25         25         25           Link Speed (mph)         30         30         30         30           Link Distance (ft)         471         196         172           Travel Time (s)         10.7         4.5         3.9           Peak Hour Factor         0.95         0.95         0.95         0.95           Heavy Vehicles (%)         3%         3%         0%         1%           Shared Lane Traffic (%)         2         2         293	Ideal Flow (vphpl)	1900			1900	1900	
Taper Length (ft)         25         25         25           Link Speed (mph)         30         30         30           Link Distance (ft)         471         196         172           Travel Time (s)         10.7         4.5         3.9           Peak Hour Factor         0.95         0.95         0.95         0.95           Heavy Vehicles (%)         3%         3%         0%         1%           Shared Lane Traffic (%)         2         2         293	Storage Length (ft)	0	0	75			75
Link Speed (mph)         30         30         30           Link Distance (ft)         471         196         172           Travel Time (s)         10.7         4.5         3.9           Peak Hour Factor         0.95         0.95         0.95         0.95           Heavy Vehicles (%)         3%         3%         0%         1%           Shared Lane Traffic (%)         Units         Units         Units	Storage Lanes	1	0	0			1
Link Distance (ft)         471         196         172           Travel Time (s)         10.7         4.5         3.9           Peak Hour Factor         0.95         0.95         0.95         0.95           Heavy Vehicles (%)         3%         3%         0%         1%           Shared Lane Traffic (%)         2         2         293	Taper Length (ft)	25	25	25			25
Travel Time (s)         10.7         4.5         3.9           Peak Hour Factor         0.95         0.95         0.95         0.95           Heavy Vehicles (%)         3%         3%         0%         3%         0%           Shared Lane Traffic (%)         100         10.7         72         293	Link Speed (mph)	30			30	30	
Peak Hour Factor         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95         0.95 <th0.95< th="">         0.95         0.95</th0.95<>	Link Distance (ft)	471			196	172	
Heavy Vehicles (%)         3%         3%         0%         1%           Shared Lane Traffic (%)	Travel Time (s)	10.7			4.5	3.9	
Shared Lane Traffic (%)       Lane Group Flow (vph)     330     0     277     72     293	Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95
Lane Group Flow (vph) 330 0 0 277 72 293	Heavy Vehicles (%)	3%	3%	0%	3%	0%	
	Shared Lane Traffic (%)						
Sign Control Stop Free Free	Lane Group Flow (vph)	330	0	0	277	72	293
-1998), -2005 (1997) (1997) (1997) - 1997) - 1997) (1997) (1997) (1997) (1997) (1997) (1997) (1997) (1997) (1997) (1997) (1997) (1997)	Sign Control	Stop			Free	Free	
Intersection Summary	Intersection Summary					<i>2</i> 7.	· · · · · · · · · · · · · · · · · · ·

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Other Area Type: Control Type: Unsignalized

Intersection Capacity Utilization 46.1% ICU Level of Service A Analysis Period (min) 15

10/15/2008

	≯	$\mathbf{i}$	*	†	ţ	4
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	¥			र्भ	<b>†</b>	7 7
Volume (veh/h)	155	159	228	35	68	278
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95
Hourly flow rate (vph)	163	167	240	37	72	293
Pedestrians			801 A. 1278			e militada e antica interese antica e antica e substantica e antica e antica e antica e antica e antica e antic
Lane Width (ft)						
Walking Speed (ft/s)			9-11 - 1884	states of sul		
Percent Blockage	a II. A		전통 관계			이 깨끗물 가지 않는 것을 가지 않는 것을 수 없는 것을 가 없을 뿐요.
Right turn flare (veh) Median hung	9.7 - 2.994 18	989983 - L	748 ( 1. 197	N	No	
Median type Median storage veh)	82 NB2-2	69 - A.M. (* )		None	None	
Upstream signal (ft)	988 - 1986)					
pX, platoon unblocked	1889 (1279) 1889 (1277)	- 1986 (1986). -	S & 1899-90			가방했던 그 것은 것, 방법은 관계했던 의견으로 가입니다. 그렇는 것 것은 것 것은 것 같은 것 같은 것 같은 것 같은 것 같은 것 같
vC, conflicting volume	588	72	364			
vC1, stage 1 conf vol		· · · ·	004	s in Been (1944)	1 J.W. 1983	n en 1999 en 1997 en 1997 et de la Brekken (1997 en 1997) en 1997 en 1997 en 1997 et de la Brekken (1997 et de La Brekken (1997 et de la Brekken) (1997 et de la Brekken) (1997 et de la Brekken) (1997 et de la Brekken (1997
vC2, stage 2 conf vol						
vCu, unblocked vol	588	72	364	9 - 6.5%," "F 1988,	0-11080er - 19210 1	n en herden herveligtenen i herdenen offen herbeligen herveligen herveligen i erste som ensteller er som h
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)					1 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	n na sensarat sebelaken karataran terratu terrekan bateran ana takan sebarah karatar karatar harakar t
tF (s)	3.5	3.3	2.2			
p0 queue free %	57	83	80			
cM capacity (veh/h)	376	988	1206			
Direction, Lane #	EB 1	NB 1	SB 1	SB 2		
Volume Total	331	277	72	293		
Volume Left	163	240	0	0		. na statu na sana sa sana sa
Volume Right	167	0	0	293	K. M.	
cSH	548	1206	1700	1700		navna o stana anna 1920 - Sanna Sanna an Sanna Sanna Sanna Anna A
Volume to Capacity	0.60	0.20	0.04		E-228 -	- 일이 알 운영이 가락하면 이 알 가 있는 것은 것을 것 같아. 
Queue Length 95th (ft)	99	19	0	0		n Mentin (1997), Mentin et Mart (1997) - Martine (1997), Hener, Hanston, Mentin (1997)
Control Delay (s)	21.1	7.8	0.0	0.0		. 그는 경험 관계에 있는 것같은 것은 것이 같은 것이 같이 많은 것
Lane LOS	C	A		Har têka	: 16 (. <b>1</b> 6)	
Approach Delay (s) Approach LOS	21.1 C	7.8	0.0			이 있는 것은 가슴이 있는 것은 것을 가슴을 가슴 가슴을 가슴다. 
Intersection Summary						
Average Delay			9.4			
Intersection Capacity Utilizat	ion		46.1%	ାର୍ଚ୍ଚ 🖉 🖸	U Level o	of Service A
Analysis Period (min)			15			

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Lane Group	NBL	NBR	SET	SER	NWL	NWT	
Lane Configurations	- Y		1.			्त 	
Volume (vph)	51	29	117	204	40	49	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Link Speed (mph)	30		30			30	
Link Distance (ft)	403		673			909	
Travel Time (s)	9.2	8.02	15.3			20.7	
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86	
Heavy Vehicles (%)	10%	0%	2%	2%	0%	6%	
Shared Lane Traffic (%)							
Lane Group Flow (vph)	93	0	373	0	0	104	
Sign Control	Stop		Stop			Stop	
Intersection Summary							
Area Type:	Other						
Control Type: Unsignalized							
Intersection Capacity Utilization	ation 38.1%			IC	U Level	of Service A	

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Analysis Period (min) 15

	۲	۴	X	$\mathbf{i}$	₹ <b>`</b>	×
Movement	NBL	NBR	SET	SER	NWL	NWT
Lane Configurations	Y		\$			र्भ
Sign Control	Stop		Stop	8. N. N.		Stop
Volume (vph)	51	29	117	204	40	49
Peak Hour Factor	0.86	0.86	0.86	0.86	0.86	0.86
Hourly flow rate (vph)	59	34	136	237	47	57
Direction, Lane #	NB 1	SE 1	NW 1			•
Volume Total (vph)	93	373	103			
Volume Left (vph)	0	136	47			
Volume Right (vph)	34	0	57			
Hadj (s)	-0.11	0.11	-0.18			
Departure Headway (s)	4.5	4.4	4.8			
Degree Utilization, x	0.12	0.45	0.14			
Capacity (veh/h)	769	799	688			
Control Delay (s)	8.0	11.0	8.5			
Approach Delay (s)	8.0	11.0	8.5			
Approach LOS	A	В	A			
Intersection Summary	44			<i>.</i>		
Delay			10.0		Q	
HCM Level of Service			В			
Intersection Capacity Utiliza	tion		38.1%	IC	U Level o	f Service
Analysis Period (min)			15			

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Lane Group	NBL	NBT	SBT	SBR	SEL	SER	1.1			19 J.
Lane Configurations		<del>4</del> 1	ţ,		۲					
Volume (vph)	4	129	287	8	2	4	E Starter		in States	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900				
Link Speed (mph)		30	30		30					Kara -
Link Distance (ft)		92	212		622					
Travel Time (s)		2.1	4.8		14.1					
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85	a mara na sakadar			
Shared Lane Traffic (%)										
Lane Group Flow (vph)	0	157	347	0		0	والمراجع المراجع	Anton Marson		- and the second of
Sign Control	Constantine (State)	Free	Free	9. NG 82	Stop	8 G. AK				
Intersection Summary										.1
Area Type:	Other									

Control Type: Unsignalized
Intersection Capacity Utilization 25.6%
ICU Level of Service A Analysis Period (min) 15

10/15/2008

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Movement	NBL	NBT S	SBT SBR	SEL	SER
Lane Configurations		र्भ	4	Y	
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Sign Control			ree	Stop	
Grade Peak Hour Factor	0 0F		0%	0%	
Hourly flow rate (vph)	0.85 5		0.85 0.85 338 9	0.85	0.85 5
Pedestrians		192	200 2	4	2 - 1998년 1997년 1월 1997년 1월 1997년 br>1997년 1997년 1997
Lane Width (ft)					
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Percent Blockage					
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Median type		None N	one		
Median storage veh)	NAMES AND AND	23820 (T-1983) (T-			
Upstream signal (ft) pX, platoon unblocked					
vC, conflicting volume	347			504	342
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Direction, Lane #	<u>NB 1</u> 156	SB 1 S 347	<u>E1</u>		
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Volume Right	ŏ	9	5	1381. <i>3</i> 8	
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Approach Delay (s) Approach LOS	0.3	0.0 1	0.7 B		
Intersection Summary					
Average Delay	ii ii daa		0.2	<b></b>	· · · · · · · · · · · · · · · · · · ·
Intersection Capacity Util	lization	25		JU Level o	of Service A
Analysis Period (min)			15		

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# NOTICE OF INTENT FOR

# NORTH STREET CONDOMINIUMS NORTHAMPTON, MA.

PREPARED BY TOFINO ASSOCIATES, INC AND NORTHERN AVENUE HOMES, INC NOVEMBER 14, 2008

> TOFINO ASSOCIATES, INC NORTHERN AVENUE HOMES, INC 31 CAMPUS PLAZA ROAD HADLEY, MA 01035 (413) 256-0321

### **City of Northampton--Wetlands Application**

This form is required for all applications filed under the Northampton Wetlands Ordinance

File with the Office of Planning and Development, 210 Main Street, Northampton, MA 01060 We recommend applicants consult with the Land Use and Conservation Planner (587-1263) before applying

- 1. Check what kind of permit you are requesting
  - Request for Determination of Applicability (WPA form 1)
- Notice of Intent (WPA form 3)
- Abbreviated Notice of Resource Area Delineation (WPA form 4A)
- 2. Property Street Address: 8 Vican Avenue, and Machiner Avenue.
- 3. Assessors' Map and Parcel: <u>250 + 12</u> Second lot (if any) Map and Parcel(s): <u>250 + 11</u> Additional property description:
- 4. Check the items enclosed. Your application will not be accepted if any items are missing.
  - The appropriate completed Massachusetts DEP application <u>http://www.mass.gov/dep/water/approvals/wwforms.htm</u>
  - Completed versions of this Wetlands Application
  - Nine (9) copies of the fully completed and collated application packages (forms, plans and attachments)
  - All plans folded (not rolled) and collated with each application packet
  - For Notice of Intent applications only, submit the following:
    - Appropriate Notice of Intent Conservation Commission Fees <u>http://www.northamptonma.gov/opd/uploads/listWidget/2533/opd%20fees.pdf</u>
    - An abutters list of all property owners within at least 100 feet of the property line of your project. Abutters lists may be generated at <u>www.NorthamptonMA.gov/opd</u> (click on Database: Abutters, Permits and Historic). Computers are available at City Hall, Forbes and Lilly Libraries.
  - □ For **Request for Determination** applications, appropriate Request for Determination of Applicability Fees <u>http://www.northamptonma.gov/opd/uploads/listWidget/2533/opd%20fees.pdf</u>
  - □ For Notice of Resource Area Delineation use Notice of Intent Fee http://www.northamptonma.gov/opd/uploads/listWidget/2533/opd%20fees.pdf
  - A #10 business envelope addressed to the applicant.
- 5. **Provide an Existing Conditions Site Plan. Check the items shown on that plan**. You may request a waiver from submittal requirements, with a reason for the waiver request.
  - Boundary of entire lot and notation of lot area
- 11/A 🔲 Context of adjacent lots, if necessary to show extent of wetland/Riverfront Area
- Numbered wetland flags
- M/h **D** Existing and potential vernal pools
  - 50' AND 100' wetland buffer ; 32' buffer
- N/A 🔲 Mean Annual High Water line, for Riverfront Area permits
- 100' inner riparian zone AND 200' outer riparian zone, for Riverfront Area permits
  - Existing structures, impervious surfaces (ie: pavement, gravel) and lawn areas
    - Edge of vegetation accurately measured or surveyed
    - Significant (8"+ Diameter Breast Height) trees within the limit of work area that are also within the 200' Riverfront Area, Bordering Vegetated Wetland, or 100' wetland buffer
    - 2' contours
- $\mathbb{N}/\mathbb{A}$   $\square$  Elevations in feet (not meters), for projects within the floodplain
  - Zoning setbacks
  - □ 1:20 scale, if possible

- 6. If new work is proposed, provide a Proposed Site Plan. Check the items shown on that plan. You may request a waiver from submittal requirements, with a reason for the waiver request.
  - Grading/proposed new contours
  - Hardscape (i.e.: footprint of house, driveway, walkways, terraces, etc...)
  - Any removal of vegetation and significant trees within the Riverfront Area, wetland and buffer
  - Landscaping and plantings within the Riverfront Area, wetland and wetland buffer
  - Location of erosion control barrier
  - Limit of work line
  - Utility lines
  - Stormwater Management Form (use DEP form <u>www.mass.gov/dep/brp/ww/wwforms.htm</u>), if required

₩/A □ Wildlife assessment if the site is in a habitat resource area based on NHESP maps, Northampton Potential and Certified Vernal Pools Map or otherwise required by the Act or Ordinance.

At the same scale as the Existing Conditions Site Plan

 $\mathbb{W}/\mathbb{A}$  **D** For new homes in the Riverfront Area only, documentation of the date the lot was recorded.

# 7. We have provided and requested information and believe and understand that (initial each item below):

Application deadline is one calendar month prior to a public hearing. If the application is incomplete or waivers are requested, however, the public hearing may be delayed; We will check for the date and time of our public hearing at <u>www.NorthamptonMA.gov</u> or in the *Daily* 

*Hampshire Gazette* Legal Ads section. Such notice is posted seven days prior to the public hearing; The Conservation Commission may request an alternatives analysis for work proposed within the buffer zone of a wetland:

The Conservation Commission and their representatives have permission to enter the property;

All documents and plans submitted are in the public domain and may be copied freely in any form; and

* The City will record Orders of Conditions and Order of Resource Area Delineations at the Hampshire

County Registry of Deeds.

# 8. PLEASE COMPLETE ONLY IF APPLYING FOR A NOTICE OF INTENT or ABBREVIATED NOTICE OF RESOURCE ARE DELINEATION:

We certify under the pains and penalties of perjury, that PRIOR to filing this application all abutters were notified of this application pursuant to the requirements of M.G.L. c. 131 § 40. Notice must be made in writing by hand delivery or certified mail (return receipt requested) to all abutters within 100 feet of the property line of the project location.

 $\Lambda$ 

Applicant (print or type): Applicant (print or type): Applicant Applicant (print or type): Applicant Appli	nd of the
Applicant (print or type): Martharen han handen the.	_Applicant Signature:
Address: 31 Compare March P. Hadlog	Applicant Phone: 1136 1939.
Owner (print or type):	_Owner Signature:
Address:	_Owner Phone:

Date submitted: 11 - 11 - 15

The Northampton Conservation Commission generally meets on the 2nd and 4th Thursdays of each month in Hearing Room 18 located on the 2nd floor of City Hall, 210 Main Street

### NOTICE OF INTENT NORTH STREET CONDOMINIUMS PROJECT NARRATIVE

This Notice of Intent is being submitted to the Northampton Conservation Commission for the construction of a 25-unit townhouse condominium project, with associated roadway and stormwater management system, on property consisting of 2 parcels totaling approximately 5.6 acres, located ½ mile from downtown.

#### **Existing Conditions**

The property is located off View Avenue, a private way off North Street owned by the applicant, and off the end of Northern Avenue. There is an intermittent stream that flows from the Industrial Park on the north, through a culvert under the new bike path. The stream is also fed by the storm drain system on Northern Avenue, which flows into the swale adjacent to the bike path. There are bordering vegetated wetlands associated with the intermittent stream. The property slopes gradually and drains toward the BVW.

The wetland and areas of upland within the wetland have some significant native trees, but there are many invasive plant species in the area, including multi-flora rose, honeysuckle, and poison ivy. The adjacent uplands are also degraded by historic filling, masonry and other construction and road building debris.

The property has an existing house near View Avenue, for which a demolition permit has already been obtained. The house is surrounded by lawn, with a low stone wall at the edge of a portion of the lawn, and a plantation of non-native Norway Spruces beyond the lawn.

#### **Proposed Work**

The proposed project consists of a duplex on Northern Avenue and 23 townhouse condominiums off North Street, for a total of 25 new dwelling units, with associated roadways, parking areas, driveways, sidewalks, utilities, landscaping and stormwater management system. There is approximately 2.2 acres of Bordering Vegetated Wetland. No alteration of any resource area is proposed, but a large portion of the project falls within the Buffer Zone of the BVW.

Five of the six buildings, each containing 2-6 units, fall within the 100-foot Buffer Zone. All buildings are outside the 35 foot wetland buffer.

Roof run-off is infiltrated through the use of linear dry wells at the rear of units 1-2, 3-7, 8-13, and 22-25. Roof run-off from units 14-15, as well as some road run-off, is also treated in the infiltration trench behind units 14-15. All road run-off is pretreated before it enters a detention basin. Mechanisms to treat water quality include a rain garden/bio-retention basin, proprietary treatment chamber, and deep sump hooded catch basins.

There are 2 detention basins and a bio-retention basin, each located within the 100-foot Buffer Zone. All grading, pipes and outfall structures are kept at least 12 feet from the BVW.

Utilities will be installed to service the lots as follows: Sewer: All units are sewered by the City sewer system. Water: All units are serviced by the City water system. Electric, Telephone and Cable Systems: All units are served by underground services. Natural Gas: All units are served by underground gas service.

No work is proposed that will enter or alter the 2.2 acre Bordering Vegetated Wetland resource areas.

#### **Relationship to the Northampton Wetlands Protection Ordinance**

The North Street condominium project is a true infill project, providing an attractive residential option within easy walking distance of schools, jobs, retail establishments, restaurants and entertainment.

Section 337-10(B) of the City Code states that "To encourage infill development, which is considered more sustainable under the principles of smart growth and generally has a smaller environmental footprint than development in outlying areas, in ... Urban Residential-B... Zoning Districts, the Conservation Commission hereby waives any of the § 337-10 performance standards that are over and above state law with the exception of the setback requirements in Table (1):

Zoning District	No-Encroachment Zone
Urban Residential-B and Urban Residential-C	35 feet from wetlands; 10 feet from wetlands may be allowed at the discretion of the Conservation Commission if applicant provides extraordinary mitigation, replication, restoration or open space preservation measures

The plans show all buildings at least 35 feet from the BVW. Grading, walls, yards, patios, and certain components of the stormwater management system are kept at least 12 feet from the BVW. To the best of our knowledge, this is the first time a request has been made to reduce the No Encroachment Zone from 35 feet to 10 feet under this specific section of the new City Wetlands Ordinance. We are interested in discussing with the Conservation Commission what mitigation or open space preservation measures would be appropriate to permit the proposed reduction.

#### **Bordering Vegetated Wetland Delineation Method**

The boundaries of the Bordering Vegetated Wetlands on site were flagged by Chuck Dauchy using wetland vegetation and soil indicators, and were accepted by the Northampton Conservation Commission with a positive determination issued August 24, 2007. A copy of the Determination is attached to this Notice of Intent.

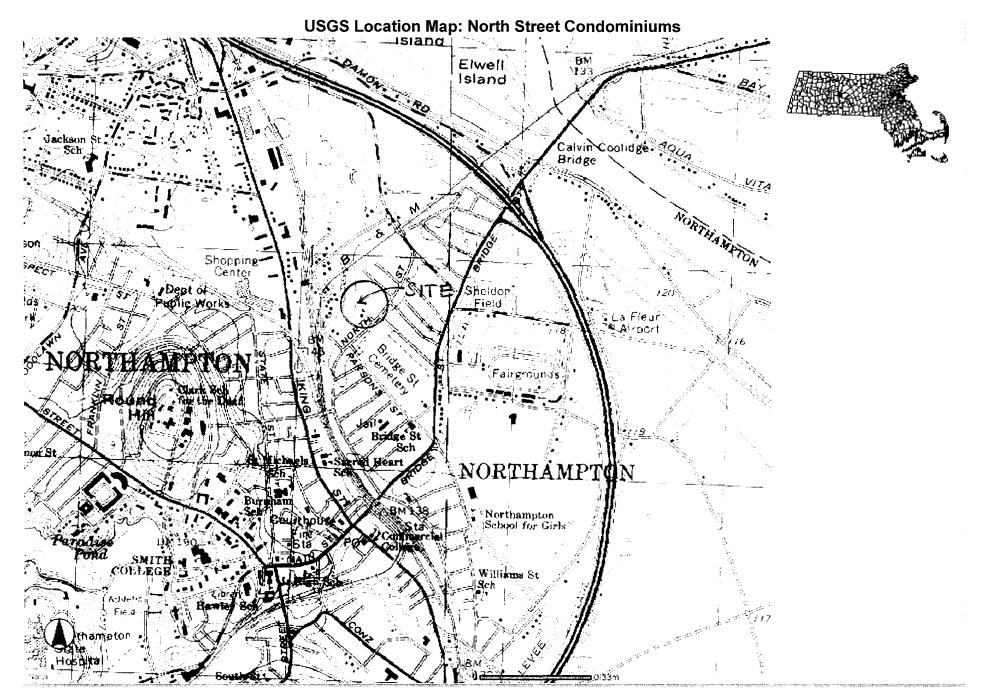
#### Mitigation of Potential Impacts to Resource Areas

Erosion controls will consist of entrenched silt fencing, located no closer than 10' to the wetland buffer as shown on the plan. This will be the limit of work line. Erosion controls will remain in place until construction is complete and exposed soils have been successfully stabilized by vegetation.

Wetland markers, clearly visible at 18 inches above grade, have been installed and will remain in place during construction. Afterward, they will be hammered flush with the ground and left in place permanently.

#### Additional Information

USGS Location Map WPA Form 3 – Notice of Intent Notification Sent to Abutters Abutters List for Map 25C, Parcels 12 and 17 Summary Stormwater Report Determination of Applicability, Issued August 24, 2007 "Site Plan" by the Berkshire Design Group, dated Full Stormwater Report





Bureau of Resource Protection - Wetlands

WPA Form 3 – Notice of Intent Massachusetts Wetlands Protection Act M.G.L. c. 131, §40 Provided by MassDEP:

MassDEP File Number

Document Transaction Number Northampton City/Town

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



Note:
Before
completing this
form consult
your local
Conservation
Commission
regarding any
municipal bylaw
or ordinance.

•	Project Location (Note: electronic filers will click on button to locate project site):				
	Northern Avenue		Northampton	01060	
	a. Street Address		b. City/Town	c. Zip Code	
	Latitude and Longitu	ude:	d. Latitude	e. Longitude	
	25C		12 & 17	e. Longitude	
	f. Assessors Map/Plat Nu	umber	g. Parcel /Lot Number		
	Applicant:				
	a. First Name		b. Last Name		
		nc. and Northern Aven	ue Homes, Inc.		
	c. Organization	load			
	31 Campus Plaza R d. Street Address	luau	100 m		
	Hadley		MA	01035	
	e. City/Town		f. State	g. Zip Code	
	(413) 256-0321	(413) 256-0130		0,	
	h. Phone Number	i. Fax Number	j. Email Address		
	a. First Name	uired if different from a	pplicant): Check if n	nore than one owner	
	a. First Name c. Organization	uired if different from a	···	nore than one owner	
	a. First Name	uired if different from a	···	nore than one owner	
	a. First Name c. Organization	uired if different from a	···	nore than one owner	
	a. First Name c. Organization d. Street Address	uired if different from a	b. Last Name		
-	a. First Name c. Organization d. Street Address e. City/Town	i. Fax Number	b. Last Name		
-	a. First Name c. Organization d. Street Address e. City/Town h. Phone Number	i. Fax Number	b. Last Name		
-	a. First Name c. Organization d. Street Address e. City/Town h. Phone Number Representative (if ar	i. Fax Number	b. Last Name f. State j. Email address		
-	a. First Name c. Organization d. Street Address e. City/Town h. Phone Number Representative (if ar a. First Name	i. Fax Number	b. Last Name f. State j. Email address		
-	a. First Name c. Organization d. Street Address e. City/Town h. Phone Number Representative (if ar a. First Name c. Company	i. Fax Number	b. Last Name f. State j. Email address		

a. Total Fee Paid



Bureau of Resource Protection - Wetlands

# WPA Form 3 – Notice of Intent

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

Provided by	MassDEP:
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MassDEP File Number

**Document Transaction Number** Northampton City/Town

# A. General Information (continued)

6. General Project Description:

The proposed project consists of a duplex on Northern Avenue and 23 townhouse condominiums off North Street, for a total of 25 new dwelling units, with associated stormwater management, site, utility and road work. A portion of the project falls within the Buffer Zone of BVW. No alteration of any resource area is proposed.

#### 7a. Project Type Checklist:

1. 🔲 Single Family Home	2. 🛛 Residential Subdivision
3. Limited Project Driveway Crossing	4. Commercial/Industrial
5. Dock/Pier	6. 🔲 Utilities
7. 🗌 Coastal Engineering Structure	8. Agriculture (e.g., cranberries, forestry)
9. Transportation	10. 🗌 Other
Is any portion of the proposed activity eligible to be 10.24 (coastal) or 310 CMR 10.53 (inland)?	treated as a limited project subject to 310 CMR
1. Yes No If yes, describe which limite	d project applies to this project:

2. Limited Project

7b.

8. Property recorded at the Registry of Deeds for:

Hampshire	
a. County	b. Certificate # (if registered land)
Book 8428, Page 219	Book 8829, Page 341
c. Book and Page	d. Book and Page

### B. Buffer Zone & Resource Area Impacts (temporary & permanent)

- 1. Buffer Zone Only Check if the project is located only in the Buffer Zone of a Bordering Vegetated Wetland, Inland Bank, or Coastal Resource Area.
- 2. Inland Resource Areas (see 310 CMR 10.54-10.58; if not applicable, go to Section B.3, Coastal Resource Areas).

Check all that apply below. Attach narrative and any supporting documentation describing how the project will meet all performance standards for each of the resource areas altered, including standards requiring consideration of alternative project design or location.

For all projects affecting other	Resou	rce Area	Size of Proposed Alteration	Proposed Replacement (if any)
Resource Areas, please attach a narrative	a. 🗌	Bank	1. linear feet	2. linear feet
explaining how the resource area was	b. 🗌	Bordering Vegetated Wetland	1. square feet	2. square feet
delineated.	c. 🗌	Waterbodies and	1. linear feet	2. linear feet
		Waterways	3. cubic yards dredged	



Bureau of Resource Protection - Wetlands

WPA Form 3 – Notice of Intent

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Provided by MassDEP:

MassDEP File Number

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# B. Buffer Zone & Resource Area Impacts (temporary & permanent) (cont'd)

Resou	irce Area	Size of Proposed Alteration	Proposed Replacement (if any)
d. 🗌	Bordering Land Subject to Flooding	1. square feet	2. square feet
		3. cubic feet of flood storage lost	4. cubic feet replaced
e. 🗌	Isolated Land Subject to Flooding	1. square feet	
		2. cubic feet of flood storage lost	3. cubic feet replaced
f. 🗌	Riverfront Area	1. Name of Waterway (if available)	
2.	Width of Riverfront Area (ch	eck one):	
	25 ft Designated De	ensely Developed Areas only	
	🔲 100 ft New agricultu	ral projects only	
	🔲 200 ft All other proje	ects	
3.	Total area of Riverfront Area	a on the site of the proposed project	square feet
4.	Proposed alteration of the F	Riverfront Area:	
	total square feet	-	c. square feet between 100 ft. and 200 ft.
5.	Has an alternatives analysis	been done and is it attached to this	NOI?
6.	Was the lot where the activi	ty is proposed created prior to Augu	st 1, 1996? 🗌 Yes 🗌 No
3. 🗌 Co	astal Resource Areas: (See	310 CMR 10.25-10.35)	
will m	eet all performance standard	n narrative and supporting documents is for each of the resource areas alto ve project design or location.	
Reso	urce Area	Size of Proposed Alteration	Proposed Replacement (if any)
a. 🗌	Designated Port Areas	Indicate size under Land Under th	ne Ocean, below
b. 🗌	Land Under the Ocean	1. square feet	
		2. cubic yards dredged	
c. 🗌	Barrier Beach	Indicate size under Coastal Beach	es and/or Coastal Dunes below
d. 🗌	Coastal Beaches	1. square feet	2. cubic yards beach nourishment
e. 🗌	Coastal Dunes	1. square feet	2. cubic yards dune nourishment

Online Users: Include your document transaction number (provided on your receipt page) with all supplementary information you submit to the Department.



Bureau of Resource Protection - Wetlands

WPA Form 3 – Notice of Intent

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Provided by MassDEP:

MassDEP File Number

Document Transaction Number Northampton City/Town

# B. Buffer Zone & Resource Area Impacts (temporary & permanent) (cont'd)

		Size of Proposed Alteration	Proposed Replacement (if any)
f. 🗌	Coastal Banks	1. linear feet	
g. 🗌	Rocky Intertidal Shores	1. square feet	
h. 🗌	Salt Marshes	1. square feet	2. sq ft restoration, rehab., creation
i. 🗌	Land Under Salt Ponds	1. square feet	
		2. cubic yards dredged	
j. 🗌	Land Containing Shellfish	1. square feet	
k. 🗌	Fish Runs		nks, inland Bank, Land Under the er Waterbodies and Waterways,
		1. cubic yards dredged	
I. 🗌	Land Subject to		
	Coastal Storm Flowage	1. square feet	
	storation/Enhancement	e	
		f restoring or enhancing a wetland	
square	: ioolaye liial iias been en	tered in Section B.2.b or B.3.h abo	we, please enter the additional

4.

amount here.

a. square feet of BVW	b. square feet of Salt Marsh

# C. Other Applicable Standards and Requirements

# Streamlined Massachusetts Endangered Species Act/Wetlands Protection Act Review

1. Is any portion of the proposed project located in Estimated Habitat of Rare Wildlife as indicated on the most recent Estimated Habitat Map of State-Listed Rare Wetland Wildlife published by the Natural Heritage and Endangered Species Program (NHESP)? To view habitat maps, see the Massachusetts Natural Heritage Atlas or go to http://www.mass.gov/dfwele/dfw/nhesp/nhreamap.htm.

If yes, include proof of mailing or hand delivery of NOI to: a. 🗌 Yes 🕅 No

	Natural Heritage and Endangered Species Program Division of Fisheries and Wildlife
2008 (MassGIS)	Route 135, North Drive Westborough, MA 01581
b. Date of map	Westbolough, WA 01561

If yes, the project is also subject to Massachusetts Endangered Species Act (MESA) review (321 CMR 10.18). To qualify for a streamlined, 30-day, MESA/Wetlands Protection Act review, please complete Section C.1.C. and include requested materials with this Notice of Intent (NOI); OR complete Section C.1.d, if applicable. If MESA supplemental information is not included with the NOI. by completing Section 1 of this form, the NHESP will require a separate MESA filing which may take up to 90 days to review (unless noted exceptions in Section 2 apply, see below).

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Bureau of Resource Protection - Wetlands

Provided by MassDEP:

MassDEP File Number

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

Document Transaction Number Northampton City/Town

# C. Other Applicable Standards and Requirements (cont'd)

- 1. c. Submit Supplemental Information for Endangered Species Review *

1.	Percentage/acreage of property to be altered	1:	
	(a) within wetland Resource Area	percentage/acreage	
	(b) outside Resource Area	percentage/acreage	
2.	Assessor's Map or right-of-way plan of s	site	
3.	3. Project plans for entire project site, including wetland resource areas and areas or wetlands jurisdiction, showing existing and proposed conditions, existing and propose tree/vegetation clearing line, and clearly demarcated limits of work **		
	(a) Project description (including descrip buffer zone)	tion of impacts outside of wetland resource area &	
	(b) D Photographs representative of the sit	e	
	(c) ☐ MESA filing fee (fee information avail <u>http://www.mass.gov/dfwele/dfw/nhes</u> Make check payable to "Natural Heritag <i>NHESP</i> at above address		
	Projects altering <b>10 or more acres</b> of land, also	submit:	
	(d) Uegetation cover type map of site		
	(e) Project plans showing Priority & Estir	nated Habitat boundaries	
d. OR	Check One of the Following		
<u>htt</u>	Project is exempt from MESA review. each applicant letter indicating which MESA ex p://www.mass.gov/dfwele/dfw/nhesp/nhenvex HESP if the project is within estimated habitat	cemptions.htm; the NOI must still be sent to	
2. [	Separate MESA review ongoing.		
	a. NHESP Tracking Number	b. Date submitted to NHESP	
3. [		mination or valid Conservation & Management	

- * Some projects not in Estimated Habitat may be located in Priority Habitat, and require NHESP review (see www.nhesp.org regulatory review tab). Priority Habitat includes habitat for statelisted plants and strictly upland species not protected by the Wetlands Protection Act.
- MESA projects may not be segmented (321 CMR 10.16). The applicant must disclose full development plans ** even if such plans are not required as part of the Notice of Intent process.



Bureau of Resource Protection - Wetlands

Provided by MassDEP:

MassDEP File Number

# WPA Form 3 – Notice of Intent

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Document Transaction Number Northampton City/Town

# C. Other Applicable Standards and Requirements (cont'd)

- 2. For coastal projects only, is any portion of the proposed project located below the mean high water line or in a fish run?
  - a. 🛛 Not applicable project is in inland resource area only

b. 🗌 Yes 📋 No

es 🗌 No 🛛 If yes, include proof of mailing or hand delivery of NOI to either:

South Shore - Cohasset to Rhode Island, and the Cape & Islands:

Division of Marine Fisheries -Southeast Marine Fisheries Station Attn: Environmental Reviewer 838 South Rodney French Blvd. New Bedford, MA 02744 North Shore - Hull to New Hampshire:

Division of Marine Fisheries -North Shore Office Attn: Environmental Reviewer 30 Emerson Avenue Gloucester, MA 01930

Also if yes, the project may require a Chapter 91 license. For coastal towns in the Northeast Region, please contact MassDEP's Boston Office. For coastal towns in the Southeast Region, please contact MassDEP's Southeast Regional Office.

If yes, provide name of ACEC (see instructions to WPA Form 3 or MassDEP

Website for ACEC locations). Note: electronic filers click on Website.

3. Is any portion of the proposed project within an Area of Critical Environmental Concern (ACEC)?

Online	Users:
Include	vour

Include your document transaction number (provided on your receipt page) with all supplementary information you submit to the Department.

b. ACEC

4. Is any portion of the proposed project within an area designated as an Outstanding Resource Water (ORW) as designated in the Massachusetts Surface Water Quality Standards, 314 CMR 4.00?

a. 🗌 Yes 🛛 No

a. 🗌 Yes 🛛 No

5. Is any portion of the site subject to a Wetlands Restriction Order under the Inland Wetlands Restriction Act (M.G.L. c. 131, § 40A) or the Coastal Wetlands Restriction Act (M.G.L. c. 130, § 105)?

a. 🗌 Yes 🛛 No

- 6. Is this project subject to provisions of the MassDEP Stormwater Management Standards?
  - a. Xes. Attach a copy of the Stormwater Report as required by the Stormwater Management Standards per 310 CMR 10.05(6)(k)-(q) and check if:
    - 1. Applying for Low Impact Development (LID) site design credits (as described in Stormwater Management Handbook Vol. 2, Chapter 3)
    - 2. A portion of the site constitutes redevelopment
    - 3. Proprietary BMPs are included in the Stormwater Management System.
  - b. No. Check why the project is exempt:
    - 1. Single-family house
    - 2. Emergency road repair
    - 3. Small Residential Subdivision (less than or equal to 4 single-family houses or less than or equal to 4 units in multi-family housing project) with no discharge to Critical Areas.



# epartment of Environmental Protection س Massachusetts

Bureau of Resource Protection - Wetlands

# WPA Form 3 – Notice of Intent

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

Provided by MassDEP:

MassDEP File Number

Document Transaction Number Northampton City/Town

# **D.** Additional Information

Applicants must include the following with this Notice of Intent (NOI). See instructions for details.

**Online Users:** Attach the document transaction number (provided on your receipt page) for any of the following information you submit to the Department.

- 1. USGS or other map of the area (along with a narrative description, if necessary) containing sufficient information for the Conservation Commission and the Department to locate the site. (Electronic filers may omit this item.)
- 2. Plans identifying the location of proposed activities (including activities proposed to serve as a Bordering Vegetated Wetland [BVW] replication area or other mitigating measure) relative to the boundaries of each affected resource area.
- 3. Identify the method for BVW and other resource area boundary delineations (MassDEP BVW Field Data Form(s), Determination of Applicability, Order of Resource Area Delineation, etc.), and attach documentation of the methodology.
- 4.  $\square$  List the titles and dates for all plans and other materials submitted with this NOI.

Notice of Intent Plans for North Street	Condominiums, sheets L1-5, EC1	
a. Plan Title		
The Berkshire Design Group	Mark Darnold	
b. Prepared By	c. Signed and Stamped by	
November 11, 2008	varies	
d. Final Revision Date	e. Scale	

f. Additional Plan or Document Title

g. Date

- 5. If there is more than one property owner, please attach a list of these property owners not listed on this form.
- 6. Attach proof of mailing for Natural Heritage and Endangered Species Program, if needed.
- 7. Attach proof of mailing for Massachusetts Division of Marine Fisheries, if needed.
- 8. Attach NOI Wetland Fee Transmittal Form
- 9. Attach Stormwater Report, if needed.

### E. Fees

1. Fee Exempt: No filing fee shall be assessed for projects of any city, town, county, or district of the Commonwealth, federally recognized Indian tribe housing authority, municipal housing authority, or the Massachusetts Bay Transportation Authority.

Applicants must submit the following information (in addition to pages 1 and 2 of the NOI Wetland Fee Transmittal Form) to confirm fee payment:

5083	11-10-2008	
2. Municipal Check Number	3. Check date	
5077	11-10-2008	
4. State Check Number	5. Check date	
Northern Avenue Homes, Inc.		
6. Payor name on check: First Name	7. Payor name on check: Last Name	

Payor name on check: Last Name



Bureau of Resource Protection - Wetlands

# WPA Form 3 – Notice of Intent

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

Provided by MassDEP:

MassDEP File Number

Document Transaction Number Northampton City/Town

# F. Signatures and Submittal Requirements

I hereby certify under the penalties of perjury that the foregoing Notice of Intent and accompanying plans, documents, and supporting data are true and complete to the best of my knowledge. I understand that the Conservation Commission will place notification of this Notice in a local newspaper at the expense of the applicant in accordance with the wetlands regulations, 310 CMR 10.05(5)(a).

I further certify under penalties of perjury that all abutters were notified of this application, pursuant to the requirements of M.G.L. c. 131, § 40. Notice must be made by Certificate of Mailing or in writing by hand delivery or certified mail (return receipt requested) to all abutters within 100 feet of the property line of the project location.

cl cill	11-13-2008
1. Signature of Applicant	2. Date
3. Signature of Property Owner (if different)	4. Date
5. Signature of Representative (if any)	6. Date

#### For Conservation Commission:

Two copies of the completed Notice of Intent (Form 3), including supporting plans and documents, two copies of the NOI Wetland Fee Transmittal Form, and the city/town fee payment, to the Conservation Commission by certified mail or hand delivery.

#### For MassDEP:

One copy of the completed Notice of Intent (Form 3), including supporting plans and documents, one copy of the NOI Wetland Fee Transmittal Form, and a **copy** of the state fee payment to the MassDEP Regional Office (see Instructions) by certified mail or hand delivery.

#### Other:

If the applicant has checked the "yes" box in any part of Section C, Item 3, above, refer to that section and the Instructions for additional submittal requirements.

The original and copies must be sent simultaneously. Failure by the applicant to send copies in a timely manner may result in dismissal of the Notice of Intent.



# Massachusetts Jepartment of Environmental Protection Bureau of Resource Protection - Wetlands NOI Wetland Fee Transmittal Form

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return



# A. Applicant Information

1. Applicant:

a. First Name		b. Last Name	
Tofino Associates, Ir	nc. and Northern Avenue F	Homes, Inc.	
c. Organization			
31 Campus Plaza Re	oad		
d. Mailing Address			
Hadley		MA	01035
e. City/Town		f. State	g. Zip Code
(413) 256-0321	(413) 256-0130		
h. Phone Number	i. Fax Number	j. Email Address	

2. Property Owner (if different):

a. First Name		b. Last Name		
c. Organization				
d. Mailing Address				
e. City/Town		f. State	g. Zip Code	
h. Phone Number	i. Fax Number	j. Email Address		
Project Location:				
Northern Avenue		Northampton		
a. Street Address		b. City/Town		

To calculate filing fees, refer to the category fee list and examples in the instructions for filling out WPA Form 3 (Notice of Intent).

# **B.** Fees

The fee should be calculated using the following six-step process and worksheet. **Please see Instructions before filling out worksheet.** 

**Step 1/Type of Activity:** Describe each type of activity that will occur in wetland resource area and buffer zone.

Step 2/Number of Activities: Identify the number of each type of activity.

**Step 3/Individual Activity Fee:** Identify each activity fee from the six project categories listed in the instructions.

**Step 4/Subtotal Activity Fee:** Multiply the number of activities (identified in Step 2) times the fee per category (identified in Step 3) to reach a subtotal fee amount. Note: If any of these activities are in a Riverfront Area in addition to another Resource Area or the Buffer Zone, the fee per activity should be multiplied by 1.5 and then added to the subtotal amount.

Step 5/Total Project Fee: Determine the total project fee by adding the subtotal amounts from Step 4.

**Step 6/Fee Payments:** To calculate the state share of the fee, divide the total fee in half and subtract \$12.50. To calculate the city/town share of the fee, divide the total fee in half and add \$12.50.



### Massachusetts Jepartment of Environmental Protection Bureau of Resource Protection - Wetlands **NOI Wetland Fee Transmittal Form** Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

### **B.** Fees (continued)

Step 1/Type of Activity	Step 2/Number of Activities	Step 3/Individual Activity Fee	Step 4/Subtotal Activity Fee
Category 3(b) – each building	5	\$1,050	\$5,250
	Step 6/F	tal Project Fee: ee Payments: Project Fee:	\$5,250
	State share	of filing Fee:	a. Total Fee from Step 5 \$2,612.50 b. 1/2 Total Fee less \$12.50 \$2,637.50 c. 1/2 Total Fee plus \$12.50

# C. Submittal Requirements

a.) Complete pages 1 and 2 and send with a check or money order for the state share of the fee, payable to the Commonwealth of Massachusetts.

Department of Environmental Protection Box 4062 Boston, MA 02211

b.) To the Conservation Commission: Send the Notice of Intent or Abbreviated Notice of Intent; a copy of this form; and the city/town fee payment.

**To MassDEP Regional Office** (see Instructions): Send a copy of the Notice of Intent or Abbreviated Notice of Intent; a **copy** of this form; and a **copy** of the state fee payment. (E-filers of Notices of Intent may submit these electronically.)

5077 网络拉尔斯拉马林 医结肠切开的 建分离合 ST CAMPUS PLAZA ROAD, SUITE 1 HADLEY, MA 01035 (413) 256-0321 ****************Two thousand six hundred twelve dollars and 50 cents Pay: November 10, 20085077 \$*****2,612.50 Commonwealth of Massachusetts 1054265434 5083 MODIFICE AVENUE HOMES NO. 31 CAMPUS PLAZA ROAD, SUITE 3 HADLEY, MA 01035 (413) 256-0321 ***********Two thousand seven hundred thirty-seven dollars and 50 cents Pay: November^{DAJE}, 2008</sup> CHECK083 \$****^{*}²,737.50 City of Northampton 212 Main Street Northampton, MA 01060 "005083" :: 21187172: 10542654941



# A. Introduction

#### Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return



The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report

certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

A Stormwater Report must be submitted with the Notice of Intent permit application to document

compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for

the Stormwater Report (which should provide more substantive and detailed information) but is offered

Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist,

Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and

the Stormwater Report must contain the engineering computations and supporting information set forth in

here as a tool to help the applicant organize their Stormwater Management documentation for their

- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



# B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

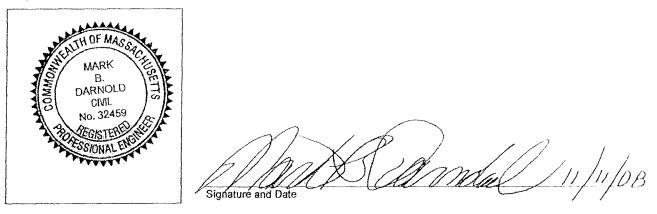
*Note:* Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

# **Registered Professional Engineer's Certification**

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application

Registered Professional Engineer Block and Signature



# Checklist

**Project Type:** Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



#### Checklist (continued)

**LID Measures:** Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

- No disturbance to any Wetland Resource Areas
- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
  - Credit 1
  - Credit 2
  - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe):

#### Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



# **Checklist for Stormwater Report**

#### Checklist (continued)

#### Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.
- Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

#### Standard 3: Recharge

- Soil Analysis provided.
- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

🛛 Static	🗌 Simple Dynamic	
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- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

Dynamic Field¹

- Recharge BMPs have been sized to infiltrate the Required Recharge Volume for its respective drainage area.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
  - Site is comprised solely of C and D soils and/or bedrock at the land surface
  - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
  - Solid Waste Landfill pursuant to 310 CMR 19.000
  - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



#### Checklist (continued)

#### Standard 3: Recharge (continued)

The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.

Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

#### Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- · Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
  - is within the Zone II or Interim Wellhead Protection Area
  - is near or to other critical areas
  - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
  - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



## Checklist (continued)

#### Standard 4: Water Quality (continued)

ד 🛛	The BMP	is sized	(and calculations	provided	) based	on:
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- The ¹/₂" or 1" Water Quality Volume or
- The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.

$\Box$	A TMDL exists that indicates a need to reduce pollutants other than	TSS and documentation showing
	that the BMPs selected are consistent with the TMDL is provided.	

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs) Not Applicable – Proposed project site is not expected to yield high potential pollutant loads.

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted *prior to* the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has not been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

#### Standard 6: Critical Areas Not Applicable – The project site does not discharge to a critical area.

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



**Checklist for Stormwater Report** 

#### Checklist (continued)

# Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

- The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:site with only "Hydrologic Group C" Soils
  - Limited Project
  - Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
  - Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
  - Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
  - Bike Path and/or Foot Path
  - Redevelopment Project
  - Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.
- ☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

#### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



#### Checklist (continued)

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the DRAFT SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

#### **Standard 9: Operation and Maintenance Plan**

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
  - Name of the stormwater management system owners;
  - Party responsible for operation and maintenance;
  - Schedule for implementation of routine and non-routine maintenance tasks;
  - Plan showing the location of all stormwater BMPs maintenance access areas;
  - Description and delineation of public safety features;
  - Estimated operation and maintenance budget; and
  - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
  - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
  - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

#### Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

#### Notification to Abutters

#### Under the Massachusetts Wetlands Protection Act and the City of Northampton Wetlands Protection Ordinance

In accordance with the second paragraph of Massachusetts General Laws Chapter 131, Section 40 and the Town of Amherst Wetlands Protection Bylaw, you are hereby notified of the following.

- A. The name of the applicant is <u>Tofino Associates</u>, Inc. and Northern Avenue Homes, Inc.
- B. The applicant has filed a Notice of Intent with the Conservation Commission for the municipality of <u>Northampton</u> under the Wetlands Protection Act (General Laws Chapter 131, section 40) and the City of Northampton Wetlands Protection Ordinance.
- C. The address of the property where the Orders of Conditions is requested is <u>8 View</u> <u>Avenue and Northern Avenue</u> Parcel ID: Map 25C, Parcels 12 and 17
- D. Copies of the filings may be examined by contacting the Northampton Conservation Commission.
- E. Copies of the filings may be obtained from either (check one): the applicant [X], or the applicant's representative [] by calling this telephone number (413) 256-0321 between the hours of 9 am and 5 pm on the following days of the week: Monday through Friday for a printing fee of \$50.00.

NOTE: Notice of the public hearing, including its exact date, time, and location, will be published at least five (5) days in advance in the <u>Daily Hampshire Gazette</u>.

NOTE: Notice of the public hearing, including its date, time, and location, will be posted in the City Hall not less than forty-eight (48) hours in advance.

NOTE: Details of the public hearing, including its date, time, and location, can be seen at the City Website calendar at <u>www.NorthamptonMA.gov/calendar/</u>

NOTE: You also may contact your local Conservation Commission or the nearest Department of Environmental Protection Regional Office for more information about this application or the Wetlands Protection Act. To contact DEP, call:

Central Region: 508-792-7650	Northeast Region: 617-935-2160
Southeast Region: 508-946-2800	Western Region: 413-784-1100

2.5 C. - 17. 166 aballer:

ARCHAMBAULT GERALD R & MARY E 150 NORTH ST NORTHAMPTON, MA 01060	CARLBERG IRENE M & 57 WOODMONT RD NORTHAMPTON, MA 01060	DEVINE JOYCE E 1 VIEW AVE NORTHAMPTON, MA 01060
FENTON JOHN ROBERT & JOAN A 164 NORTH ST NORTHAMPTON, MA 01060	FREEMAN-DANIELS OWEN D 53A WOODMONT RD NORTHAMPTON, MA 01060	JACKSON CAROLE A & 90 WOODMONT RD NORTHAMPTON, MA 01060
MALONEY DIANE A 168 NORTH ST NORTHAMPTON, MA 01060	MASSACHUSETTS COMMONWEALTH OF DAMON RD NORTHAMPTON, MA 01060	MCELHANEY DOUGLAS J & 51 WOODMONT RD NORTHAMPTON, MA 01060
NORTHAMPTON CITY OF 210 MAIN STREET NORTHAMPTON, MA 01060	NORTHERN AVENUE HOMÉS INC 31 CAMPUS PLAZA RD HADLEY, MA 01035	OLANDER RAE 85 WOODMONT RD NORTHAMPTON, MA 01060
PAULINSKI DAWN TRUSTEE 25 SYCAMORE ST SAN FRANCISCO, CA 94110	87 WOODMONT RD	REITER JENNIFER B & 351 PLEASANT ST PMB 222 NORTHAMPTON, MA 01060
TATRO LAWRENCE R & KAREN K 188 BRIDGE ST NORTHAMPTON, MA 01060	TOFINO ASSOCIATES INC 31 CAMPUS PLAZA RD HADLEY, MA 01035	WALDRON ELIZABETH C 176 NORTH ST NORTHAMPTON, MA 01060
ZIPPAY MARLA		

ZIPPAY MARLA 53B WOODMONT RD UNIT 1 NORTHAMPTON, MA 01060

# The off Hold Aballing

CAPERS PHYLLIS A & RAYMOND L 48 NORTHERN AVE NORTHAMPTON, MA 01060	FENTON JOHN ROBERT & JOAN A 164 NORTH ST NORTHAMPTON, MA 01060	HATHAWAY STEPHEN B & MARIE 32 NORTHERN AVE NORTHAMPTON, MA 01060
HATHAWAY STEPHEN B & MARIE 32 NORTHERN AVE. NORTHAMPTON, MA 01060	HATHAWAY STEPHEN B & MARIE 32 NORTHERN AVE. NORTHAMPTON, MA 01060	JACKSON CAROLE A & 90 WOODMONT RD NORTHAMPTON, MA 01060
LAVALLE ROLAND L & GABRIELE P O BOX 686 NORTHAMPTON, MA 01061	MALONEY DIANE A 168 NORTH ST NORTHAMPTON, MA 01060	MARDAS PAUL A PO BOX 60185 FLORENCE, MA 01062
MASSACHUSETTS COMMONWEALTH OF DAMON RD NORTHAMPTON, MA 01060	MESSER TIMOTHY A & EILEEN A 49 NORTHERN AVE NORTHAMPTON, MA 01060	MESSER TIMOTHY A & EILEEN A 49 NORTHERN AVE NORTHAMPTON, MA 01060
MOFFAT JAMES A JR & JUNE J & 16 NORTHERN AVE NORTHAMPTON, MA 01060	E NORTHERN AVENUE HOMES INC 31 CAMPUS PLAZA RD HADLEY, MA 01035	O'KANE EILEEN 50 NORTHERN AVE NORTHAMPTON, MA 01060
TOFINO ASSOCIATES INC 31 CAMPUS PLAZA RD HADLEY, MA 01035	TORREY ROSILAND & MARK STAPLES 45 NORTHERN AVE NORTHAMPTON, MA 01060	WALDRON ELIZABETH C 176 NORTH ST NORTHAMPTON, MA 01060
WHITE RICHARD D & ANNE E 33 NORTHERN AVE NORTHAMPTON, MA 01060	WILSON KEITH P & AMY L 20 NORTHERN AVE NORTHAMPTON, MA 01060	

# Stormwater Drainage Report

for Northern Avenue Housing Northampton, MA

November 11, 2008

Prepared by:

The Ber Des Gro

Berkshire Design Group, Inc.

4 Allen Place, Northampton, Massachusetts 01060

Prepared for: Tofino Associates, Inc. 31 Campus Plaza Road Hadley, MA 01035

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- **Appendix B** Soil Test Pit Information
- Appendix C TSS Removal Summary and Calculations
- Appendix D Standard 3 Recharge Calculations
- Appendix E Proposed Stormwater Management System Operation & Maintenance Plan
- Appendix F Long Term Pollution Prevention Plan

Appendix G Stormwater Pollution Prevention and Erosion Control Plan

#### I. Introduction

The following report presents an analysis of the stormwater management system for the proposed development of 25 housing units located off of Northern Avenue in zoning district URB in Northampton, Massachusetts. The proposed development includes 25 new housing units and associated parking areas, driveways, and sidewalks, utilities, landscape features and stormwater management system. The total site area is approximately 6 acres of which approximately 3.4 will be disturbed by construction activities. The impervious area on site will increase due to the new development and the stormwater management system has been designed to minimize proposed peak flows to reduce or match existing flows off the site. Mechanisms to reduce runoff and treat water quality include a rain garden, a proprietary treatment chamber, infiltration trench, dry wells, deep sump hooded catch basins, and 2 detention basins.

#### II. Site Terrain and Soils

The project site is comprised of gradual sloping terrain, which generally drains toward the wetlands on the west part of the site.

The USDA Soil Survey of Hampshire County, Massachusetts, Central Part report classifies the site soils as (see attached soil map):

#### • (Ra) Raynham Silt Loam

Hydrologic Group: C Flood Risk: None Depth to Water Table: 0.5'-2.0' Depth to Bedrock: >60"

#### • (Au) Amostown-Windsor Silty Substratum

Hydrologic Group: C Flood Risk: None Depth to Water Table: 1.5'-3.0' Depth to Bedrock: >60"

#### • (Ud) Udorthents Smooth

Soil formed by cutting or filling developed area. Reference pedon not given. *Assumed* Hydrologic Group: C

Stormwater Drainage Report

A series of test pits were conducted on site to determine subsurface conditions. The purpose of the test pits was to evaluate the site for the existence of ledge, the ability of the site to support stormwater drainage components, and for groundwater information. In general, the test pits confirmed the USDA Soil Survey findings for the site as ground water is generally very high throughout the site, thereby reducing the potential areas where infiltration would be feasible. The test pit logs are attached in Appendix B.

#### III. Existing Conditions

The existing site includes one drainage area: E-1. The existing drainage area boundary is depicted on the Pre-Development Drainage Area Plan (Figure 1). The overall curve number (CN) in existing conditions is 74. The control point to determine peak flow in existing conditions is the stream located on the property line west of the site shown on Figure 1 as E-CP. The following is a brief description of the drainage area:

<u>E-1</u>

E-1 is approximately 7.75 acres in size and contains existing houses, pavement, grass, wooded areas, and a large wetland area on the west part of the site. Runoff flows overland in a southwestern direction through the wetlands and to the stream located southwest of the site.

#### **IV.** Proposed Conditions

The stormwater management system in proposed conditions has been designed to treat and reduce runoff on site. The proposed site contains eight drainage areas: P-1, P-2, P-3, P-4, P-5, P-6, P-7 and P-8 (Figure 2) and the overall curve number (CN) in proposed conditions is 80. The control point to determine peak flow in proposed conditions is the stream located on the property line located west of the site shown on Figure 2 as P-CP. The following is a brief description of each drainage area:

#### <u>P-1</u>

P-1 is approximately 4.99 acres in size and contains the northwestern area of the site consisting of all of the wetland area, grass and wooded areas, and new roof and pavement. The drainage follows a similar pattern as in existing conditions. It flows overland in a southwestern direction through the wetlands and to the stream located southwest of the site. The runoff from the back of the new roof areas located within P-1 are directed to dry wells where the water is infiltrated into the ground. These dry wells are designed to be very shallow (approximately one foot in depth) due to high groundwater throughout the site. The dry wells are designed with an overflow outlet that allows roof water to sheet flow across the land toward the wetlands as it does in existing conditions. The new driveway and front roof

Stormwater Drainage Report

areas of units 1 and 2 will flow in a similar pattern as the pavement and grass area does in existing conditions.

#### <u>P-2</u>

P-2 is approximately 0.24 acres in size and is located in the eastern portion of the site. It contains a portion of the roof from unit 14 and 15 in which runoff flows through roof leaders into the infiltration trench which overflows into a catch basin within the area. This area also contains a small portion of new pavement, grass, and trees. Excluding the roof, all other runoff from this area is directed into a catch basin which flows into a water quality basin then to a detention basin (DB#2) located on the west part of the site.

#### <u>P-3</u>

P-3 is approximately 0.65 acres in size and is located in the northeastern part of the site. It contains new pavement and roof areas, grass, and a detention basin. Runoff from this area is directed to a water quality swale which flows into a water catch basin followed by a detention/infiltration basin (DB#1) that discharges approximately 100 ft to the south.

#### <u>P-4</u>

P-4 is approximately 0.34 acres in size in the east part of the site. It contains a portion of the new roof and pavement area, and grass and wooded areas. Runoff flows into a catch basin which directs the water to the infiltration trench noted is area P-2. The runoff follows the same pattern as area P-2 once within the trench.

#### <u>P-5</u>

P-5 is approximately 0.19 acres in size and is located toward the center of the developed portion of the site. It contains mostly new pavement and roof areas and a small portion is grass and wooded area. Runoff flows into a catch basin where it is directed to a water quality basin and detention basin (DB#2) which discharges approximately 40ft from the wetland, allowing adequate overland flow to occur.

#### <u>P-6</u>

P-6 is approximately 0.54 acres in size and is located on the south portion of the site. It contains a portion of the roof areas from units 16-21, new pavement, and grassed areas. The runoff is directed to a grass swale which flows into a catch basin. The catch basin flows through a proprietary stormwater treatment chamber that discharges into a detention basin (DB#2).

#### <u>P-7</u>

P-7 is approximately 0.27 acres in size and is located on the southwestern portion of the site. It contains approximately mostly new roof and paved areas and only a small portion of the area is grass. The runoff flows southwest to a proprietary treatment chamber which discharges into a detention basin (DB#2).

#### <u>P-8</u>

P-8 is approximately 0.53 acres in size and is located on the southwestern portion of the site. It contains a portion of the roof areas from units 22-25, new paved area, grass, and a detention basin (DB#2) and water quality basin. The paved area flows through a pre treatment system consisting of a stone diaphragm and grassed area which discharges into the water quality basin (rain garden) which overflows into the detention basin. The remaining area of P-8 sheet flows into the detention basin.

#### V. Calculations and Design

Drainage calculations were performed on Hydrocad Stormwater Modeling System version 8.0 using Soil Conservation Service (SCS) TR-20 methodology. The SCS method is based on rainfall observations, which were used to develop the Intensity-Duration-Frequency relationship, or IDF curve. The mass curve is a dimensionless distribution of rainfall over time, which indicates the fraction of the rainfall event that occurs at a given time within a 24-hour precipitation event. This synthetic distribution develops peak rates for storms of varying duration and intensities. The SCS distribution provides a cumulative rainfall at any point in time and allows volume dependent routing runoff calculations to occur. These calculations are included in the appendices.

The watershed boundaries for calculation purposes are divided according to the proposed site grading and the natural limits of the drainage areas. The curve numbers (CNs) and times of concentration for the existing and proposed subcatchment areas are based on the soil type and the existing and proposed cover conditions at the site. The soil hydrologic group assumed for the site is noted in Figure 3. Watershed subcatchment areas, runoff coefficients and watercourse slopes are based on survey information.

Calculations were performed for the 2-, 10-, and 100-year frequency storms under existing and proposed conditions. The results of the calculations are presented in Table 1 on the following page. Appendix A presents the Hydrocad calculations.

#### Flow Rates & Water Quantity

In the post development conditions the runoff from the proposed site will be routed to 2 open detention basins located along west part of the developed site. The proposed detention basins will attenuate peak flows in the proposed conditions through the use of outlet control structures. Stormwater will be discharged to the wetland that receives runoff in existing conditions. Although there are 5 infiltration systems are proposed (1 detention/infiltration basin, 4 dry wells and 1 infiltration trench) these were not included in the hydrocad

Stormwater Drainage Report

Northampton, Massachusetts

calculations in order to provide a more conservative runoff quantity. Table 1 on the following page presents the comparison of flow rates and water quantity at both existing and proposed control points.

#### **Table 1 Peak Flow and Volume Summary**

Condition & Point of	2-Year Storm		10-Year Storm		100-Year Storm	
Analysis	3.00"		4.50"		6.50"	
	Peak Flow	Volume	Peak Flow	Volume	Peak Flow	Volume
	Rate(cfs)	(acre-ft)	Rate(cfs)	(acre-ft)	Rate(cfs)	(acre-ft)
Existing – Control Pt. (E-CP)*	4.66	0.563	10.95	1.242	20.77	2,320
Proposed – Control Pt. (P-CP)*	4.62	0.733	10.45	1.477	18.20	2.609

*Names in parentheses refer to HydroCad model and calculations.

#### VI. MADEP Stormwater Standards Compliance

The following section details how the project will meet DEP Stormwater Management Policy's ten stormwater management standards.

#### Standard 1 - Untreated Stormwater

The proposed stormwater system is designed to treat the new point source discharge prior to flowing to the resource area. All new outlets are outfitted with flared ends and rip rap to prevent any erosion from occurring in the area. See Appendix C for TSS removal summary.

#### Standard 2 - Post-Development Peak Discharge Rates

The stormwater system is designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates leaving the site. In order to reduce runoff rates in proposed conditions 2 detention basins with outlet control structures are proposed. Note that although 5 infiltration systems are proposed, no exhilaration was included in the runoff calculations in order to maintain a more conservative peak discharge rate. Refer to Table 1 Peak Flow and Volume Summary and Appendix A for HydroCAD calculations.

#### Standard 3 - Recharge to Groundwater

Recharge to groundwater is designed to infiltrate to the maximum extent practicable in proposed conditions. The entire site consists of hydrologic group "C" soils and there is very high groundwater throughout most of the site (see Appendix B for test pit logs) which caused limitations for infiltration on many areas of the site because the separation of 2 feet from groundwater could not be

Stormwater Drainage Report

met. Where possible, infiltration is proposed: half of the areas of the roof from units 1-15 and 22-25 and a portion of the pavement located toward the center of the development are directed to dry wells and an infiltration trench sized to accommodate these areas. The upper detention/infiltration basin (DB#1) has been designed also hold and infiltrate the required recharge volume for its respective drainage area (see Appendix D for recharge calculations). Due to restrictions of the site terrain and soil conditions, not all of the impervious area could be directed to an infiltration system therefore all 5 of the infiltration systems proposed are designed to hold at least twice the required recharge volume and still drawdown within 72 hours in order to meet Standard 3 to the maximum extent practicable (see Appendix D for recharge calculations).

#### Standard 4 - Water Quality

The proposed stormwater management system has been designed to remove the average annual Total Suspended Solids (TSS) load in excess of 80% for the proposed site conditions (see Appendix C for calculations). There are 4 separate treatment chains proposed:

#### Treatment Train 1(total of 85% TSS removed)

The first treatment chain contains the impervious areas within P-3. The runoff is directed into a water quality swale to a catch basin which discharges into detention/infiltration basin (DB#1) which has been designed to hold the required water quality volume for its respective area which achieves a total TSS removal rate of approximately 85%. Note that the water quality swale was not included in the calculations of total TSS removal in Appendix C to maintain a more conservative removal rate.

#### Treatment Train 2(total of 93% TSS removed)

The second treatment chain contains the impervious areas from P-2, P-4, and P-5. The runoff is directed into a catch basins followed by a water quality basin (rain garden) which achieves a total TSS removal rate of approximately 93%. The water quality basin has been designed to hold a larger volume of water (738cf) than the water quality volume required (713cf) for the impervious area directed to it.

#### Treatment Train 3(total of 90% TSS removed)

The second treatment chain contains the paved impervious areas from P-8. The runoff is through a pretreatment system consisting of a stone diaphragm and grassed area which discharges into a water quality basin (rain garden) which achieves a total TSS removal rate of approximately 90%. The water quality basin has been designed to hold a larger volume of water (738cf) than the water quality volume required (713cf) for the impervious area directed to it.

Stormwater Drainage Report

#### Treatment Train 4(total of 83% TSS removed)

The third treatment chain contains the impervious areas from P-6 and P-7. The runoff is directed into catch basins and then to a proprietary treatment chamber (Stormceptor STC 900*) which achieves a total TSS removal rate of approximately 83%.

*Note: The stormwater treatment chamber has been sized based on MASTEP test evaluations. The attached table in appendix C displays TSS removal rates for systems based on the impervious area directed to the system. See attached Stormceptor sizing chart for impervious areas directed to the stormwater treatment chamber.

In addition to removal of TSS, a Long Term Pollution Prevention Plan has been created to maintain a clean site and ensure that all BMPs are functioning to their maximum potential. See Appendix F for Long Term Pollution Prevention Plan.

<u>Standard 5 - Higher Potential Pollutant Loads</u> The proposed project is not expected to yield high potential pollutant loads.

<u>Standard 6 - Protection of Critical Areas</u> The project site does not discharge to critical areas as defined in MA DEP Stormwater Policy Handbook.

Standard 7 - Redevelopment Projects

The redevelopment of previously developed site standard is not applicable for this project.

#### Standard 8 - Erosion/Sediment Control

Erosion and sediment controls have been incorporated into the project design to prevent erosion, control sediments, and stabilized exposed soils during construction and land disturbance. See Appendix G for Construction Period Pollution Prevention and Erosion Sedimentation Control.

#### Standard 9 - Operation/Maintenance Plan

An Operation and Maintenance Plan for the proposed project is included in Appendix E. It includes general controls for construction and long term maintenance of the stormwater management system.

#### Standard 10 – Prohibition of Illicit Discharges

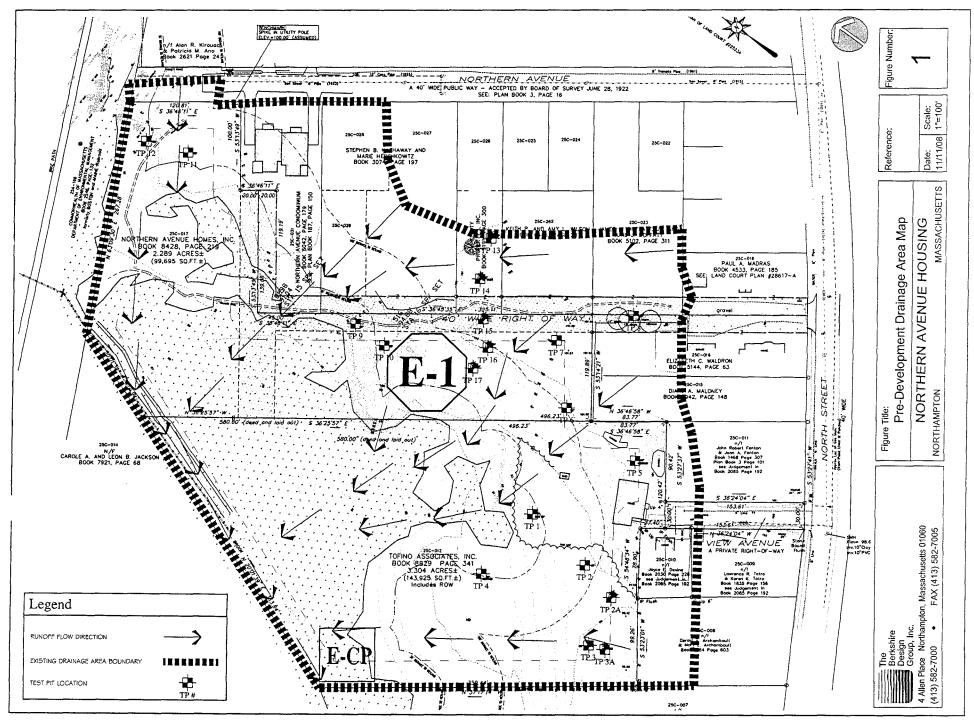
No Illicit Discharge Compliance Statement is included with this report however one will be submitted prior to the discharge of any stormwater to postconstruction BMPs.

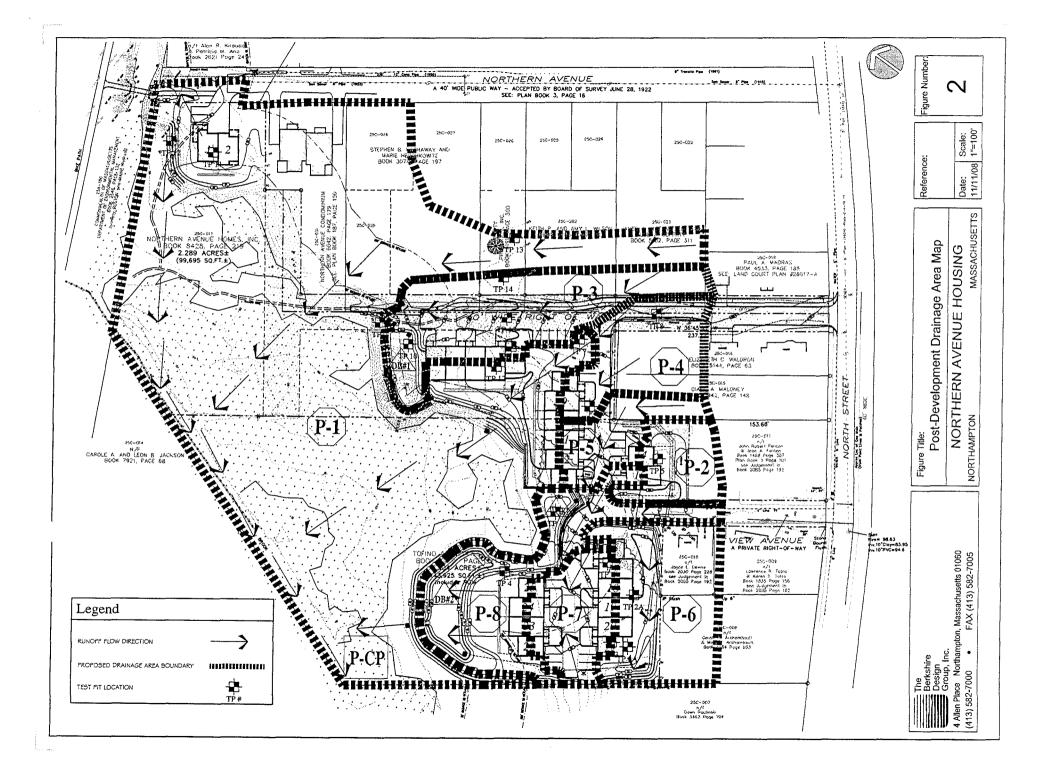
#### VII. Summary

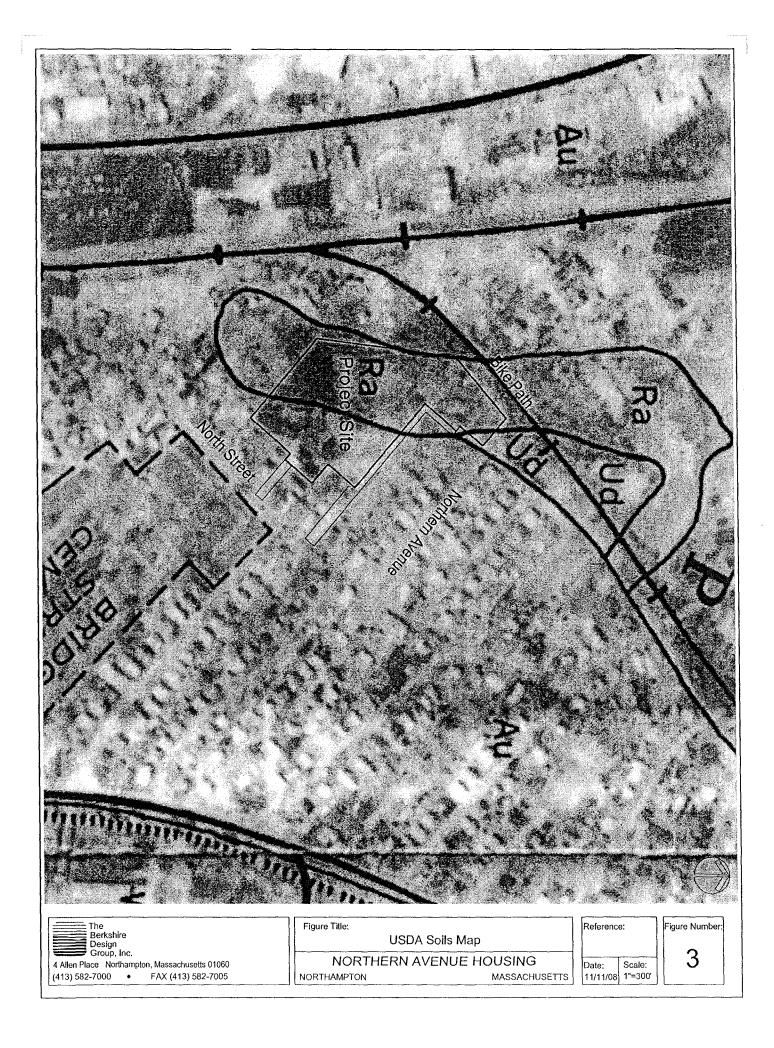
The impervious area from existing to proposed conditions will increase by approximately 51,000 sf from the new roadway and housing units. The proposed stormwater management system is designed to maintain or reduce the peak flow rates in proposed conditions for the 2-, 10-, and 100-year storm frequencies. Special care has been taken to treat runoff with a series of best management practices to ensure water quality and annual TSS removal rates in excess of 80%. These methods include deep sump hooded catch basins, a bioretention basin, a detention/infiltration basin, and a stormwater treatment chamber.

#### VIII. References

United States Department of Agriculture. 1998. Soil Survey of Hampshire County (Central Part), Massachusetts.









#### **Massachusetts Department of Environmental Protection** Bureau of Resource Protection - Wetlands

# WPA Form 2 – Determination of Applicability

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

A. General Information

<b>Important:</b> When filling out	Fro	om:					
forms on the		Northampton			x		
computer, use only the tab		Conservation Commission	·····				
key to move your cursor -	To:	Applicant			Property Owner (if dif	ferent from ap	oplicant):
do not use the		Northern Avenue Homes, II	nc and Tofi	no	Douglas Kohl		
return key.		Associates			Name /		
A COLORIZATION OF COLORIZATIONO OF COLORIZATICO OFICICO		31 Campus Plaza Road			31 Campus Plaza Road		
Ind		Mailing Address			Mailing Address		
×/		Hadley	MA	01035	Hadley	MA	01035
		City/Town	State	Zip Code	City/Town	State	Zip Code
	1.	Title and Date (or Revised	Date if appl	licable) of Fina	al Plans and Other Docu	iments:	
		"Topographic" Plan of Land	l in Northar	npton, Massa	chusetts prepared for	Auġust 2	20, 2007
		Northern Avenue Homes, II	nc.			Date	
		· · · · · · · · · · · · · · · · · · ·			·		
-		Title				Date	
		·			·		
		Title				Date	
	2.	Date Request Filed:					
		June 20, 2007		•			
		······································					

#### **B.** Determination

Pursuant to the authority of M.G.L. c. 131, § 40, the Conservation Commission considered your Request for Determination of Applicability, with its supporting documentation, and made the following Determination.

Project Description (if applicable):

Resource	Area	Delineation

Project Location:

Northern Avenue Street Address 25C

Assessors Map/Plat Number

Northampton	
City/Town	
12 & 17	
Parcel/Lot Number	



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands

# WPA Form 2 – Determination of Applicability

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

## B. Determination (cont.)

The following Determination(s) is/are applicable to the proposed site and/or project relative to the Wetlands Protection Act and regulations:

#### **Positive Determination**

Note: No work within the jurisdiction of the Wetlands Protection Act may proceed until a final Order of Conditions (issued following submittal of a Notice of Intent or Abbreviated Notice of Intent) or Order of Resource Area Delineation (issued following submittal of Simplified Review ANRAD) has been received from the issuing authority (i.e., Conservation Commission or the Department of Environmental Protection).

1. The area described on the referenced plan(s) is an area subject to protection under the Act. Removing, filling, dredging, or altering of the area requires the filing of a Notice of Intent.

2a. The boundary delineations of the following resource areas described on the referenced plan(s) are confirmed as accurate. Therefore, the resource area boundaries confirmed in this Determination are binding as to all decisions rendered pursuant to the Wetlands Protection Act and its regulations regarding such boundaries for as long as this Determination is valid.

The intermittent stream and wetlands delineation, as shown on the referenced plan, have been confirmed as accurate. Vernal pools have been identified within the area shown as wetlands and have not been delineated.

2b. The boundaries of resource areas listed below are <u>not</u> confirmed by this Determination, regardless of whether such boundaries are contained on the plans attached to this Determination or to the Request for Determination.

3. The work described on referenced plan(s) and document(s) is within an area subject to
protection under the Act and will remove, fill, dredge, or alter that area. Therefore, said work
requires the filing of a Notice of Intent.

- 4. The work described on referenced plan(s) and document(s) is within the Buffer Zone and will alter an Area subject to protection under the Act. Therefore, said work requires the filing of a Notice of Intent or ANRAD Simplified Review (if work is limited to the Buffer Zone).
- 5. The area and/or work described on referenced plan(s) and document(s) is subject to review and approval by:

City of Northampton	
Name of Municipality	

Pursuant to the following municipal wetland ordinance or bylaw:

Northampton Wetlands Ordinance	Chapter 337 of the Code of
Name	Ordinances



#### Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands

# **WPA Form 2** – Determination of Applicability

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

### B. Determination (cont.)

- 6. The following area and/or work, if any, is subject to a municipal ordinance or bylaw but not subject to the Massachusetts Wetlands Protection Act:
- 7. If a Notice of Intent is filed for the work in the Riverfront Area described on referenced plan(s) and document(s), which includes all or part of the work described in the Request, the applicant must consider the following alternatives. (Refer to the wetland regulations at 10.58(4)c. for more information about the scope of alternatives requirements):
  - Alternatives limited to the lot on which the project is located.
  - Alternatives limited to the lot on which the project is located, the subdivided lots, and any adjacent lots formerly or presently owned by the same owner.
  - Alternatives limited to the original parcel on which the project is located, the subdivided parcels, any adjacent parcels, and any other land which can reasonably be obtained within the municipality.
  - Alternatives extend to any sites which can reasonably be obtained within the appropriate region of the state.

#### **Negative Determination**

Note: No further action under the Wetlands Protection Act is required by the applicant. However, if the Department is requested to issue a Superseding Determination of Applicability, work may not proceed on this project unless the Department fails to act on such request within 35 days of the date the request is post-marked for certified mail or hand delivered to the Department. Work may then proceed at the owner's risk only upon notice to the Department and to the Conservation Commission. Requirements for requests for Superseding Determinations are listed at the end of this document.

1. The area described in the Request is not an area subject to protection under the Act or the Buffer Zone.

- 2. The work described in the Request is within an area subject to protection under the Act, but will not remove, fill, dredge, or alter that area. Therefore, said work does not require the filing of a Notice of Intent.
- 3. The work described in the Request is within the Buffer Zone, as defined in the regulations, but will not alter an Area subject to protection under the Act. Therefore, said work does not require the filing of a Notice of Intent, subject to the following conditions (if any).
- 4. The work described in the Request is not within an Area subject to protection under the Act (including the Buffer Zone). Therefore, said work does not require the filing of a Notice of Intent, unless and until said work alters an Area subject to protection under the Act.



#### Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands WPA Form 2 – Determination of Applicability

VFA FOITH 2 - Determination of Applicabilit

Massachusetts Wetlands Protection Act M.G.L. c. 131, §40

## B. Determination (cont.)

5. The area described in the Request is subject to protection under the Act. Since the work described therein meets the requirements for the following exemption, as specified in the Act and the regulations, no Notice of Intent is required:

Exempt Activity (site applicable statuatory/regulatory provisions)

6. The area and/or work described in the Request is not subject to review and approval by:

Name of Municipality

Pursuant to a municipal wetlands ordinance or bylaw.

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Ordinance or Bylaw Citation

# C. Authorization

Name

This Determination is issued to the applicant and delivered as follows:

by hand delivery on	by certified mail, return receipt requested on
Ave 24, 2007 Date	Date

This Determination is valid for **three years** from the date of issuance (except Determinations for Vegetation Management Plans which are valid for the duration of the Plan). This Determination does not relieve the applicant from complying with all other applicable federal, state, or local statutes, ordinances, bylaws, or regulations.

This Determination must be signed by a majority of the Conservation Commission. A copy must be sent to the appropriate DEP Regional Office (see <u>http://www.mass.gov/dep/about/region.findyour.htm</u>) and the property owner (if different from the applicant).

Signa

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Avb 23,2007